An extended model to predict the compressive, tensile and flexural strengths of HPFRCs and UHPFRCs: definition and experimental validation

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Abstract

High manufacturing costs of UHPFRC and expensive and time-consuming tests performed to understand the mechanical response under loading restrict still its wider applications in the field of the structural engineering. Predictive models can be useful to reduce the number of requested tests and to optimize the amount of compounds of the mixture, for example detecting the minimal dosage of fibers necessary to attain a given tensile strength and toughness as well. Currently, not many predictive models do exist and one of the most recent, developed in order to estimate the compressive and tensile responses of HPFRCs, was not notably suitable for UHPFRCs. The main purpose of this work concerns the extension of such a model, in order to predict the mechanical response (in flexion as well) of a given HPFRC/UHPFRC for any change of matrix and fiber properties. Theoretical results were compared with experimental data, thus confirming some shortcomings of the previous model. Once the matrix and fiber properties of a marked UHPFRC were selected, the extended model was used to predict the tensile and flexural bending responses of a full scale UHPFRC structural beam, showing good agreement with the experimental results.

Keywords: Metal-matrix composites; Mechanical properties; Damage

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1. Introduction

Available technical guides and professional recommendations define the Ultra-High-Performance-Concrete (UHPC) in different ways [53, 57, 56, 55]. However, the mechanical behavior of UHPFRCs in tension can be strain-softening or strain-hardening, according to the product features [28]. Many researchers have discovered the main parameters influencing such a mechanical response [16]. Matrix properties are highly dependent on various factors such as the dosage of fine mineral admixtures [4, 34, 41, 46], size of aggregates [6, 25, 31], size effect of the specimen [1, 18, 29], curing condition [19, 50] and rate of loading [14, 15]. Not less important is the water-to-binder ratio that strongly affects the classical high strength and the flow-able characteristic of the UHPC matrix with the presence of steel fibers [54, 56]. Other works also focused on fiber properties that mostly affecting the mechanical response in tension of UHPFRCs. The fiber shape is closely related to the magnitude of the post-cracking strain capacity of UHPFRC. Previous studies showed the difference in magnitude of pullout strength when the shape of fibers changes [43]. A comparison of results by using straight and deformed fibers highlighted that hooked-end and twisted steel fibers achieve a maximum fiber stress three times higher than straight steel fibers, as also confirmed in [42]. The aspect ratio \( l/d_e \) (\( l = \) length of fiber, \( d_e = \) equivalent diameter) also largely influences the post-cracking behavior of UHPFRC. Adding steel fibers with a high \( l/d_e \) (97.5), [47] improved the fracture energy of about 35% and 121% as compared to fibers of medium (81.5) and low (65) \( l/d_e \), respectively. This effect is mainly due to the increase of the bonding area between the matrix and fibers, leading to higher pullout load carrying capacity. In [42] by increasing the Volume Fraction of fibers embedded within the UHPC (\( V_f \)) from 1.5 to 2.5%, both tensile strength and strain capacity were improved of about two times. Other works have been conducted to evaluate how the fiber orientation influences the mechanical response of UHPFRC, e.g. [2, 47]. In [13] was shown that a properly designed casting

