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Abstract: This work focuses on a DG-SOFC-MGT (downdraft gasifier- solid oxide fuel cell - micro gas turbine) power plant for electrical energy production and investigates two possible performance-upgrading systems: polyphenylene oxide (PPO) membrane and zeolite filters. The first is used to produce oxygen-enriched air used in the reactor, while the latter separates the CO2 content from the syngas. In order to prevent power plant shutdowns during the gasifier reactor scheduled maintenance, the system is equipped with a gas storage tank. The generation unit consists of a SOFC-MGT system characterized by higher electrical efficiency when compared to conventional power production technology (IC engines, ORC and EFGT). Poplar wood chips with 10% of total moisture are used as feedstock. Four different combinations with and without PPO and zeolite filtrations are simulated and discussed. One-year energy and power simulation were used as basis for comparison between all the cases analyzed. The modeling of the gasification reactions gives results consistent with literature about oxygen-enriched processes. Results showed that the highest electrical efficiency obtained is 32.81%. This value is reached by the power plant equipped only with PPO membrane filtration. Contrary to the PPO filtering, zeolite filtration does not increase the SOFC-MGT unit performance while it affects the energy balance with high auxiliary electrical consumption. This solution can be considered valuable only for future work coupling a CO2 sequestration system to the power plant.

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Professor Moh' Ahmad Al-Nimr
Editor-in-Chief
Energy Conversion and Management

Dear Professor Moh' Ahmad Al-Nimr:

I am pleased to submit an original research article entitled **"Effects of upgrading systems on energy conversion efficiency of a gasifier - fuel cell - gas turbine power plant"** by Simone Pedrazzi, Giulio Allesina and Paolo Tartarini for consideration for publication in the *Energy Conversion and Management* journal.

This work focuses on a downdraft gasifier- solid oxide fuel cell - micro gas turbine power plant for electrical energy production and investigates two possible performance-upgrading systems: polyphenylene oxide (PPO) membrane and zeolite filters. The first is used to produce oxygen-enriched air before the reactor, while the latter separates the CO_2 content from the syngas. In order to prevent power plant shutdowns during the gasifier reactor scheduled maintenance, the system is equipped with a gas storage tank. The generation unit consists of a SOFC-MGT system characterized by higher electrical efficiency when compared to conventional power production technology (IC engines, ORC and EFGT). Poplar wood chips with 10 % of total moisture are used as feedstock. Four different combinations with and without PPO and zeolite filtrations are simulated and discussed. One-year energy and power simulation were used as basis for comparison between all the cases analyzed. The modeling of the gasification reactions gives results consistent with literature about oxygen-enriched processes. Results shown that the highest electrical efficiency obtained is 32.81 %. This value is reached by the power plant equipped only with PPO membrane filtration. Contrary to the PPO filtering, zeolite filtration does not increase the SOFC-MGT unit performance while it affects the energy balance with high auxiliary electrical consumption. This solution can be considered valuable only for future work coupling a CO_2 sequestration system to the power plant.

Furthermore, with this letter the authors certify that the content of the paper and its novelty results are the original work of the authors and it was not submitted before in this journal. With this letter all the authors mutually agree to submit their manuscript to Energy Conversion and Management. If you felt that the manuscript is appropriate for your journal, we suggest the following reviewers:

- Prof. S. Dasappa, Faculty, Center for Sustainable Technologies, Indian Institute of Science;
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- Dr. Florian Monlau, APESA, Plateau Technique, France.

We look forward to hearing from you soon.

Best regards,

Dr. Simone Pedrazzi
Dr. Giulio Allesina
Pror. Paolo Tartarini

Highlights

- An advanced gasifier-SOFC-MGT system is modeled.
- An overall electrical efficiency of 32.81% is reached.
- Influence of all the sub-system modeled on the power plant efficiency is discussed.
- Compression storage of syngas is taken into account.

Effects of upgrading systems on energy conversion efficiency of a gasifier - fuel cell - gas turbine power plant

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Abstract

THIS PAPER IS SUBMITTED WITH THE OPTION 'YOUR PAPER YOUR WAY'. FOR THIS REASON LAYOUT AND STYLE MAY DIFFER FROM THE JOURNAL ONE.

This work focuses on a DG-SOFC-MGT (downdraft gasifier- solid oxide fuel cell - micro gas turbine) power plant for electrical energy production and investigates two possible performance-upgrading systems: polyphenylene oxide (PPO) membrane and zeolite filters. The first is used to produce oxygen-enriched air used in the reactor, while the latter separates the CO_2 content from the syngas. In order to prevent power plant shutdowns during the gasifier reactor scheduled maintenance, the system is equipped with a gas storage tank. The generation unit consists of a SOFC-MGT system characterized by higher electrical efficiency when compared to conventional power production technology (IC engines, ORC and EFGT). Poplar wood chips with 10% of total moisture are used as feedstock. Four different combinations with and without PPO and zeolite filtrations are simulated and discussed. One-year

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energy and power simulation were used as basis for comparison between all the cases analyzed. The modeling of the gasification reactions gives results consistent with literature about oxygen-enriched processes. Results showed that the highest electrical efficiency obtained is 32.81%. This value is reached by the power plant equipped only with PPO membrane filtration. Contrary to the PPO filtering, zeolite filtration does not increase the SOFC-MGT unit performance while it affects the energy balance with high auxiliary electrical consumption. This solution can be considered valuable only for future work coupling a CO_2 sequestration system to the power plant.
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1. Introduction

Due to the abundant availability and distribution, biomasses hold key-roles in plans for renewable energy production. This trend is becoming even more relevant thanks to the good degree of reliability and efficiency of the biomass-based technologies together with the high subsidies granted by several government for sustainable electrical energy production [1].

Depending on the feedstock quality and availability, biomasses are converted into energy through different technologies. In the case of ligno-cellulosic biomasses, a technolgy of great validity is gasification. This thermo-chemical process turns solid biomass into a gaseous fuel known as syngas, which can be converted into electrical energy through all those systems used for power production from gaseous fuels [2]. Gasification is today one of the most effi-

cient technologies to convert wood into electricity and it is also sustainable in terms of the environmental balance of CO_2 [3, 4].

Most of the gasification power plants use an IC engine-generator to convert the syngas chemical energy into electrical power. However, in some cases other conversion machines are used, i.e. Organic Rankine Cycles (ORC), External Firing Gas Turbines (EFGT)[5] and Stirling engines are used with the major advantage of having minor limitation about the syngas level of purification [2, 6, 7, 8, 9]. These systems are usually characterized by low conversion efficiencies of about 10-12%. Major conversion rates can be obtained only with electrochemical devices such as proton exchange membrane fuel cells [10], Molten Carbonate Fuel Cells (MCFC) [11, 12], Solid Oxide Fuel Cells (SOFC) [13, 14, 15], systems composed of SOFC and Micro Gas Turbines (MGT) [16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26] and systems composed of SOFC-MGT-ORC [27]. Despite the high rate of energy conversion, these systems require perfectly clean syngas [28]. Downdraft gasifiers are the most suitable architecture due to the low tar and particulate content in their gas when compared to updraft, crossdraft or fluidized bed gasifiers [2, 6, 29]. However, downdraft gasifiers commonly use air as gasification agent. This solution generates a syngas with a low calorific value where the hydrogen, methane and carbon monoxide are diluted in non-burnable gases: N_2 (about 50%) and CO_2 (from 10 to 20%). Otherwise, it is possible to choose oxygen gasification that produces a syngas with negligible N_2 content. However, oxygen gasification is a complex and expensive technology due to the gasification agent supply sub-systems and reactor material choice. Indeed, temperatures inside the reactor can reach 1200-1300 K when oxygen is used instead of air

[30].

The basic system discussed in this study is composed of an air blown-downdraft-fixed bed gasifier fed with poplar wood chips. This work is aimed at investigating the effects of different power plant designs on the overall energy conversion efficiency.

The first power plant upgrading sub-system consists of a polyphenylene oxide (PPO) membrane used to produce oxygen-enriched air. The gas separation characterization of this membrane is reported in literature [31, 32]. In practice, membrane gas separation is applied to increase the oxygen content in the inlet air of biomass boilers [33]. Bisio et al. studied the thermodynamics of combustion with enriched air and reviewed several types of memebranes [34]. Coombe and Nieh developed a membrane-based device for air enrichment in small scale burners [35]. Hao et al. applied an oxygen-permeable membrane to a reactor for the co-production of dimethyl ether (DME)/methanol and electricity [36]. This paper uses PPO membrane in order to obtain air with about 50% of oxygen then used as gasification agent. This solution is a hybrid between air and pure oxygen gasification. Enriched air reduces the reactor thermal stress compared to pure oxygen gasification, while the syngas has a lower N_2 content than the one obtained in pure air gasification. In addition, the syngas flow rate decreases because, for a fixed power output, the enriched air flow required for gasification is lower than air used in conventional gasification. This happens because the same amount of oxygen is used in both cases and its concentration in enriched air is higher than untreated air. Finally, the tar production is lower than air gasification as consequence of the higher temperature that cracks more efficiently the

primary tars from pyrolysis [37].

A second solution discussed in this work consists of a porous media used to upgrade the syngas. In fact, syngas has a variable CO_2 content depending on gasification process as well as several boundary conditions. This value ranges from 10% to 30% and it reduces significantly the higher heating value of the syngas [37]. A solution to overcome this issue is to adopt a pressure-swing selective synthetic zeolite filter. This system is placed before the gas storage in order to separate carbon dioxide from syngas [38, 39]. The filter can be constantly regenerated using a rotary valve packaged into modules as described by Tagliabue et al. [40]. Literature investigation about zeolite filtration outlines several works. Bacsik et al. studied the biogas CO_2-CH_4 separation through zeolites [41]. Kacem et al. investigated the pressure swing adsorption for CO_2/N_2 and CO_2/CH_4 separation using activated carbon and several types of zeolites [42]. Dirar et al. investigated intrinsic adsorption properties of CO2 on 5A and 13X zeolite [43].

The syngas obtained from gasification is stored and then used in a SOFC unit able to produce electrical and thermal energy. The number of stacks within the cell is optimized taking into account the optimal electrical current density. The chosen number guarantees a good efficiency, however the gas discharged from the cell still contains some chemical energy. For this reason, this work suggests to convert this residual energy in a micro gas turbine (MGT). The syngas storage allows the generation unit to operate in its optimal point, furthermore it prevent the power plant shoutting down during the maintenance operations of the gasifier. This management preserves the SOFC and MGT reliability. However, it is difficult to design the stor-

age capacity because an oversize storage rises the systems costs, while an undersized capacity reduces the time gained for the maintenance. For this reason, the storage was designed taking into account the tanks pressure, the electrical power production of the SOFC-MGT unit and the time required for scheduled stops of the gasifier for maintenance operations.

The mathematics of the whole system was developed starting from literature. The overall model has been implemented in Matlab Simulink^{TM} software environment in order to simulate the behavior of the system under different conditions over a year long simulation.

2. System modeling

The basic system layout is reported in Figure 1. The most relevant components are:

- **Downdraft gasifier:** The gasifier is equipped with a subsystem for the syngas filtering and cooling with water scrubber and electrostatic filters.
- **Syngas storage:** It consists of a tank of a total volume of 650 m^3.
- **SOFC unit:** This subsystem consists of 10875 solid oxide cells and it is connected to the electrical grid by a power inverter.
- **Micro gas turbine (MGT):** this turbo-machinery is used to convert the last part of chemical energy content in the syngas purged by the SOFC.

This work investigates the effect of the implementation of the following sub-systems to the basic scheme:

- **PPO membrane filter module:** The PPO sub-system consists of the membrane filter and a compressor that increases the pressure of the air before the PPO membrane filter to about 1 MPa. The oxygen enriched air is sent to the gasifier at atmospheric pressure. A flow of nitrogen is purged from the PPO module.

- **Zeolite (ZEO) filter module:** the zeolite (ZEO) filter module is placed after the first syngas compressor. There is a further syngas compression stage ahead the storage tanks because the ZEO module works at 0.5 MPa of pressure as described in Section 2.3, while the pressure in the storage is often higher.

The syngas is used as fuel in the SOFC stack. In this device, the fuel reforming occurs at the anode and there is a recirculation of the 20% of the anode exhaust to increase the fuel reforming performance [18, 22]. The anode exhaust is used to preheat the syngas, then it is finally burned in the MGT burner together with the cathode exhaust. The air required for the electrochemical reaction is compressed and preheated in the recuperator of the MGT as well as in the air preheater of the SOFC.

The SOFC stack generates DC current which is converted into AC current by an inverter and it is sent to the electrical grid. The MGT drags the air compressor and the remaining mechanical energy is converted into electrical energy by an alternator.

2.1. PPO module modeling

Polymeric membranes allow to separate different gaseous components depending on the pore size and pressure applied to the filter [31]. In this work a membrane is used to separate nitrogen from air. The membranes widely used for this purpose are: Matrimid, Polyphenylenoxide (PPO) and Polydimethylsiloxan (PDMS) [31]. As showed in Figure 2, in membranes the inlet air flow is divided in permeate and retentate molar flows. The inlet flow (Q_{air} [mol/s]) has a pressure p_{feed} [atm] and it is composed of x_{O_2Feed} and x_{N_2Feed} molar fractions of oxygen and nitrogen. The permeate molar flow (Q_P [mol/s]) has a pressure $p_{permeate}$ [atm] and it is composed of y_{O_2} and y_{N_2} molar fractions of oxygen and nitrogen. The retentate molar flow (Q_R [mol/s]) has a pressure p_{feed} [atm] and it is composed of $x_{O_2Retentate}$ and $x_{N_2Retentate}$ molar fractions of oxygen and nitrogen.

Each membrane behavior is identified through two parameters: the selectivity (α) and the permeability to oxygen (γ). The first factor represents the attitude of the membrane to attract oxygen, the second quantifies the attitude of the membrane to be crossed by it. High selectivity and permeability ensure great filtering performance in terms of high value of y_{O2} and a small membrane surface area is required to filter a given amount of air. Table 1 presents the parameters of Matrimid, PPO and PDSM membranes.

The choice of a PPO membrane is a compromise in terms of acceptable values of selectivity and permeability. In order to simulate the behavior of the membranes, a mathematical model has been implemented from Melin and Rautenbach [31]. The model is based on the following assumptions:

- Air is considered a binary gas mixture with 21% oxygen and 79% ni-

trogen.

- Steady state conditions.
- Isotherm conditions.
- Isobaric conditions.
- Perfect gas law.
- Constant permeability.
- Perfect mixing conditions on upstream and downstream sides.
- Concentration polarization at the membrane is neglected.
- Pressure loss in the porous support layer is neglected.
- The permeate can drain off freely.

The calculation of the permeate composition is made with the following formula taken from the work of Melin and Rautenbach [31]:

$$y_{O_2} = \frac{1}{2}\left[1 + \phi * \left(x_{O_2Feed} + \frac{1}{\alpha - 1}\right)\right] - \sqrt{\left[\frac{1}{2}\left[1 + \phi * \left(x_{O_2Feed} + \frac{1}{\alpha - 1}\right)\right]\right]^2 - \frac{\alpha * \phi * x_{O_2Feed}}{\alpha - 1}} \tag{1}$$

$$y_{N_2} = 1 - y_{O_2} \tag{2}$$

where ϕ [-] is the feed-permeate pressure ratio given by the following equation:

$$\phi = p_{feed}/p_{permeate} \tag{3}$$

Figure 3 reports the permeate composition over pressure ratio for the three membrane types considered. It can be seen that only a certain maximum of oxygen ratio can be achieved because all the graphs are leveling off. Therefore a pressure ratio of 1 MPa was chosen for further calculations as suggested in Melin and Rautenbach [31] and the $p_{retentate}$ was fixed at 1 atm.

The Matrimid membrane is able to produce the highest oxygen ratio of 0.58 % vol. in the permeate, however PPO membrane presents a good value of oxygen ratio (0.49 % vol.) and an acceptable value of permeability, therefore this membrane is adopted in the simulations. The active area of the membrane can be assessed from the molar flow of oxygen required for the gasification Q_{PO_2} [mol/s]:

$$A_{membrane} = \frac{Q_{PO_2}}{\gamma * (x_{O_2Feed} * p_{feed} + y_{O_2} * p_{permeate})} \tag{4}$$

The molar flow of nitrogen Q_{PN_2} [mol/s] and the total permeate molar flow Q_P [mol/s] is given by the following equations:

$$Q_{PN_2} = \frac{\gamma}{\alpha} * [p_{feed} * (1 - x_{O_2Feed}) + p_{permeate} * (1 - y_{O_2})] \tag{5}$$

$$Q_P = Q_{PN_2} + Q_{PO_2} \tag{6}$$

The molar flow of the inlet air Q_{air}, the retentate molar flow Q_R and the retentate composition ($x_{O_2Retentate}$ and $x_{N_2Retentate}$) are calculated setting to zero the amount of oxygen in the retentate flow as suggested by Melin and

Rautenbach[31]. Thus, a mass balance equation can be applied to estimate Q_{air} and Q_R:

$$Q_{air} * x_{O_2Feed} = Q_P * y_{O_2} \rightarrow Q_{air} = \frac{Q_P * y_{O_2}}{x_{O_2Feed}} \tag{7}$$

$$Q_{air} = Q_P + Q_R \rightarrow Q_R = Q_{air} - Q_P \tag{8}$$

Finally, the electrical power consumption to pressurize the inlet air flow is calculated as a polytropic compression by Equation 15 assuming $T_{in} = 20$ ^{o} C; $m = 1.2$ and $\eta_{comp} = 90$ %.

2.2. Gasifier modeling

In this work, the gasification process is simulated using a black-box model based on Barman's work [44]. The model is validated for downdraft gasifiers; it is based on the following gasification equation:

$$\begin{aligned} CH_xO_yN_z + wH_2O + m\left(O_2 + 3.76N_2\right) \rightarrow \\ n_{H_2}H_2 + n_{CO}CO + n_{CO_2}CO_2 + n_{H_2O}H_2O \\ +n_{CH_4}CH_4 + \left(z/2 + 3.76m\right)N_2 + n_{tar}CH_pO_q \end{aligned} \tag{9}$$

where $CH_xO_yN_z$ is the equivalent chemical formula of "dry and ash free" (daf) biomass; CH_pO_q is the equivalent chemical formula of tar [45]; w $[mol/mol_{bio}]$ is the specific molar amount of the biomass moisture; m $[mol/mol_{bio}]$ is the specific molar amount of oxygen calculated starting from the equivalence ratio ER as suggested by Jarungthammachote and Dutta[46]; $n_{H_2}, n_{CO}, n_{CO_2}, n_{H_2O}, n_{CH_4}$, n_{tar} $[mol/mol_{bio}]$ are the specific molar amounts of $H_2, CO, CO_2, H_2O, CH_4$ and tar which constitute the syngas.

This model is used and discussed in several other works [47, 48, 49]. It consists of a chemical and a thermal sub-models that converge to the final composition of the gas. The first step is to choose an initial temperature T [K] and calculate the equilibrium constant of the following reactions:

- **K1:** Water-gas shift $CO + H_2O \leftrightarrow CO_2 + H_2$
- **K2:** Hydrogasification $C + 2H_2 \leftrightarrow CH_4$
- **K3:** Methane steam reforming $CH_4 + H_2O \leftrightarrow CO + 3H_2$

The system of equations 10 reported below is composed of three chemical balances calculated from Equation 9 (carbon, hydrogen and oxygen) and the three equilibrium constants for water-gas, hydrogasification and methane reforming reactions. The system is solved with the Newton-Raphson method.

$$\begin{cases} n_{CO} + n_{CO_2} + n_{CH_4} + n_{tar} - 1 = 0 \\ 2n_{H_2} + 2n_{H_2O} + 4n_{CH_4} + pn_{tar} - x - 2w = 0 \\ n_{CO} + 2n_{CO_2} + n_{H_2O} + qn_{tar} - w - 2m - y = 0 \\ K_1 = \frac{n_{CO_2} * n_{H_2}}{n_{CO} * n_{H_2O}} \\ K_2 = \frac{n_{CH_4} * \frac{\dot{n}_{tot,wet}}{\dot{n}_{bio,daf}}}{n_{H_2}^2} \\ K_3 = \frac{n_{CO} * n_{H_2}^3}{\left(\frac{\dot{n}_{tot,wet}}{\dot{n}_{bio,daf}}\right)^2 n_{H_2O} n_{CH_4}} \end{cases} \tag{10}$$

Once the molar specific amounts of the syngas species are evaluated, it is possible to solve the thermodynamic energy balance of the system reported in the following equation:

$$\sum_{j=react} n_j * HF_j^0 = \sum_{i=prod} n_i * \left(HF_i^0 + \Delta H_{T,i}\right) \tag{11}$$

where n_j [moles] and HF_j^0 [kJ/kmol] are the specific moles amount and standard heat of formation of the j-th reagent (biomass, air and moisture); n_i [moles] and HF_i^0 [kJ/kmol] are the specific moles amount and the standard heat of formation of the i-th product (H_2, CO, CO_2, H_2O ,CH_4 and N_2) and $\Delta H_{T,i}$ is the enthalpy difference between any given state and the standard state for the i-th product. $\Delta H_{T,i}$ can be calculated starting from the specific heat of the product:

$$\Delta H_{T,i} = \int_{298.15}^{T} C_p(T)\, dT = \left| aT + b\frac{T^2}{2} + c\frac{T^3}{3} + d\frac{T^4}{4} \right|_{298.15}^{T} \tag{12}$$

where the coefficient a,b,c and d are defined for each gas by Jarungthammachote and Dutta[46]. In order to find the equilibrium temperature T_{new}, the system is considered adiabatic and the the Newton-Raphson method is applied to the equations. If $abs(T - T_{new}) < 0.1$ K then the calculated equilibrium temperature and molar specific gases amounts are the final results; otherwise, a new iteration is done in order to satisfy the previous condition. The model is implemented in Python and the input are the biomass equivalent molecule, the equivalence ratio ER and the initial temperature. The temperature input is used only as a starting point for the iterating system; after few cycles the temperature converges to the ones that satisfy both the chemical and thermal sub-systems. About the ER, a value of 0.335

is assumed. This value is consistent with air blown gasification parameters [50, 37] and it is confirmed by the low tar content in the syngas. Poplar wood chips properties and gasifier model parameters are summarized in Table 1.

2.3. ZEO module modeling

The zeolite filter is able to reduce the total syngas molar flow of about 20% - 30 % by the adsorption of CO_2. Zeolite 5A is chosen because it has a great selectivity for carbon dioxide in comparison with the other gases that constitute syngas [38]. The gas adsorption in porous solids has been described by the Langmuir equation [38, 39]:

$$q_i = \frac{q_{mi} * B_i * p_i}{1 + \sum_{j=1}^{n} B_j * p_j} \tag{13}$$

where q_i [mmol/g] is the adsorbed amount of the component i; q_{mi} [mmol/g] is the saturation adsorbed amount of the component i; B_i [1/kPa] is the Langmuir constant of the component i; p_i [kPa] is the equilibrium partial pressure of the component i; B_j [1/kPa] is the Langmuir constant of the component j; p_j [kPa] is the equilibrium partial pressure of the component j; i and j are the gas species of the syngas. Table 1 reports the Langmuir constants and the saturation adsorbed amounts for Zeolite 5A, while Figure 4 depicts the adsorption trends of the syngas gases as function of pressure. It can be noted the high CO_2 selectivity of the zeolite in comparison with others gases.

The mass of zeolite required for adsorbing all the carbon dioxide of the syngas depends on the molar flow of the dry syngas, its CO_2 molar fraction and kinetic constant of adsorption. The ZEO filter module can be constantly regenerated using a rotary valve packaged into modules as described in [40].