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1Recent studies about the mechanical performances of fabric-reinforced cementitious matrix composites can be found in [11, 12, 30, 38], whereas an application of a polymer-based mortar for retrofitting has been reported in [20].
placement should improve the fiber orientation, leading to better tensile per-
formances. For horizontal placements the viscosity of the fluid mixture and
the wall effect [26] cause almost all fibers to be aligned perpendicularly to
the pouring direction [3] and parallel to its flow in the molding [14].
Few authors attempted to take into account some of properties discussed
above in order to accurately predict the compressive and tensile splitting
strengths of a given FRC, e.g. [33, 39, 45]. The work of [35] focused both
to predict the tensile strength by uniaxial tests, being more realistic than
splitting tests, and to improve the reliability of previous models extending
the investigation towards more types of fibers and dosages. Despite the good
results, its application was limited to the fact that only one type of matrix
was investigated, confirming its reliability only for concretes with the same
strength range (HPFRC). The present work aims at extending the model
proposed in [35] in order to predict the compressive and the uniaxial tensile
strengths for any HPFRC/UHPFRC as matrix and fiber properties change.
The extended model can also estimate the toughness magnitude under flex-
ural bending stress conditions. Its reliability will be discussed by predicting
the mechanical performances of a full scale structural beam.
The present work is organized as follows: a description about the materials
and test methods adopted in the experimental program are provided in Sec-
tion 2 in Section 3 the most relevant results of the experimental investigation
are highlighted; the extended model is presented in Section 4; conclusions are
drawn in Section 5.

2. Experimental program

The empirical previous model developed in [35] was here extended in
order to predict the compressive, tensile and flexural bending strengths of
a given HPFRC/UHPFRC for any change of matrix and fiber properties.
Experimental data of strength tests recorded on both marked UHPFRC (la-
beled hereafter UHPFRC-A) and marked HPC series - investigated in [35]-
by varying fiber properties, were taken into account for this purpose. In
order to confirm the reliability of the extended model, the mechanical per-
formance of a marked UHPFRC full scale structural beam (labeled hereafter
UHPFRC-B) was evaluated and compared with the model prediction.
2.1. Materials

Four types of steel fibers, different in shape (straight and hooked-end) and aspect ratio $l/d_e$ (65, 75 and 85), as illustrated in Fig.1, were selected in order to reinforce the UHPC-A matrix and realize several series of specimens. Four different volume fractions $V_f$ were treated for each kind of fiber investigated, i.e. 0, 1.5, 2 and 3%. Dosages higher than 3% caused fiber balling in the fresh mixture. Each series was composed of three standard 100 × 100 × 100 mm cubes and three dog-bone-shaped specimens, whose geometry is illustrated in Fig.2, of matrix reinforced with a given type of fibers and dosage. For example, the specimens in the first series contain straight fibers with $l/d_e$ of 65 and $V_f$ of 1.5%. Each series is labeled according to the shape of the studied fiber, $l/d_e$, and $V_f$. SF and HF stand for straight fiber and hooked fiber; 65, 75, 85 represent the $l/d_e$ ratio; 1.5, 2, 3 are the $V_f$ values. Also a series of specimens without fibers was made as control.

A full scale structural 80 × 1000 × 10000 mm beam of UHPFRC-B was cast in-situ. No thermal treatment was applied after casting. The beam was kept in the molds for at least 20 hours then was demolded, protected with plastic sheets and kept inside the precasting plant until 28 days. Six 80 × 100 × 500 mm long beams and six ø 50 × 200 mm cores specimens were drilled from the structure in order to test the uniaxial tensile and bending flexural strengths. The geometry of the full scale beam and the position of the drilled specimens are illustrated in Fig. 3. As control, a UHPFRC-B series of 100 × 100 × 100 mm cube and dog-bone shaped specimens were made in lab according to standard conditions. A series of specimens without fibers was also made.

In order to understand the scatter in strength between cores and cast (cylinder) specimens a proper study is discussed afterwards, by using a marked UHPFRC (labeled hereafter UHPFRC-C), see Table 1.