The mass of zeolite that needs to be regenerated every cycle with duration of t_{cycle} can be calculated as follows:

$$m_{zeo} = t_{cycle} * \dot{n}_{DG} * \frac{1 + \sum_{j=1}^{n} B_j * p_j}{q_{m,CO_2} * B_{CO_2} * p_{ads} * x_{CO_2}} \tag{14}$$

where p_{ads} [kPa] is the total pressure of the syngas inside the ZEO filter. A constant temperature of the zeolite filter and of the inlet syngas of 303 K is assumed and the pressure of the inlet syngas is set to 500 kPa as suggested in [38, 39]. The cycling time of regeneration depends on kinetic CO_2 adsorption constant. In this study a plausible time of 60 seconds is assumed and future work will investigate this aspect. Zeolites adsorption generates heat, Ranjani et al. [51] suggests that 64-70 kJ are released for every mole of CO_2 adsorbed. This heat needs to be discharge by the ZEO module in order to keep the temperature constant at 303 K. In this preliminary study, no attention was paid to the ZEO module heat balance. Furthermore, the gas filtering subsystem considered in this work is based on the power plant described by Allesina et al. [50]. It was designed with the idea of coupling the gasifier with an internal combustion engine. Since the minimum presence of tars could negatively affect the performance of the zeolite adsorber, syngas purification unit should be properly designed. A potential alternative to water scrubber is oil scrubber with subsequent stripping of tars [52, 53].

2.4. Compressor and storage system modeling

The modeling of the syngas compression is carried out considering it as a polytropic transformation. The electrical power required for compression is given by Pedrazzi et al. [54]:

$$P_{comp} = \frac{\dot{n}_{gas} L_{comp,is}}{\eta_{comp}} = \frac{\dot{n}_{gas}}{\eta_{comp}} \frac{zRT_{in}}{z-1} \left[1 - \left(\frac{p_{out}}{p_{in}} \right)^{\frac{z-1}{z}} \right] \tag{15}$$

where z is the polytrophic coefficient, R is the universal gas constant equal to 8.314 J mol^{-1} K^{-1}, T_{in} is the gas inlet temperature (25°C for syngas compressor 1 and 30°C for syngas compressor 2), p_{in} and p_{out} [atm] are the gas inlet and outlet pressures, $\dot{n}_{gas}$ [mol/s] is the gas molar flow and η_{comp} is the compressor efficiency available from manufacturer's data [54]. The maximum pressure value inside the storage system is a fundamental parameter required todesign the tanks and the compressor properly. Assuming ideal gas and a constant syngas storage temperature $T_s = 25$ ^{o}C, the pressure inside the tanks is calculated by the ideal gas law:

$$p_s = \frac{nRT_s}{V} \tag{16}$$

where n [mol] are the moles of syngas inside the tanks and V [m^3] is the storage total volume. Assuming a value of the initial syngas moles n_{in} inside the storage, the moles of syngas at the time τ [s] are given by:

$$n = n_{in} + \int_0^{\tau} \left(\dot{n}_{in,s}(t) - \dot{n}_{out,s}(s) \right) dt \tag{17}$$

where $\dot{n}_{in,s}(t)$ and $\dot{n}_{out,s}(t)$ [mol/s] are the inlet and the outlet molar flow at the instantaneous time t [s]. Table 2 reports the model parameters of the storage and compressor sub-systems. The total volume of storage and the initial syngas amount in the tank are reduced of about 50% in comparison with the conventional system without PPO and ZEO modules as investigated in [55, 56]. This result is reached thanks to the PPO adoption that decreases

the molar flow of dry syngas of about the 20% - 30%, while the filtration in the ZEO module further reduces the syngas molar flow of about another 20% - 30% as shown in the results.

2.5. SOFC modeling

The SOFC model used in this study is based on the work of Bang-Møller and Rokni [18]. This model does not take into account the recirculation of gas at the cell anode. This feature may strongly compromise the fuel cell efficiency in case of the presence of gases that do not take part in the electro-chemical, shift and reforming reactions. Unfortunately, syngas contains considerable amounts of CO_2 and N_2. To overcome this issue, the model previously cited is implemented with the reforming model presented by Rami Salah El-Emam et al. [22]. As described by Rami Salah El-Emam, the electro-chemical reactions take place in both the anode and the cathode of the cell (Eq.22), while the reforming and the monoxide water shift occur only near the anode (Eqs. 18, 19). Equation 22 presents the overall electro-chemical reaction that is divided into two sub-reactions: the hydrogen reacts with the oxygen ions to form water and electrons according to Eq. 20 at the anode, while, at the cathode, the oxygen from inlet air reacts with the electrons from the anode (Eq. 21) to form oxygen ions that flow to the anode through the solid oxide electrolyte.

$$CH_4 + H_2O \rightarrow CO + 3H_2 \tag{18}$$

$$CO + H_2O \rightarrow CO_2 + H_2 \tag{19}$$

$$H_2 + O^{2-} \rightarrow H_2O + 2e^- \tag{20}$$

$$\frac{1}{2}O_2 + 2e^- \rightarrow O^{2-} \tag{21}$$

$$H_2 + \frac{1}{2}O_2 \rightarrow H_2O \tag{22}$$

The mathematical modeling of reforming and electrochemical reactions is explained in References [22] and [18]. Using these models, it is possible to calculate the electrical power production and the electrical conversion efficiency for a given syngas inlet flow with a specific composition. The SOFC model parameters adopted in the simulations are reported in Table 2.

2.6. MGT modeling

Mathematical description of gas turbines is well described in literature. Details and assumptions of the present model can be found in Bang-Møller and Rokni work [18]. Characteristics of the turbine and others components connected to the MGT are listed in Table 2.

3. Simulation results and discussion

In this work four different cases are simulated. First of all, the basic system composed of a downdraft gasifier, a storage tank and a SOFC-MGT is simulated. After this step, the two possible solutions consisting of N_2 purging from air or CO_2 separation from syngas are discussed separately. Finally, the complete system provided with PPO module and ZEO module is simulated.

3.1. Case I (Gasifier + SOFC + MGT)

The SOFC-MGT unit constantly produces energy all over the year of simulation in order to preserve the stability of the cells and their gaskets, which are very sensitive to thermal stresses [57]. The syngas molar flow consumed by the SOFC-MGT unit is calculated by Equation 23 that considers the cycling working of the DG:

$$\dot{n}_{syngas-SOFC} = \frac{h_{operation}\dot{n}_{DG}}{h_{operation} + h_{maintenance}} \tag{23}$$

Figure 5 depicts the overall model implemented in Matlab Simulink^{TM} software environment. Table 3 reports the simulation results. Gasifier cold efficiency is about 79%, this value is confirmed by literature that suggests an efficiency of 70% - 80% for air-blown downdraft gasifier [37, 4, 44]. Syngas composition consists of about 19% vol. of H_2 and 15% vol. of CO, the higher heating value of 4.75 MJ/Nm^3 is similar to the results reported by Basu [37] for this kind of gasifier. SOFC-MGT unit has a constant electrical power production of 197.43 kW all over the simulated year. The auxiliary consumption of the whole system strongly depends on tank pressurization level. The average annual value is 34.24 kW. For this reason, the net average power production is reduced to 163.19 kW and the electrical efficiency of the system is 25.43%.

3.2. Case II (PPO + Gasifier + SOFC + MGT)

Table 4 shows the results of the simulation of the system previously described and now equipped with the PPO module. The oxygen enriched air

flow is about 1.27 mol/s. This value is lower than 2.94 mol/s obtained without PPO membrane (Case I). Syngas composition is consistent with the work of Wang et al. [58], where oxygen-enriched air (50% oxygen and 50% nitrogen) is used as gasifying agent in a double stage downdraft gasifier fueled with pine sawdust pellets. Differences of 1-2% between the model outputs and Wang's results about CO and H_2 contents are achieved (29% vs. 27% for H_2 and 26% Vs. 25% for CO). The gasification with oxygen-enriched air assures high gasifier performance in terms of cold gas efficiency (92%), tar production (0.27 g/Nm^3) and syngas higher heating value (7.55 MJ/Nm^3). The syngas outlet flow is 3.589 mol/s, consistently lower than Case I where syngas flow is 5.01 mol/s. The average equilibrium temperature of gasification in this case is 931 K. This value is only 36 K higher than Case I. Wang et al.[58] suggestes a peak temperature of about 1200 K with oxygen-enriched air. With this temperature, conventional material adopted in air gasifier can be used (i.e. stainless steel and refractory brick [2, 6]). In Case II, the overall net power production is 210.52 kW and the electrical efficiency is boosted to 32.81%. The average auxiliary consumption is 42 kW, 8 kW higher than Case I. This is due to the PPO module that uses air at 1 MPa pressure generated by an air compressor. The electrical consumption of the air compressor is 15.3 kW and it is fully compensated by the increasing of the gasifier efficiency and the SOFC-MGT unit efficiency.

3.3. Case III (Gasifier + ZEO + SOFC + MGT)

Table 5 resumes the simulation results of the system with the ZEO filtering module instead of PPO membrane. The filtered syngas has a higher heating value of 5.9 MJ/Nm^3. This value falls between Case I (4.75 MJ/Nm^3)

and Case II (7.55 MJ/Nm^3). The pressure of the storage tank ranges between 0.267-0.488 MPa, similar to the values obtained in Case II (0.266-0.462 MPa) and Case I (0.267-0.539 MPa). The zeolite mass required to perform continuosly the filtration is 23.742 kg. The value obtained is consistent with Tagliabue et al. work [40]. However, in future work, the CO_2 adsorbed by the ZEO module can be stored in order to create a carbon sequestration system. The power production and the net electrical efficiency of the system is low (148.74 kW of power production and 22.87% of electrical efficiency) as a consequence of the energy absorbed by the syngas compressor 1 (see Figure 1) to increase the pressure of the syngas to 0.5 MPa before the ZEO module. This electrical energy consumption is higher than Cases II and I, in addition the efficiency of the SOFC-MGT module fueled with the filtered syngas is lower. As shown in Table 5, the SOFC-MGT efficiency in Case III is about 34%, thus lower than Case II (42.08%) and Case I (37.46%).

3.4. Case IV (PPO + Gasifier + ZEO + SOFC + MGT)

The results about the fully equipped gasifier power system are reported in Table 6. A high power production (194.53 kW) and electrical efficiency (30.32%) is reached thanks to the high H_2 and CO amounts in the filtered syngas. In fact, the H_2 volume percentange reaches 41.53% and the CO volume percentange is boosted to 32.54%. As a consequence of this composition, the higher heating value of the syngas is 10.19 MJ/Nm^3, a value typical for oxygen-blown gasifiers [37]. Therefore, the SOFC-MGT unit syngas consumption is 2.696 mol/s. This value is about 45% lower than Case I (4.95 mol/s), 24% lower than Case II (3.545 mol/s) and 33% lower than Case III (4.02 mol/s). A pressure range of 0.266-0.415 MPa is achieved. In this

case power production and efficiency is lower than Case II as result of higher average auxiliary consumption (51.80 kW) and lower SOFC-MGT unit efficiency (38.41%). However, the utilization of the ZEO module has several advantages: separates the CO_2 and reduces the storage peaks pressure.

3.5. Performance and energy considerations

Figure 6 shows the electrical efficiency and the average power production in every scenario. Case II resulted the best in terms of energy conversion; the overall electrical efficiency reaches 32% and the power production is about 210 kW. These values are higher than commercial gasification power systems with internal combustion engines where the maximum electrical efficiency hardly reaches 25% [37, 4, 2]. This result is given by the PPO module that increases the gasifier efficiency to 92% (75% is the reference value for air blown gasifier [37]) and the SOFC-MGT module which has a higher electrical conversion efficiency (about 42%) compared to common engine-alternator generator units (about 27% [4, 59, 3]). Case II is the best in terms of energy balance as shown in Figure 7. These graphs do not consider the thermal energy that can be recovered from the gasifier or the SOFC-MGT unit. The highest energy loss occurs at the SOFC-MGT unit (about 52%), while auxiliary consumption of the blowers and the auxiliary equipment of the gasifier are low (9%). In Cases I and III, the low efficiency of the gasifier reduces the overall electrical performance of the system. In Cases III and IV the ZEO module consumes energy to separate the CO_2 from the gas, however no efficiency increase occours in the SOFC-MGT unit with a CO_2 free syngas and the final result is a lower power production. The system modeled in this work is obtained starting from a reference power plant described by Allesina et. al

[50] where IC engines are used instead of the SOFC-MGT unit. The author reports an experimental cold gasification efficiency of 67%. Considering an electrical IC engine-alternator unit efficiency of about 27%, as suggested by Puglia at al. [3], the total electrical efficiency is about 18%. This value is 30% lower than Case I and it is 45% lower than Case II. Another study made by Patuzzi et al. [60] reports the values of the net electrical efficiency of three different commercial biomass gasifier - IC engine power plants. The average efficiency is about 20%, this value is consistent with the one obtained for Allesina et al. [50].