The mix design of UHPFRCs here investigated was provided by the manufacturer (Table 2), even though for UHPFRC-A series different kinds of fibers and dosages were investigated. Typically, marked UHPFRCs include an optimized gradation of granular matter to obtain a high packing density. A high intensity mixer was used to ensure the mix homogeneity. The fibers were inserted in the mix in order to obtain a good dispersion and minimizing the risk of fiber balling. The specimens were made and cured in compliance to the European standards [58].
2.2. Test set-up

The amount of fibers within the UHPFRC-A (cubic and dog-bone-shaped) specimens was investigated by measuring the hardened-state density in all series according to [60]. Standard uniaxial tensile tests on dog-bone-shaped and cores and standard four-point flexural bending tests on the beams drilled from the full scale structure were performed by using a machine Walter Bay.
Table 1: Specimens parameters

<table>
<thead>
<tr>
<th>UHPFRC series</th>
<th>cube</th>
<th>dog-bone cores</th>
<th>drilled density</th>
<th>weight</th>
<th>Yield strength</th>
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<tr>
<td>A_Control</td>
<td>3</td>
<td>3</td>
<td>0</td>
<td></td>
<td>-</td>
</tr>
<tr>
<td>A_SF65,1.5</td>
<td>3</td>
<td>3</td>
<td>1.5</td>
<td>65</td>
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<tr>
<td>A_SF65,2</td>
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<td>3</td>
<td>2</td>
<td>65</td>
<td>1.11x10^-5</td>
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<td>A_SF65,3</td>
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<td>3</td>
<td>3</td>
<td>65</td>
<td>1.11x10^-5</td>
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<tr>
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<tr>
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<td>3</td>
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<td>1.5</td>
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</tr>
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<td>2</td>
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<td>2.27x10^-5</td>
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<tr>
<td>A_HF65,3</td>
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<td>3</td>
<td>85</td>
<td>2.27x10^-5</td>
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<td>A_HF85,2</td>
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<td>1.11x10^-5</td>
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<tr>
<td>A_HF85,3</td>
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<td>3</td>
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<tr>
<td>B_SF65,2,5</td>
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<td>2.5</td>
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<td>C_SF130,0,6</td>
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<td>6</td>
<td>0.6</td>
<td>130</td>
<td>2.77x10^-6</td>
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Table 2: Mix design

<table>
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<tr>
<th>Compounds</th>
<th>kg in 1 m³ of composite</th>
</tr>
</thead>
<tbody>
<tr>
<td>Composites</td>
<td>UHPFRC-A</td>
</tr>
<tr>
<td>Premix (cement, silica fume, quartz sable)</td>
<td>1970</td>
</tr>
<tr>
<td>Superplasticizer</td>
<td>39</td>
</tr>
<tr>
<td>Water</td>
<td>195</td>
</tr>
<tr>
<td>Straight steel fibers 13/0.175 mm</td>
<td>296 (3.8 %)</td>
</tr>
<tr>
<td>Straight steel fibers 20/0.3 mm</td>
<td>-</td>
</tr>
<tr>
<td>Straight steel fibers 20/0.15 mm</td>
<td>-</td>
</tr>
</tbody>
</table>
type LVF-200 kN, according to [51] and [57], respectively. The axial characteristic length of the strain gauge was 100 mm for all specimens. The axial elongation rate was set at 0.05 ± 0.01 mm/min. The end sides of the dog-bone-shaped specimens were larger than the central part, thus allowing the clamps of the machine to easily hold them during the test and to ensure that the failure occurs in the central zone. The compressive tests on cube and cylinder specimens were carried out by using a machine Perrier type 138-5000 kN, according to [59]; the loading rate was 0.6 MPa/s. After testing, UHPFRC-A specimens were cut near to the cracking section for a visual examination of the fibers orientation and distribution.