4. Conclusions

The biomass fueled system with PPO module (Case II) shows the higher electrical efficiency of about 33%. The reasons behind this result are various. First of all, oxygen-enriched air boosts the gasifier cold efficiency from 79% (Case I with air) to 92% (Cases II and IV with oxygen-enriched air). In addition, the SOFC-MGT unit presents a higher efficiency (about 42%) compared to IC engine-alternator unit (about 27%), ORC cycle (about 20%) or EFGT cycle (about 20%). In Cases III and IV, the zeolites adsoption module consumes energy to increases the higher heating value of the syngas but not the performance of the SOFC-MGT system, this reduces the overall system efficiency. The energy balances of four cases investigated show that the greater losses are in the SOFC-MGT unit. This unit has the difficult task to convert the chemical energy of a gas fuel into electrical energy in an efficient way. An efficiency of about 50% is reached with natural gas, in this study the maximum electrical efficiency is about 42% using a syngas

produced with an oxygen-enriched air as gasifying agent. This difference is given by the presence of several inert gases into the syngas that reduces the electrochemical conversion of the SOFC. The removal or the conversion of these gases into syntethic natural gases (SNG) is possible and, in this way, the efficiency of the SOFC-MGT unit will be similar to the value reach for natural gas one. But, cost and energy self-consumption of the upgrading process are very high and not convenient for this kind of power plants. Cases III and IV has a lower efficiency compared to Case II, however, with the ZEO module, it is possible to seperate the CO_2 content of the syngas with environmental benefits in case the module is coupled with a CO_2 sequestration system. Future work will consider exergy calculations and experimental tests on a micro-scale power system (5-20 kW of electrical power) with PPO module and SOFC module in order to validate modeling results and to assest system durability. In addition, economical net present value analysis will be done to estimate the economic sustainability of the power plant.

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modeling of energy conversion effectiveness in a gasification power plant. *International Journal of Heat and Technology*, 30(1):41–44, 2012.

Figure captions and tables

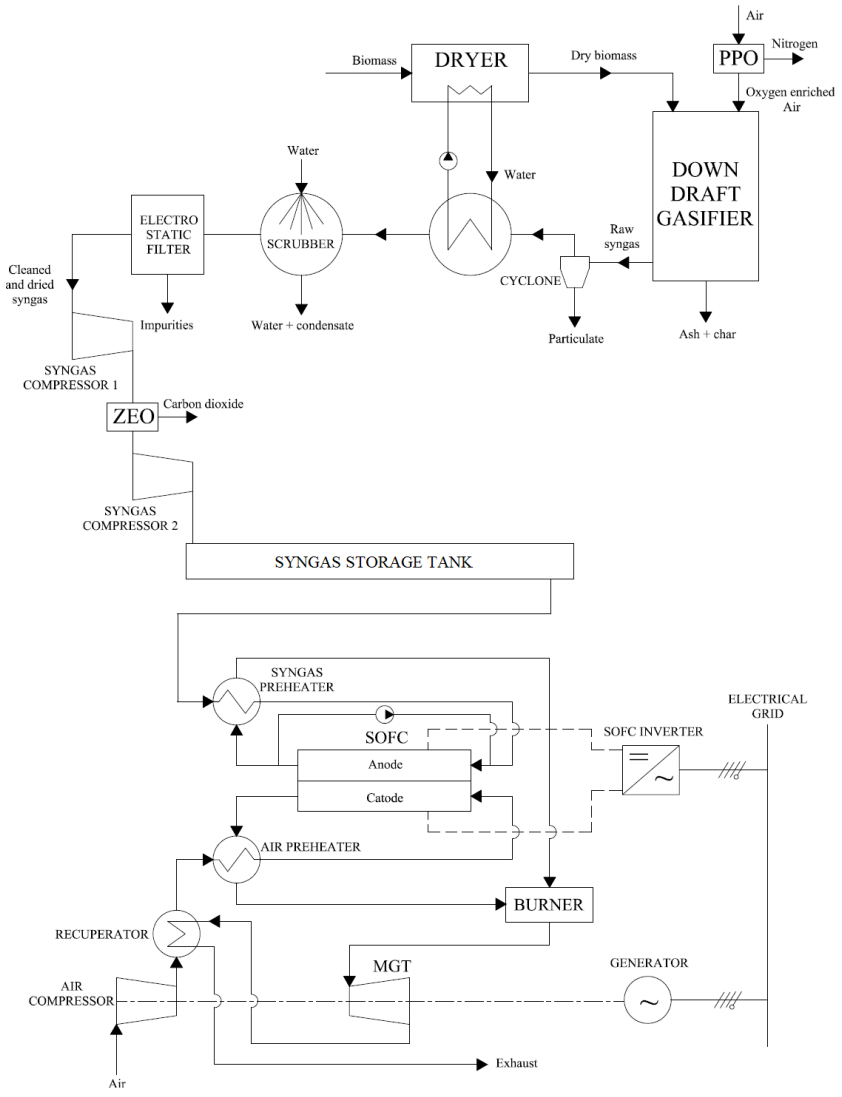

Figure 1: DG-SOFC-MGT hybrid system with zeolite CO_2 adsorption and oxygen-enriched air layout

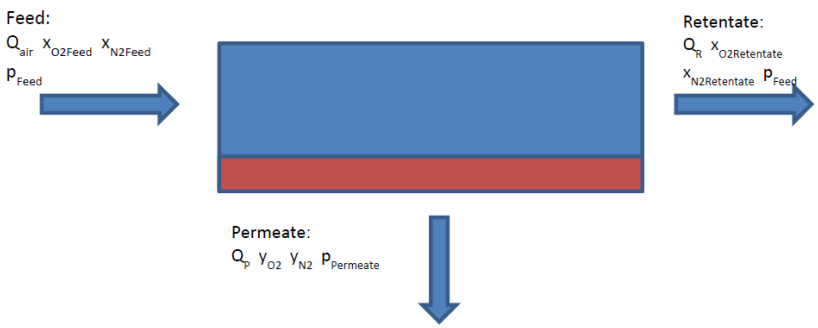

Figure 2: Oxygen enriched air membrane separator principle

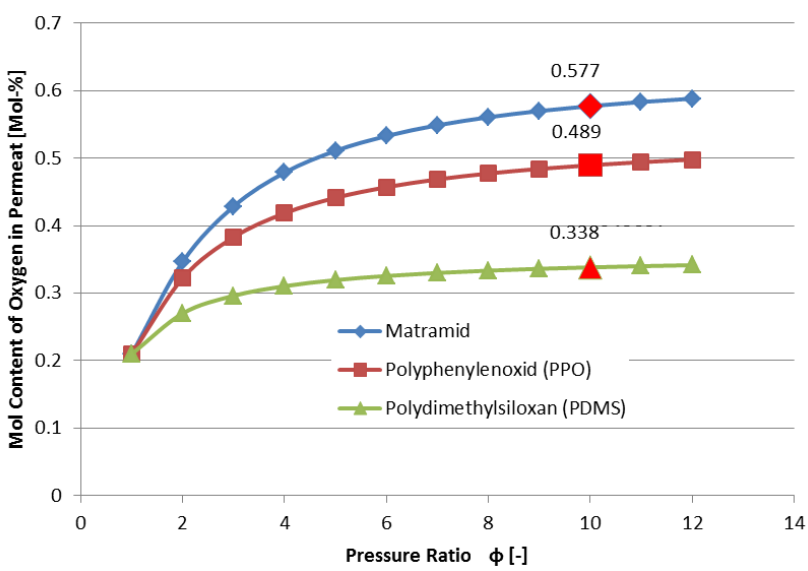

Figure 3: Characteristics of the separation membranes

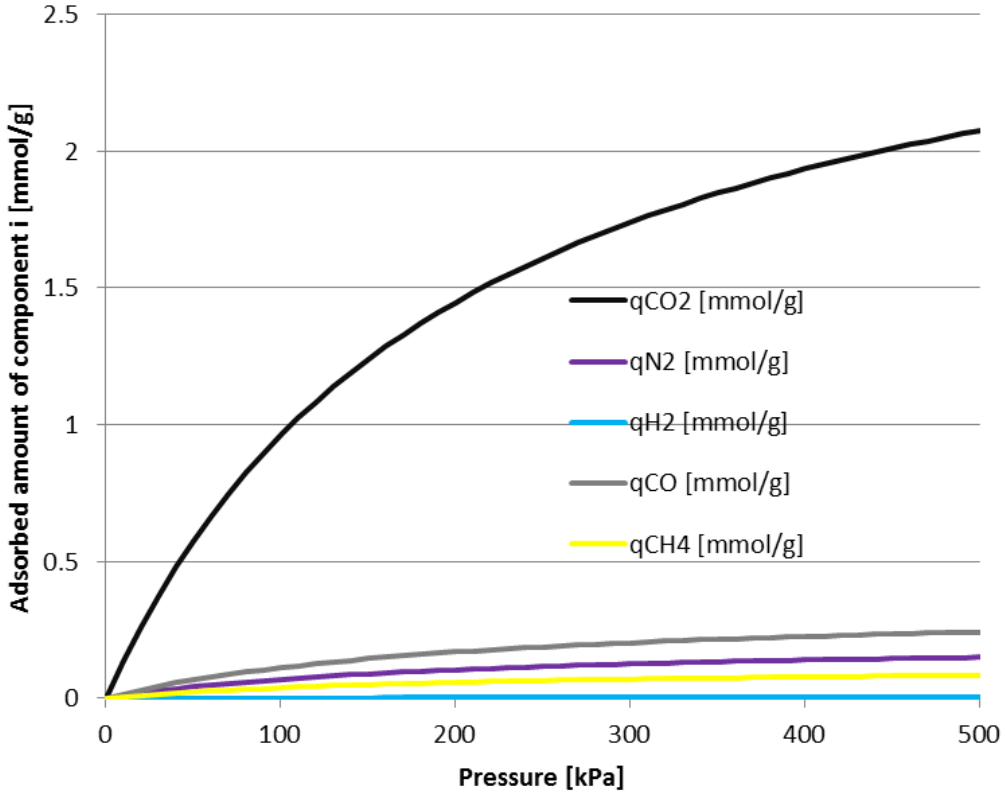

Figure 4: Zeolite 5A adsorbing curve Vs. pressure

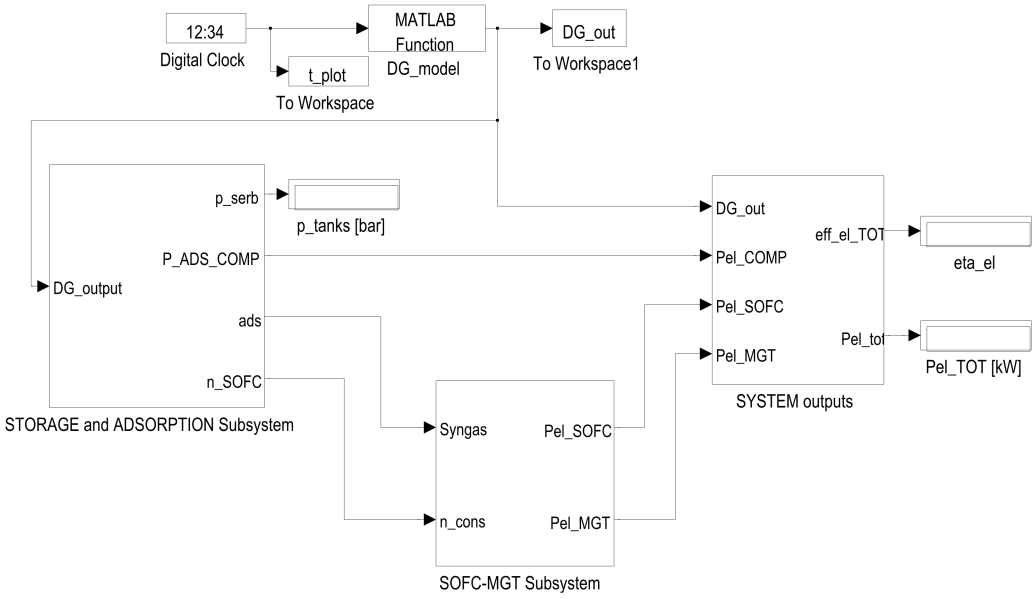

Figure 5: DG-SOFC-MGT hybrid system with zeolite CO_2 adsorption and oxygen-enriched air implemented in Matlab Simulink^{TM}

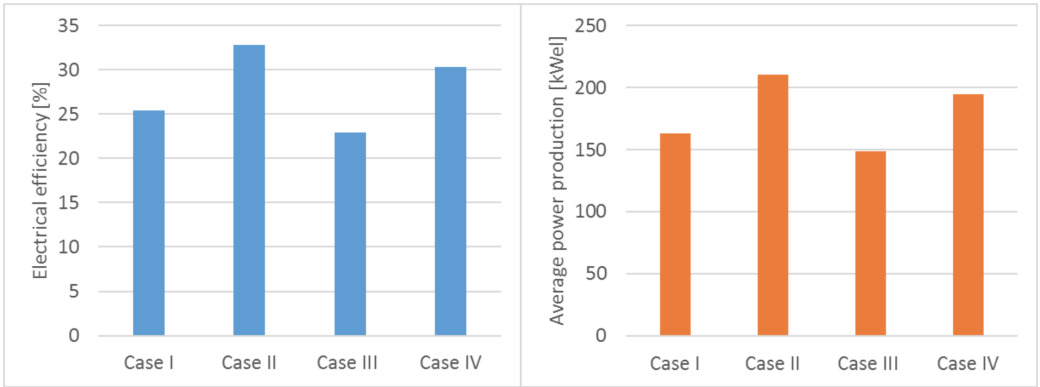

Figure 6: Efficiencies and eletrical production values of the studied cases

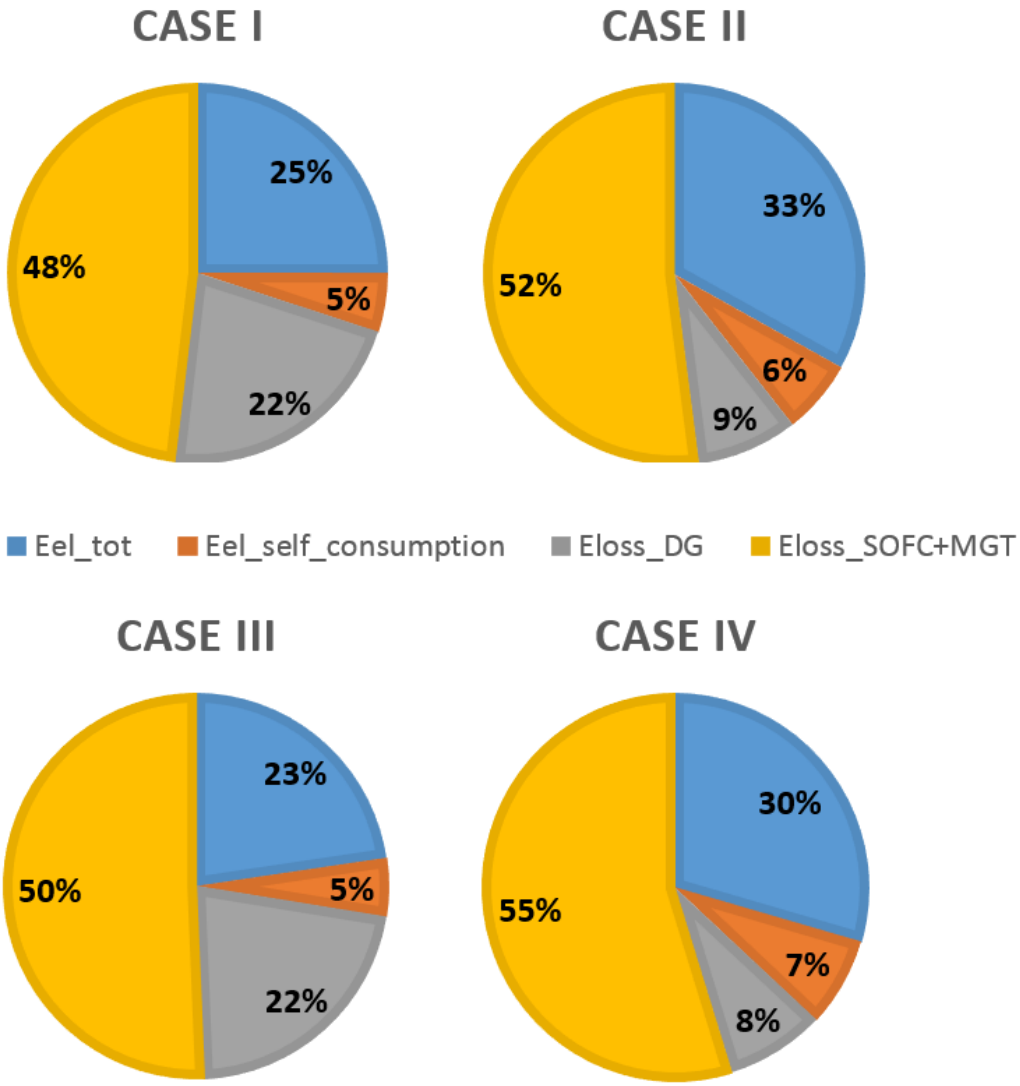

Figure 7: Energy balances of the studied cases

Table 1: Model parameters I

Membranes properties [31]		
Material	Selectivity	Oxigen Permeability
	α [ad]	γ [mol m^{-2} s^{-1} bar^{-1}]
Matrimid	6.7	62.0 x 10^{-5}
PPO	4.7	37.2 x 10^{-4}
PDMS	2.1	39.6 x 10^{-2}
Poplar wood chips properties [61]		
Description	Symbol	Value
Total moisture	M	10 %
Carbon content (as received)	C_{ar}	41.62 %
Hydrogen content (as received)	H_{ar}	5.30 %
Nitrogen content (as received)	N_{ar}	0.52 %
Oxygen content (as received)	O_{ar}	39.81 %
Ash content	ASH	2.75 %
Higher heating value (dry basis)	HHV_{db}	15.7 MJ/kg
Gasifier model parameters[48]		
Description	Symbol	Value
As received biomass consumption	$\dot{m}_{bio}$	187 kg/h
Nominal gasifier thermal power	$P_{th,gas}$	800 kW
Initial calculation temperature	T_{in}	900 K
Pressure	p	1 atm
Equivalence ratio	ER	0.335
Gasifier and filters auxiliary consumption	$P_{DG,self}$	12.5 kW
Cyclic operation hours	$h_{operation}$	360 h
Cyclic maintenance hours	$h_{maintenance}$	4 h
Zeolite 5A parameters of adsorption at 303 K [39]		
Component	B [1/kPa]	q_m [mmol/g]
CO_2	0.019500	3.91900
H_2	0.000361	0.54464
N_2	0.000837	2.62543
CH_4	0.002535	2.75403
CO	0.004350	2.75800

Table 2: Model parameters II

Storage and compressor model parameters		
Description	Symbol	Value
Politropic exponent of the syngas [54]	m	1.33
Syngas compressor efficiency [54]	η_{comp}	92 %
Storage tank temperature	T_s	298.15 K
Initial syngas amount in the tanks	n_{in}	$7 * 10^4$ mol
Total tanks volume	V	650 m^3
SOFC model parameters		
Description	Symbol	Value
Fuel utilization factor	U_f	0.85
Recirculation factor	r	0.2
Operating temperature	T_{sofc}	1073.15 K
Anode pressure loss	Δp_a	500 Pa
Cathode pressure loss	Δp_c	1000 Pa
Anode pressure loss	Δp_a	500 Pa
Current density	i	300 mA/cm^2
Active cell area	A_{cell}	81 cm^2
Cells for each stack	$n_{cell,stack}$	75 cells
Number of stacks	n_{stack}	145 stacks
Cathode air excess	$vent$	1.15
Pressure ratio	PR	2.5
Steam to carbon coefficient	STC	1.4
Electrochemical parameters taken from [18]		
MGT model parameters [18]		
Description	Symbol	Value
Politropic exponenet of the air	m	1.33
Turbine isoentropic efficiency	$\eta_{is,turb}$	84 %
Air compressor isoentropic efficiency	$\eta_{is,comp}$	75 %
Turbine mechanical efficiency	$\eta_{mec,turb}$	99 %
Air compressor mechanical efficiency	$\eta_{mec,comp}$	98 %
Recuperator effectiveness	η_{rec}	85 %
Burner efficiency	$\eta_{eff,burner}$	99 %
MGT generator efficiency	$\eta_{alt,MGT}$	95 %
Pressure ratio	PR	2.5

Table 3: Case I (Gasifier + SOFC + MGT) simulation results

Gasifier		
Description	Symbol	Value
H_2 syngas fraction	x_{H_2}	19.03 %
H_2O syngas fraction	x_{H_2O}	7.78 %
CO syngas fraction	x_{CO}	15.10 %
CH_4 syngas fraction	x_{CH_4}	1.18 %
CO_2 syngas fraction	x_{CO_2}	13.99 %
N_2 syngas fraction	x_{N_2}	42.92 %
Air inlet flow	Q_{air}	2.94 mol/s
Syngas molar flow	$\dot{n}_{syngas}$	5.01 mol/s
Syngas higher heating value	$HHV_{syngas,db}$	4.75 MJ/Nm^3
Specific volumetric tar production	m_{tar,Nm^3}	23.63 g/Nm^3
Gasifier cold gas efficiency	η_{cold}	78.98 %
Average temperature of gasification	T	895 K
SOFC + MGT		
Description	Symbol	Value
Syngas molar flow to SOFC-MGT unit	$\dot{n}_{SOFC}$	4.95 mol/s
SOFC electrical power production	P_{SOFC}	136.70 kW
MGT electrical power production	P_{MGT}	60.73 kW
Total SOFC-MGT electrical power production	$P_{SOFC+MGT}$	197.43 kW
SOFC+MGT electrical efficiency	$\eta_{SOFC+MGT}$	37.46 %
Overall system		
Description	Symbol	Value
Storage tank pressure range	p_{serb}	2.67-5.39 bar
Average electrical auxiliary consumption	P_{self}	34.24 kW_{el}
Average electrical total power production	P_{tot}	163.19 kW_{el}
Average total electrical efficiency	η_{tot}	25.43 %

Table 4: Case II (PPO + Gasifier + SOFC + MGT) simulation results

PPO module		
Air inlet flow	Q_{air}	2.97 mol/s
Permeate molar flow	Q_P	1.27 mol/s
Retentate molar flow	Q_R	1.69 mol/s
Molar fraction of O_2 in permeate	y_{O2}	48.9 %
Molar fraction of N_2 in permeate	y_{N2}	51.1 %
Electric power consumption	$P_{el,PPO}$	15.3 kW
Gasifier		
Description	Symbol	Value
H_2 syngas fraction	x_{H_2}	28.49 %
H_2O syngas fraction	x_{H_2O}	9.91 %
CO syngas fraction	x_{CO}	26.33 %
CH_4 syngas fraction	x_{CH_4}	1.66 %
CO_2 syngas fraction	x_{CO_2}	17.2 %
N_2 syngas fraction	x_{N_2}	16.41 %
Syngas molar flow	$\dot{n}_{syngas}$	3.589 mol/s
Syngas higher heating value	$HHV_{syngas,db}$	7.55 MJ/Nm^3
Specific volumetric tar production	m_{tar,Nm^3}	0.27 g/Nm^3
Gasifier cold gas efficiency	η_{cold}	92.0 %
Average temperature of gasification	T	931 K
SOFC + MGT		
Description	Symbol	Value
Syngas molar flow to SOFC-MGT unit	$\dot{n}_{SOFC}$	3.545 mol/s
SOFC electrical power production	P_{SOFC}	184.20 kW
MGT electrical power production	P_{MGT}	68.33 kW
Total SOFC-MGT electrical power production	$P_{SOFC+MGT}$	252.53 kW
SOFC+MGT eletrical efficiency	$\eta_{SOFC+MGT}$	42.08 %
Overall system		
Description	Symbol	Value
Storage tank pressure range	p_{serb}	2.67-4.62 bar
Average electrical auxiliary consumption	P_{self}	42.01 kW_{el}
Average electrical total power production	P_{tot}	210.52 kW_{el}
Average total electrical efficiency	η_{tot}	32.81 %