3. Results and discussions

3.1. Distribution and orientation of fibers (UHPFRC-A series)

Even though the procedures of mixing, fiber dispersion and casting were the same for all specimen series, the fresh mixture of HF85 series showed a phenomenon of fiber balling, see Fig. 4. It is worth noting that fiber balling affects the mechanical strength of the hardened UHPFRC as well and it creates honeycombs reducing the quality of the UHPFRC even in large scale production. These problems are magnified if an inappropriate mixer is used. Consequently HF85 series had to be discarded from the investigation. The use of special mixers and/or a proper selection of fiber type and volume fractions could permit to avoid the fiber balling. A conventional approach is to use multiple fibers bonded together with water-soluble adhesive [5]. This solution was adopted by replacing HF85 with such a kind of fibers (HF65). By a visual examination at the mixing, the vertical pouring of the fresh mixture into dog-bone-shaped molds promoted a certain level of orientation of fibers along the main axis of the specimen. This phenomenon, promoted by shear stresses, arises due both the high viscosity of the fresh mixture and the wall effect of the mold [26]. The fiber orientation is promoted by the wall effect that, together with the complex geometry of the dog-bone shaped mold, tends to slightly reduce the $V_f$ of the fiber in the specimens. In fact, by measuring the hardened-state density in each series it was found that the average density of dog-bone shaped specimens (labeled D in Fig.5a) was slightly lower than cubic specimens (labeled C) for all dosages, as also

\[^2\text{Viscoelastic effects in reinforced concrete structure have been accounted e.g. in [7, 8, 9].}\]
observed in [35]. The cubic molds were filled vertically, therefore an isotropic and homogenous distribution of fiber was expected. After testing, dog-bone-shaped specimens were cut near to the failure sections showing a preferential orientation of fibers. In cubic specimens the fibers were aligned mainly in horizontal planes and perpendicular to the loading force/pouring direction, see Fig. 5(b).

Figure 4: Phenomenon of fiber balling occurred in HF85 series

Figure 5: (a) Comparison of the specimens density; (b) Visual orientation and distribution of fibers in series a) SF65-D, b) SF65-C, c) SF75-D, d) SF75-C, e) HF65-D, f) HF65-C (b)
3.2. Influence of fibers on compressive strength (UHPFRC-A series)

It is observed that fibers increased the compressive strength $f_c$ until 39% as both $l/d_e$ and $V_f$ increased, even though the magnitude is different for each kind of fiber and dosage. In certain works, it was observed that the compressive strength is not affected significantly by the fiber presence, e.g. [49] et. al. Nevertheless the compressive strength is also strongly influenced by the homogeneity of the fiber dispersion that can be achieved by detecting the optimum fiber dosage or a range of optimum fibers dosages. In [48] an increase of compressive strength was observed up to a fiber dosage of 3%. In [32] the investigated UHPFRC recorded the highest compressive strength with a fiber dosage of 2%, whereas in [50] the compressive strength continuously increased with an increase of fiber dosage until to 4%. Similar results were also observed in [10]. This behavior has been observed in this investigation as well. In particular, SF75 series showed a higher increase of strength (up to 39%) compared to SF65 series (up to 30%), as $V_f$ increases. For fibers with same aspect ratio, HF series showed lower increase of strength, compared to SF series, for low $V_f$ (1.5%). As $V_f$ increases, HF series involves higher gain of strength, see Fig 11. Further details are drawn in Table 3. Since dosages of fibers higher than 3% caused problems of both balling and workability in the mix, $V_f = 3\%$ is considered the upper limit for achieving the best mechanical performances of such a UHPFRC. For all series the favorable orientation of fibers within the mixture permitted to gain toughness, well counteracting the opening cracks.