Table 5: Case III (Gasifier + ZEO + SOFC + MGT) simulation results

Gasifier (see Case I)		
ZEO		
Description	Symbol	Value
H_2 syngas fraction after adsoption	x_{H_2}	25.36 %
CO syngas fraction after adsoption	x_{CO}	17.08 %
CH_4 syngas fraction after adsoption	x_{CH_4}	1.43 %
CO_2 syngas fraction after adsoption	x_{CO_2}	0.39 %
N_2 syngas fraction after adsoption	x_{N_2}	55.73 %
Syngas molar flow after adsoption	$\dot{n}_{syngas}$	4.065 mol/s
Syngas higher heating value after adsoption	$HHV_{syngas,db}$	5.9 MJ/Nm^3
Active zeolite mass for every regeration cycle	m_{zeo}	23.742 kg
SOFC + MGT		
Description	Symbol	Value
Syngas molar flow to SOFC-MGT unit	$\dot{n}_{SOFC}$	4.020 mol/s
SOFC electrical power production	P_{SOFC}	138.50 kW
MGT electrical power production	P_{MGT}	44.00 kW
Total SOFC-MGT electrical power production	$P_{SOFC+MGT}$	182.5 kW
SOFC+MGT electrical efficiency	$\eta_{SOFC+MGT}$	34.33 %
Overall system		
Description	Symbol	Value
Storage tank pressure range	p_{serb}	2.66-4.88 bar
Average electrical auxiliary consumption	P_{self}	33.76 kW_{el}
Average electrical total power production	P_{tot}	148.74 kW_{el}
Average total electrical efficiency	η_{tot}	22.87 %

Table 6: Case IV (PPO + Gasifier + ZEO + SOFC + MGT) simulation results

PPO module (see Case II)		
Gasifier (see Case II)		
ZEO		
Description	Symbol	Value
H_2 syngas fraction after adsoption	x_{H_2}	41.53 %
CO syngas fraction after adsoption	x_{CO}	32.54 %
CH_4 syngas fraction after adsoption	x_{CH_4}	2.21 %
CO_2 syngas fraction after adsoption	x_{CO_2}	0.43 %
N_2 syngas fraction after adsoption	x_{N_2}	23.30 %
Syngas molar flow after adsoption	$\dot{n}_{syngas}$	2.726 mol/s
Syngas higher heating value after adsoption	$HHV_{syngas,db}$	10.19 MJ/Nm^3
Active zeolite mass for every regeration cycle	m_{zeo}	20.244 kg
SOFC + MGT		
Description	Symbol	Value
Syngas molar flow to SOFC-MGT unit	$\dot{n}_{SOFC}$	2.696 mol/s
SOFC electrical power production	P_{SOFC}	184.70 kW
MGT electrical power production	P_{MGT}	51.80 kW
Total SOFC-MGT electrical power production	$P_{SOFC+MGT}$	236.50 kW
SOFC+MGT electrical efficiency	$\eta_{SOFC+MGT}$	38.41 %
Overall system		
Description	Symbol	Value
Storage tank pressure range	p_{serb}	2.66-4.15 bar
Average electrical auxiliary consumption	P_{self}	51.80 kW_{el}
Average electrical total power production	P_{tot}	194.53 kW_{el}
Average total electrical efficiency	η_{tot}	30.32 %

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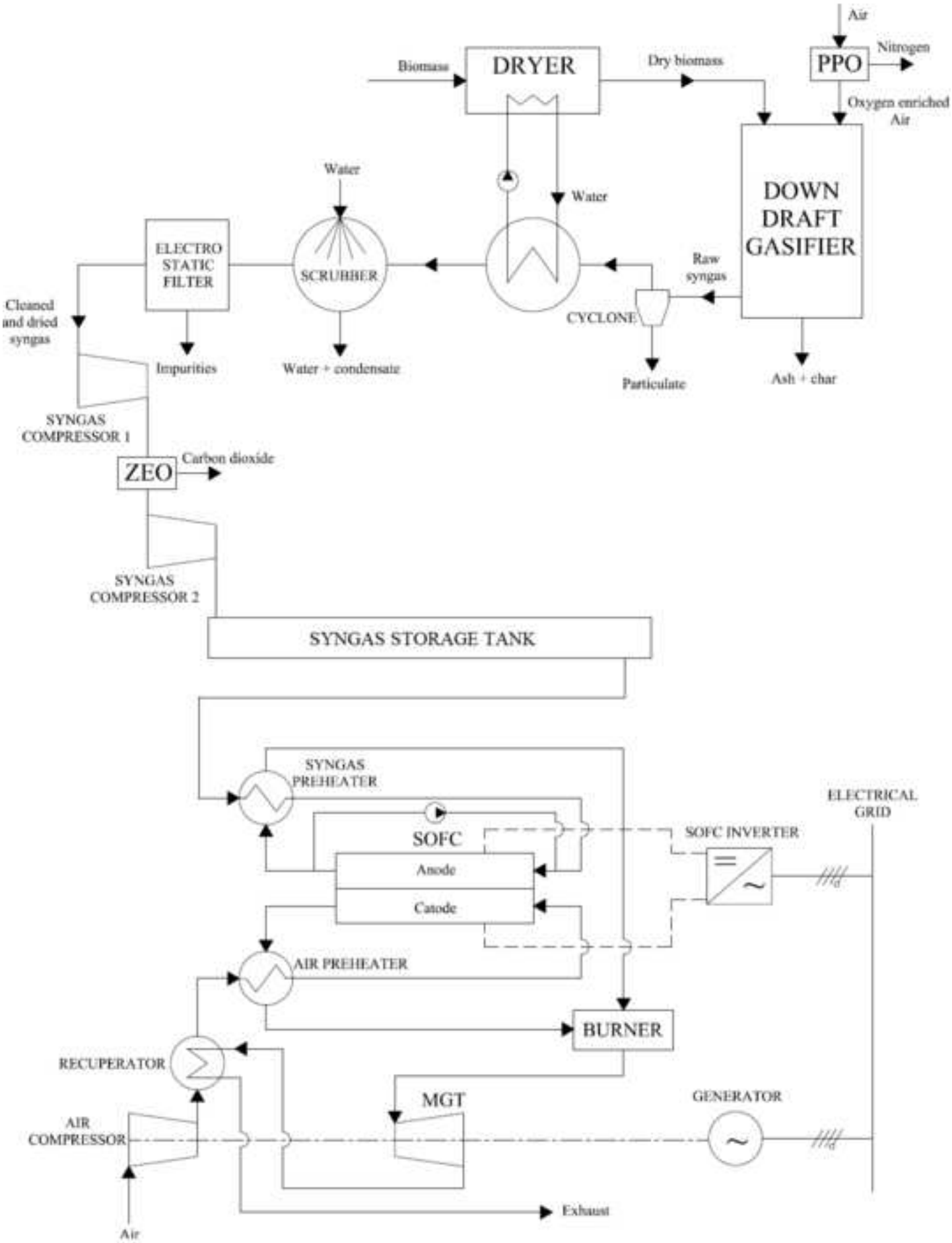

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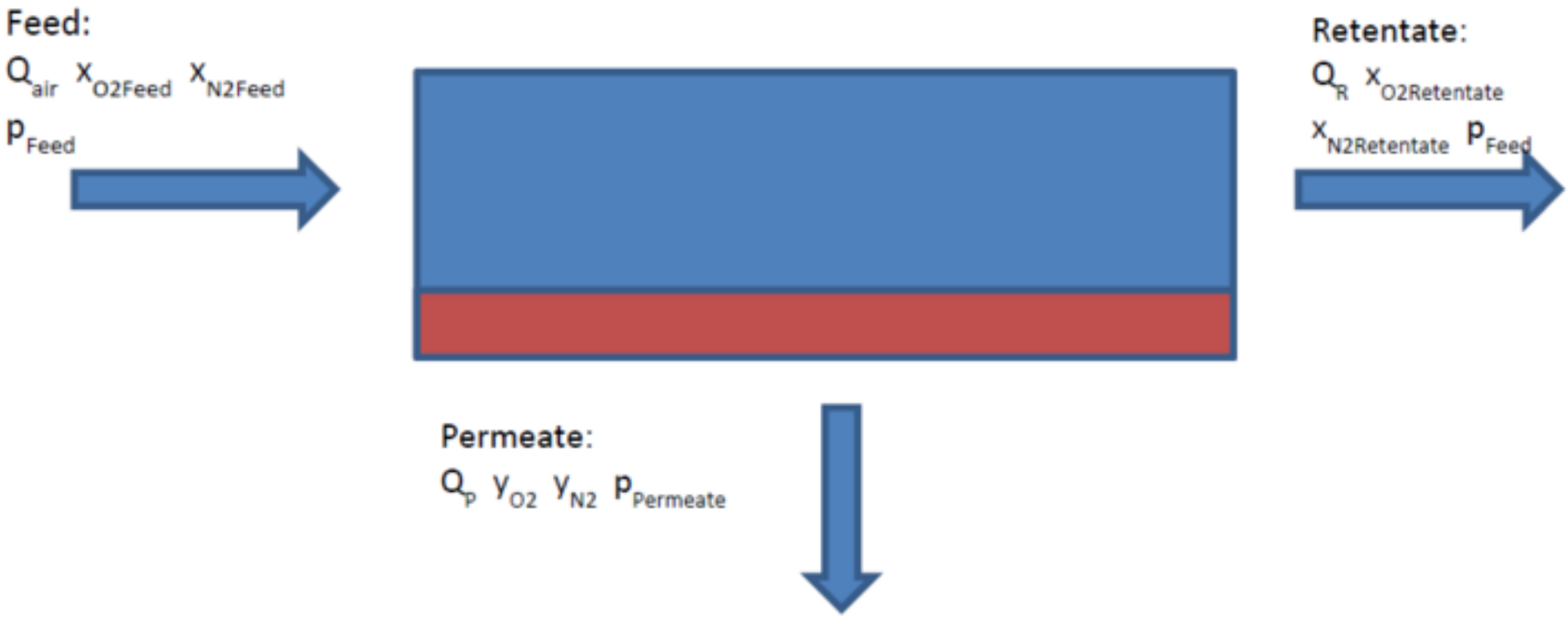

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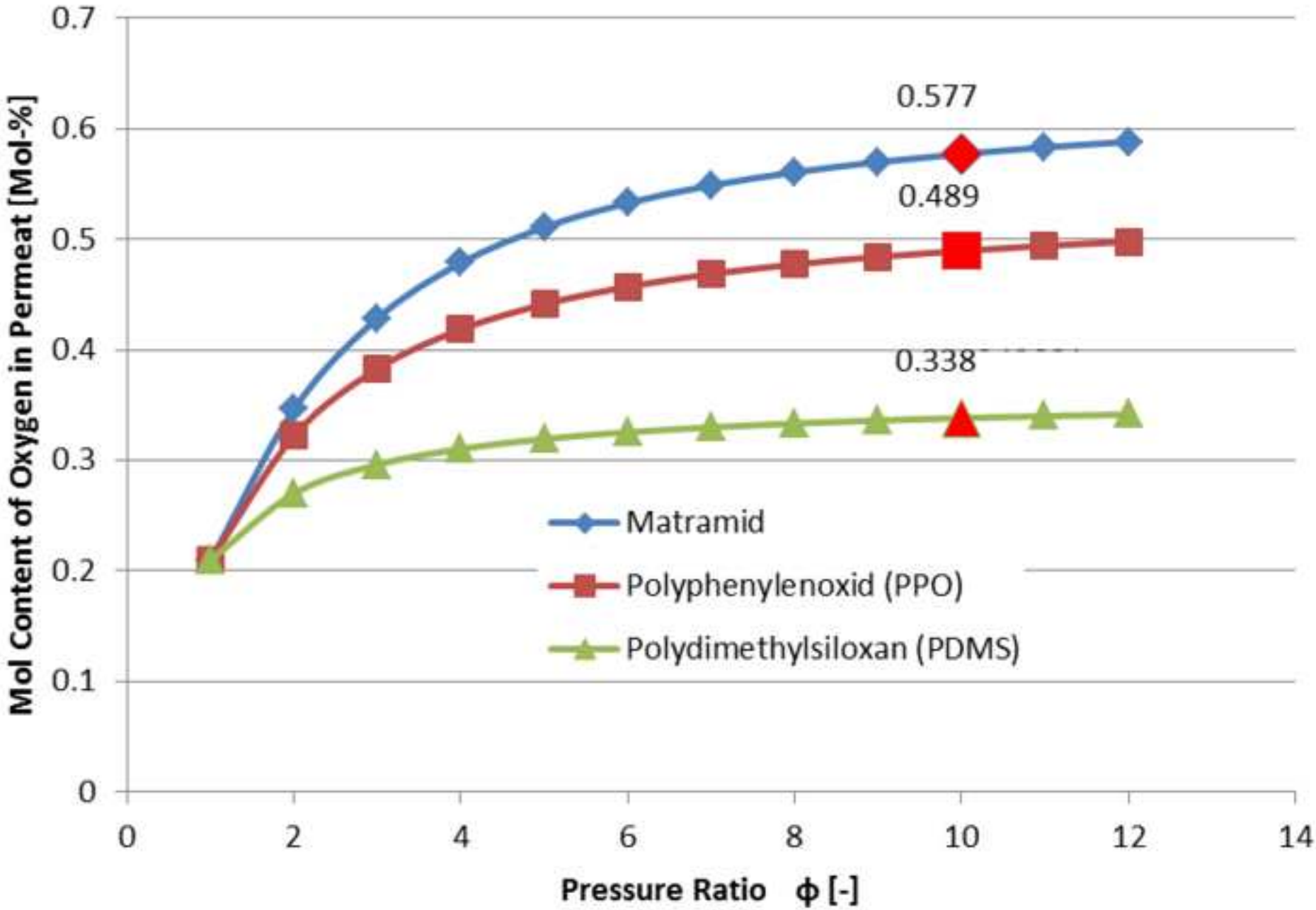

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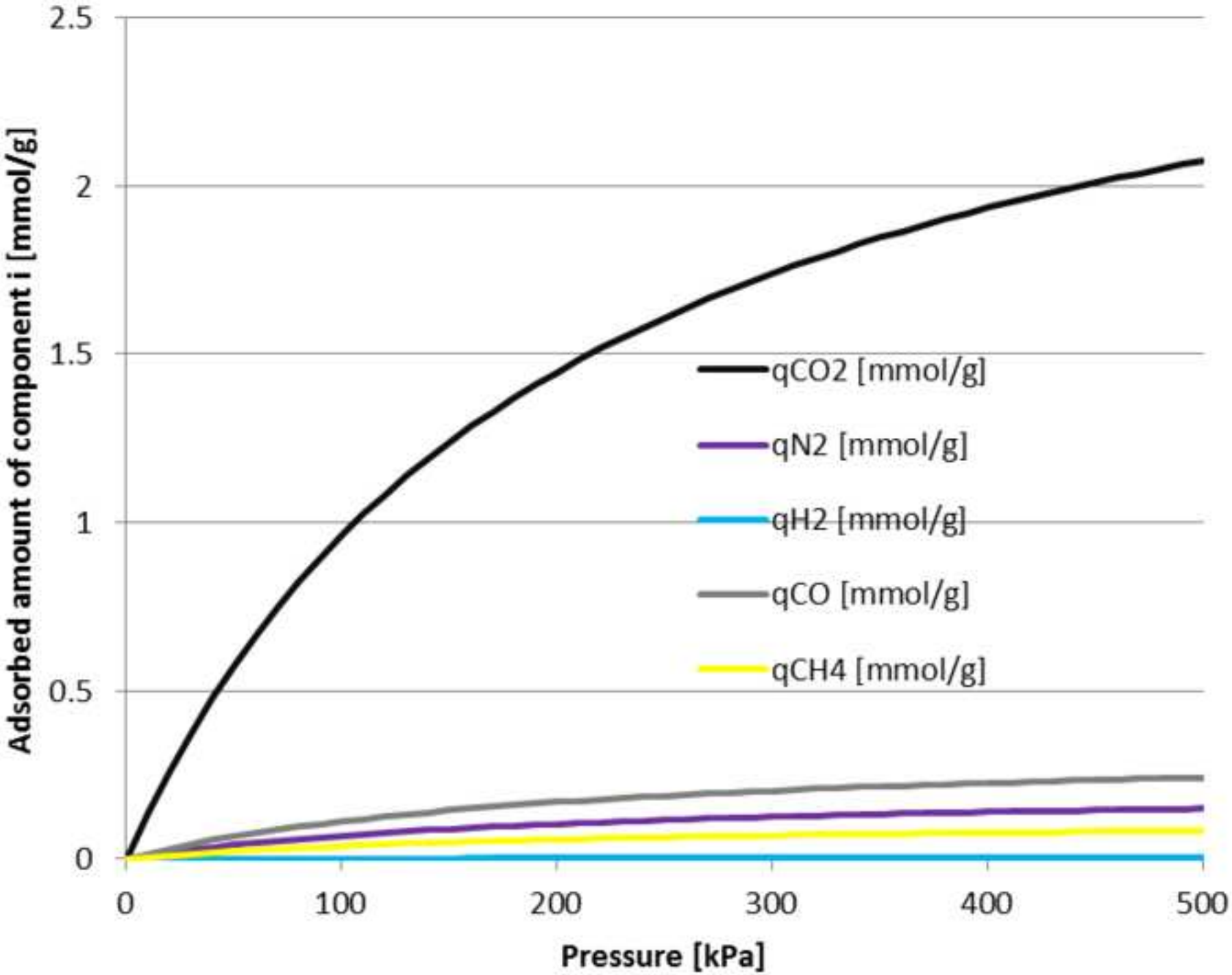

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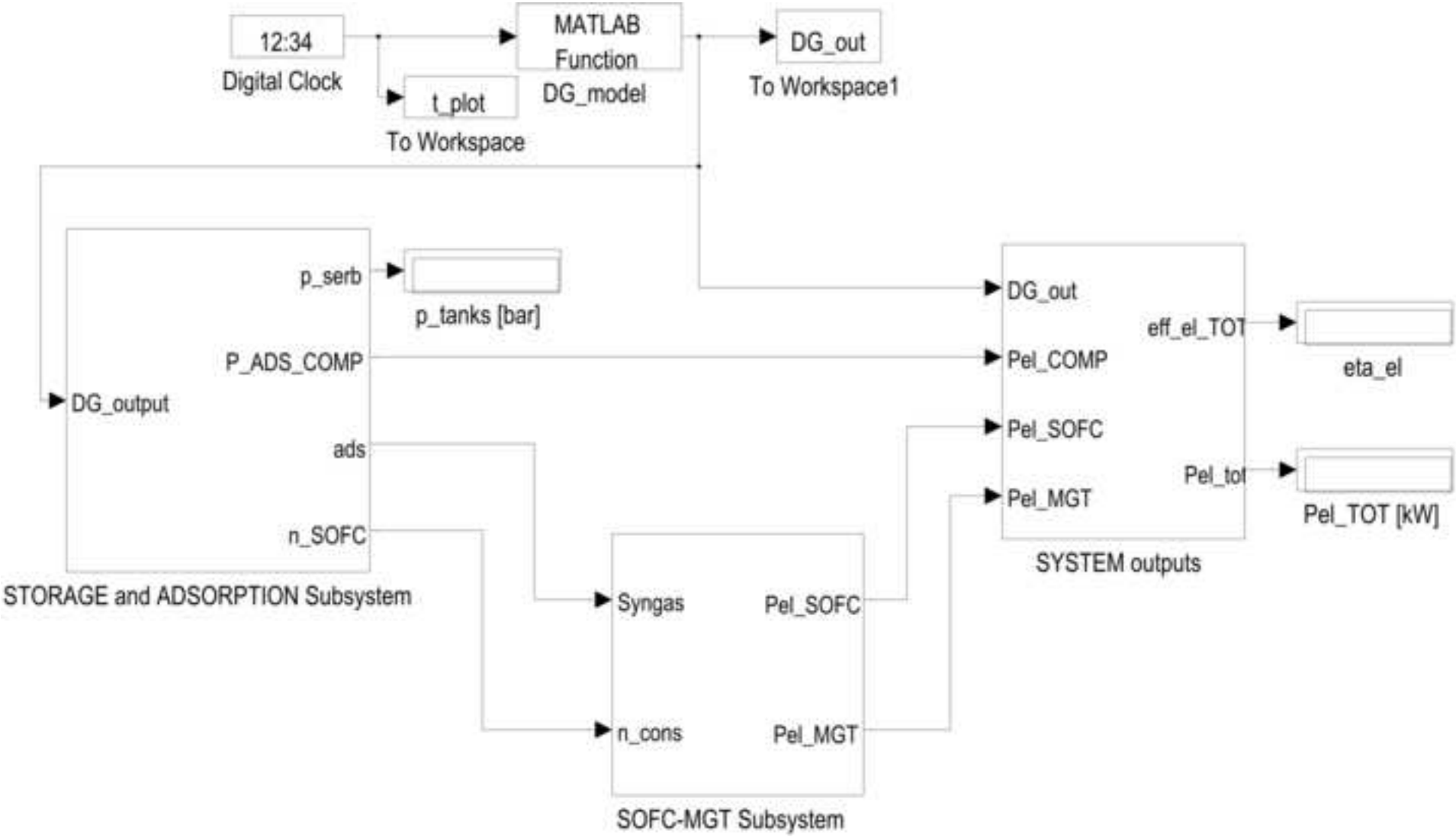

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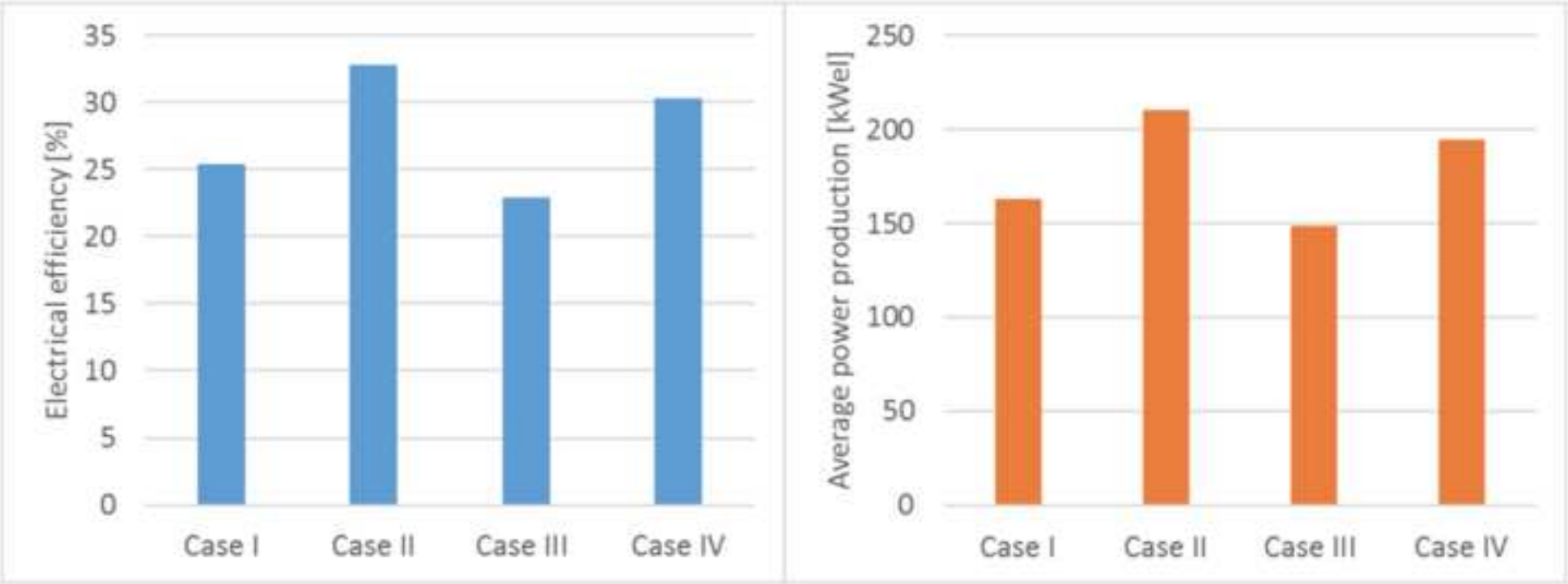