3.3. Influence of fibers on uniaxial tensile response (UHPFRC-A series)

The mechanical response under uniaxial tension is generally subdivided into three phases. Tensile strength tests carried out in the investigation showed a classical three-linear behavior, see Fig 6, with a linear elastic branch maintained up to 90-95% of the cracking strength, a phase of multi-cracking of the matrix and, finally, a softening behavior due to the debonding between fibers and matrix until a residual strength $f_{rt}$ is reached. The tensile strength $f_t$ was reached for uniaxial strain values of about 0.015%, for all series. $f_{t,matrix}$ value was 6.1 MPa. Instead, for series SF65, SF75, HF65 the maximum and minimum $f_t$ values were 9.79, 7.95, 7.62 and 6.96, 5.71, 6.13 MPa, respectively. The ratio $f_t/f_{t,matrix}$ reached about 160%. For all series, $f_t$ increased with increasing $V_f$ until the upper limit of 3% was reached. Before first cracking occurs, the stress-strain behavior was not significantly influenced by the shape of tested fibers, even though the higher number of straight
fibers in the cross-section, as compared to HF series, led to larger increasing of the first cracking strength, see Table 3. Fibers were mainly oriented along the main axis of the dog-bone-shaped specimen, see 3.1, which perpendicularly to the crack planes conferred gain of toughness in post-cracking. After the matrix crack initiation, the stress was absorbed by the fibers bridging the cracks. Whereas the strain of straight fibers causes the debonding from the matrix and consequently a total pull out, in the case of hooked-end fibers debonding is preceded by the straightening of hooked-ends that retains the fiber from being pulled out, thus extending the energy-absorbing capability (Part II in Fig 6). However, the magnitude of toughness also depends on both fiber size and amount of fibers bridging the crack plane. In the investigated series, for a given \( V_f \), the number of hooked-end fibers bridging the cracking section was lower compared to one of the straight fibers series because the size of hooked-end fiber was bigger, see Fig 5b. As explained before, it was observed that SF series showed also better post-cracking branches than HF series, highlighting the key role of fiber size and their amount. The residual strength \( f_{rt} \) is here defined as the yield strength corresponding to 1.5% of axial strain. For series SF65, SF75, HF65 the maximum and minimum \( f_{rt} \) values were 4.24, 2.01, 1.83 and 2.24, 1.5, 0.97 MPa, respectively (see Fig 11).
3.4. Mechanical strength of full scale structural beam and influence of coring (UHPFRC-B series)

Experimental graphs recorded by uniaxial tensile and flexural bending tests on UHPFRC-B specimens were reported in Fig. 7. The average $f_t$ of cores was of 8.6 MPa, about 25% lower than the values recorded for dog-bone shaped specimens (11.42 MPa). Also the toughness was lower. This difference can be ascribed to the fact that the in cast specimens the molds shape encouraged a certain degree of fibers orientation, while in the cores drilled from the full scale structural beam fibers were randomly oriented. Also the fact that cores extraction and conditioning promote a certain degree of damage on the specimens may have influenced this result. An investigation concerning such a phenomenon is reported in Section 3.5.

3.5. Performance comparison between cast and cored specimens (UHPFRC-C series)

A study on the loss of compressive strength on cores was conducted in an UHPFRC (labeled UHPFRC-C) designed for precast non-structural elements. The mix design is listed in Table 2. 15 cylinders ø 110 × 220 mm were cast along with three ø 100 × 200 mm cylinders and a 200 × 210 × 600 mm beam. The beam was further instrumented with two fiber optic sensors placed parallel to the shorter side of the mold at a distance of 52 mm from the side. The two sensors were placed about 45 mm apart in order to have one sensor on the center of the specimen and one on the side, thus avoiding the bits of the barrel ripping the sensors, see Fig. 8.

In Fig. 9a the deformation of the sensors is expressed in micro strain $\mu \epsilon$, while in Fig. 9b the temperatures are shown for the central and the side sensors. The temperature sensors seem to demonstrate that the water used for cooling the barrel did not have any visible effect in terms of deformations between core and skin of the core (thus producing a self-strain). A jump of some degrees of temperature was visible after 30 minutes of coring in the external part of the core due to an adjustment of the flow of cooling water. The external layer of the concrete tended to contract while the core expanded. At the end of the coring phase the specimens were left in the socket and the water was stopped (in the space left by the barrel there was no water because it escaped from the bottom immediately after the barrel was extracted). From

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3Mechanical modelling of damage can be found, as an example, in [21, 22, 23, 10].
that moment no further deformation was observed.
A possible explanation for the distortion of the section can be found in the release of a self-restrain or in the effect of the coring barrel. The eventual
Figure 9: Deformation and temperature of the side and center sensors at the coring operation.

Figure 10: a) Compressive strength of cylinder and core specimens at 3, 7 and 28 days; b) Compressive strength at 28 days of different size of specimens and molds types.

Water pressure on the side and the temperature of the cooling water did not seem to have any effect on this concrete. Compressive strength of cores with length-diameter ratio equal to 2 was tested. The cores were stronger...
at early age (when the higher temperatures reached in the cored beam allow for a faster hydration) while at 28 days they test lower of more than 10%, thus confirming that the strength retrogression occurred also in this case (Fig. 10a).

In order to confirm that size of specimens and molds type were not an issue, four different types of specimens were tested for compressive strength at 28 days, i.e. two cores of different diameter (real diameter of the core were 94 and 74 mm, length was the double of the diameter in both cases) and two cast cylinders (diameter 110 and 100 mm, length double of the diameter, coated with paper box and plastic molds respectively). Fig. 10b shows that cores had similar strength in average and cast cylinder as well. This permitted to check if this potential source of error was having any effect. The average weight of all cores was 2510 kg/m$^3$ while the average weight of the cylinders was of about 2550 kg/m$^3$. This difference highlights that the concrete had the same degree of compaction in both cylinders and beam. It can therefore be affirmed that the extraction of cores in UHPFRC provoke a distortion of the section that can be quantified in about 100 $\mu$ε. This distortion is not due to the coring but by the extraction of the core from the structural element. However this distortion and the torsion promoted by the barrel coring the concrete might provoke enough microcracking in specimens of UHPFRC with low fibers content. This parameter should be taken carefully into account whenever the strengths of UHPFRC in the structure and in specimens are compared.

Figure 11: Increase of mechanical strengths as steel fibers are added within the UHPC-A
The coefficients of correlation $R^2$ illustrated in Fig.12 are higher than those in [35], highlighting the strong influence of the matrix strength for a reliable prediction. Since matrix strength and fiber properties of the UHPFRC-B full scale structural member were known, the model was used to predict its compressive and tensile strengths by using relationships in equations (1)-(6). Theoretical and experimental results of UHPFRC-B specimens were compared and drawn by red points. Once the compressive and tension strengths were predicted, it was possible to compute the flexural bending response by analytical approach. The Euler-Bernoulli hypothesis was adopted. A
Figure 12: Correlation between measured (Table 3 and Table 3 in [35]) and predicted values of compressive, uniaxial and residual tensile strengths by the extended model (a-f) and the model in [35] (g-l).
Figure 13: Correlation between experimental data of a, b, c ([36]), d (UHPFRC-B series) and theoretical results both of the extended model and previous model developed in [35].

A parabola-rectangular stress-strain law in compression and bi-linear stress-strain laws in tension defined according to [52] and [57] were adopted in the model. 0.015% and 1.5% were assumed as elastic and ultimate strain tension values, as observed in Section 3.3. A numerical solver was used for computing the flexural response of the beam in terms of bending moment (kNm) vs opening crack at the bottom (mm).

The comparison with experimental data was observed in Fig. 13. It is worth noting that the prediction of flexural strength for the scale structural beam was reasonable due both to the not-preferential orientation of fibers within the cores and to the light damage of the latter during the coring and extraction, as claimed in [35]. This phenomenon was not evidenced when theoretical results were compared to experimental data measured in [36], where a (HPFRCC), b (UHPFRC-I) and c (UHPFRC-2) series of six $150 \times 150 \times 600$
mm beams, cast and cured in lab conditions, showed a preferential orientation of fibers inside. For them the convergence with the extended model was much higher. Lower convergence is instead observed when the model in [35] was adopted for the prediction, thus confirming the need of a new extended model.

\[ f_{c, SF} = 1.067 f_{c, matrix} + 5.9562 l - 393.2199 d_e + 3.3258 V_f, R^2 = 0.92 \]  
(1)

\[ f_{t, SF} = 0.9788 f_{t, matrix} - 0.9309 l + 59.6367 d_e + 1.2677 V_f, R^2 = 0.91 \]  
(2)

\[ f_{rt, SF} = 0.1644 f_{t, matrix} - 0.0507 l + 12.0514 d_e - 0.2117 V_f, R^2 = 0.82 \]  
(3)

\[ f_{c, HF} = 1.3757 f_{c, matrix} - 0.8456 l - 17.7099 d_e + 7.0429 V_f, R^2 = 0.90 \]  
(4)

\[ f_{t, HF} = 0.8526 f_{t, matrix} - 0.0747 l - 5.3867 d_e + 0.8551 V_f, R^2 = 0.90 \]  
(5)

\[ f_{rt, HF} = 0.1163 f_{t, matrix} - 0.0692 l - 3.9987 d_e + 0.5861 V_f, R^2 = 0.86 \]  
(6)

5. Conclusions

The following main conclusions can be drawn:

- The influence of both matrix and steel fibers properties on the mechanical response of a given HPFRC/UHPFRC was investigated, confirming their key role as predictive parameters;

- A previous predictive strength model was extended in order to estimate the mechanical response in terms of compressive and tensile strengths for any HPFRC/UHPFRC, as matrix and fiber properties change, showing higher \( R^2 \) values. Furthermore, the new model was used to estimate the flexural bending response of a full scale structural beam and different marked UHPFRC beam specimens. A good agreement with the experimental results was evident. The regression
analysis on more experimental data could be reduce the scatter of tensile strength results, typically high for the fiber reinforced mortars, in order to accurate the prediction of the related post-peak flexural response;

- A good agreement between the extended model and experimental data confirms not only that the model predicts well the mechanical behavior of any HPFRC/UHPFRC, but also that it can be used for detecting the optimal combination of matrix strength and fiber properties in order to identify the minimal dosage of fibers (or the minimal matrix strength) necessary to attain the strength requested in the field, reducing the costs of manufacturing as well;

- The fiber orientation strongly affects both the peak strength and the energy-absorbing capability of the post-cracking behavior, as seen by comparing the experimental results of cast and core specimens. In fact, in the cast specimens the molds shape encouraged a certain degree of fibers orientation, while in the cores drilled from the full scale structural beam fibers were randomly oriented;

- Another relevant effect of scatter in strength between cast and core specimens can be explained by considering the distortion of the section in the release of a self-restrain or in the effect of the coring barrel.

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References


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2. Geometrical dimensions (mm) of the standard dog-bone shaped specimen according to [51]

3. Geometry of the full scale beam and position of the drilled specimens (B: beams, C: cores)

4. Phenomenon of fiber balling occurred in HF85 series

5. (a) Comparison of the specimens density; (b) Visual orientation and distribution of fibers in series a) SF65-D, b) SF65-C, c) SF75-D, d) SF75-C, e) HF65-D, f) HF65-C (b)

6. Parameters of the uniaxial tensile behavior recorded from tested dog-bone shaped specimens

7. a) Standard uniaxial tensile tests on cores and dog-bone shaped specimens; b) Standard four-point bending flexural tests on beams cut from the full scale structure

8. Position of sensors at the core position

9. Deformation and temperature of the side and center sensors at the coring

10. a) Compressive strength of cylinder and core specimens at 3, 7 and 28 days; b) Compressive strength at 28 days of different size of specimens and molds types

11. Increase of mechanical strengths as steel fibers are added within the UHPC-A

12. Correlation between measured (Table 3 and Table 3 in [35]) and predicted values of compressive, uniaxial and residual tensile strengths by the extended model (a-f) and the model in [35] (g-l)

13. Correlation between experimental data of a, b, c ([36]), d (UHPFRC-B series) and theoretical results both of the extended model and previous model developed in [35]

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