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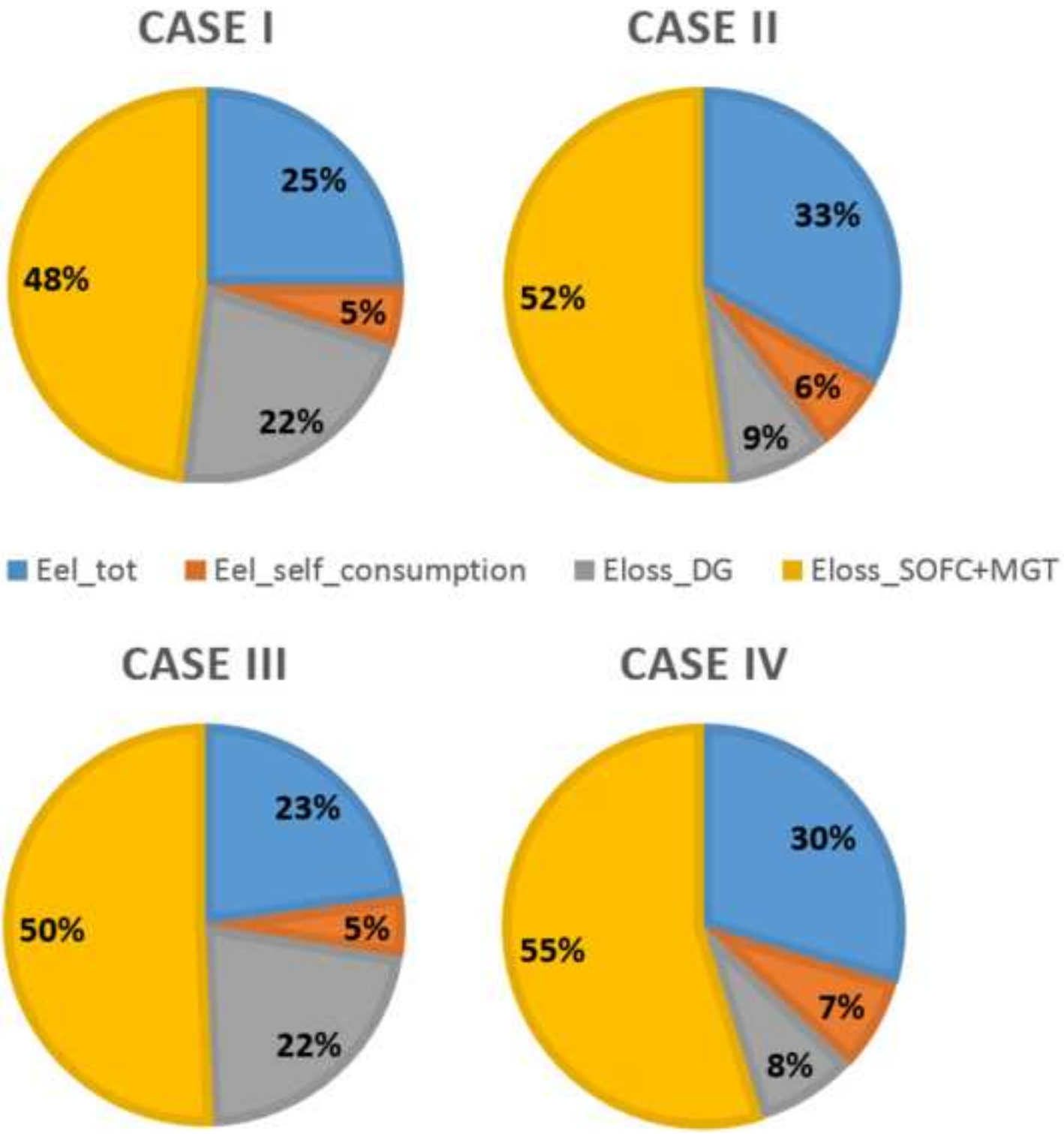

***Detailed Response to Reviewer Comments**

Response to Review Comments

Thanks to the reviewers for their work, I have revised my present research paper in the light of their useful suggestions and comments. The corrections in the manuscript were made in red color. I hope my revision has improved the paper to the level of their satisfaction:

(O) = reviewer observation

(A) = author answer

Editor

(O): Please update your literature survey by referring to the most recent and relevant references that have been published in highly ranked and prestigious journals including this journal. Please focus on relevant publications during the last few years.

(A): We add 5 recent references about fuel cells systems in the introduction section

Reviewer # 1

(O): The manuscript should be carefully checked again for typos, for example: line 18, 43, and 415 etc..

(A): Done

(O): A nomenclature section is needed to quickly refer to any symbol/acronym during the reading of the article.

(A): Done

(O): Fig. 5, Simulink model is not properly visible. An increase in font size or style maybe required.

(A): Done

(O): In introduction section, the authors have emphasized largely on the importance of PPO or ZEO module and their working principle. In one way, this is important to explain all details. But the reviewer suggest that trivial details about importance of PPO or ZEO module should be mentioned briefly with proper literature references (for further study) and more focus should be on literature review of these modules and their effect on the efficiency of the system. I could not find the authors mentioning any study related to this scope of work.

(A): Several works about PPO membrane air filtration and zeolites adsorption applications are now cited in the introduction section.

(O): The conclusion section maintains that including the PPO and ZEO might result in higher efficiencies, which is major focus of this paper. But, in results section, the discussion related to comparison of these cases with existing energy conversion systems (IC engine or ORC etc.) might be missing/less emphasized. It is suggested that a detailed comparison of energy conversion efficiencies of other technologies may be included in the discussion section.

(A): We add a comparison with a common gasifier-IC engine power plant in the “Performance and energy consideration” subsection.

(O): Table 1 (page 38), gasifier model parameters reference for data may be furnished.

(A): Reference added

(O): Table 3-6 show data obtained from different cases during simulation. It is suggested that a brief summary of all simulation results (in the form of a graph) might be helpful for the reader to get an overview of the results.

(A): Figure 6 reports efficiency and power production results reported in Table 3-6. In addition Figure 7 shows energy results of the fourth cases.

Thank you again for your review.

All the best,

Simone Pedrazzi

Effects of upgrading systems on energy conversion efficiency of a gasifier - fuel cell - gas turbine power plant

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Abstract

THIS PAPER IS SUBMITTED WITH THE OPTION 'YOUR PAPER YOUR WAY'. FOR THIS REASON LAYOUT AND STYLE MAY DIFFER FROM THE JOURNAL ONE.

This work focuses on a DG-SOFC-MGT (downdraft gasifier- solid oxide fuel cell - micro gas turbine) power plant for electrical energy production and investigates two possible performance-upgrading systems: polyphenylene oxide (PPO) membrane and zeolite filters. The first is used to produce oxygen-enriched air used in the reactor, while the latter separates the CO_2 content from the syngas. In order to prevent power plant shutdowns during the gasifier reactor scheduled maintenance, the system is equipped with a gas storage tank. The generation unit consists of a SOFC-MGT system characterized by higher electrical efficiency when compared to conventional power production technology (IC engines, ORC and EFGT). Poplar wood chips with 10% of total moisture are used as feedstock. Four different combinations with and without PPO and zeolite filtrations are simulated and discussed. One-year

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energy and power simulation were used as basis for comparison between all the cases analyzed. The modeling of the gasification reactions gives results consistent with literature about oxygen-enriched processes. Results showed that the highest electrical efficiency obtained is 32.81%. This value is reached by the power plant equipped only with PPO membrane filtration. Contrary to the PPO filtering, zeolite filtration does not increase the SOFC-MGT unit performance while it affects the energy balance with high auxiliary electrical consumption. This solution can be considered valuable only for future work coupling a CO_2 sequestration system to the power plant.

Keywords:

Biomass, Gasification, Modeling, Solide Oxide Fuel Cells, Zeolites, PPO membrane

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1. Introduction

Due to the abundant availability and distribution, biomasses hold key-roles in plans for renewable energy production. This trend is becoming even more relevant thanks to the good degree of reliability and efficiency of the biomass-based technologies together with the high subsidies granted by several government for sustainable electrical energy production [1].

Depending on the feedstock quality and availability, biomasses are converted into energy through different technologies. In the case of ligno-cellulosic biomasses, a technolgy of great validity is gasification. This thermo-chemical process turns solid biomass into a gaseous fuel known as syngas, which can be converted into electrical energy through all those systems used for power production from gaseous fuels [2]. Gasification is today one of the most effi-

cient technologies to convert wood into electricity and it is also sustainable in terms of the environmental balance of CO_2 [3, 4].

Most of the gasification power plants use an IC engine-generator to convert the syngas chemical energy into electrical power. However, in some cases other conversion machines are used, i.e. Organic Rankine Cycles (ORC), External Firing Gas Turbines (EFGT)[5] and Stirling engines are used with the major advantage of having minor limitation about the syngas level of purification [2, 6, 7, 8, 9]. These systems are usually characterized by low conversion efficiencies of about 10-12%. Major conversion rates can be obtained only with electrochemical devices such as proton exchange membrane fuel cells [10], Molten Carbonate Fuel Cells (MCFC) [11, 12], Solid Oxide Fuel Cells (SOFC) [13, 14, 15], systems composed of SOFC and Micro Gas Turbines (MGT) [16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26] and systems composed of SOFC-MGT-ORC [27]. Despite the high rate of energy conversion, these systems require perfectly clean syngas [28]. Downdraft gasifiers are the most suitable architecture due to the low tar and particulate content in their gas when compared to updraft, crossdraft or fluidized bed gasifiers [2, 6, 29]. However, downdraft gasifiers commonly use air as gasification agent. This solution generates a syngas with a low calorific value where the hydrogen, methane and carbon monoxide are diluted in non-burnable gases: N_2 (about 50%) and CO_2 (from 10 to 20%). Otherwise, it is possible to choose oxygen gasification that produces a syngas with negligible N_2 content. However, oxygen gasification is a complex and expensive technology due to the gasification agent supply sub-systems and reactor material choice. Indeed, temperatures inside the reactor can reach 1200-1300 K when oxygen is used instead of air

[30].

The basic system discussed in this study is composed of an air blown-downdraft-fixed bed gasifier fed with poplar wood chips. This work is aimed at investigating the effects of different power plant designs on the overall energy conversion efficiency.

The first power plant upgrading sub-system consists of a polyphenylene oxide (PPO) membrane used to produce oxygen-enriched air. The gas separation characterization of this membrane is reported in literature [31, 32]. In practice, membrane gas separation is applied to increase the oxygen content in the inlet air of biomass boilers [33]. Bisio et al. studied the thermodynamics of combustion with enriched air and reviewed several types of memebranes [34]. Coombe and Nieh developed a membrane-based device for air enrichment in small scale burners [35]. Hao et al. applied an oxygen-permeable membrane to a reactor for the co-production of dimethyl ether (DME)/methanol and electricity [36]. This paper uses PPO membrane in order to obtain air with about 50% of oxygen then used as gasification agent. This solution is a hybrid between air and pure oxygen gasification. Enriched air reduces the reactor thermal stress compared to pure oxygen gasification, while the syngas has a lower N_2 content than the one obtained in pure air gasification. In addition, the syngas flow rate decreases because, for a fixed power output, the enriched air flow required for gasification is lower than air used in conventional gasification. This happens because the same amount of oxygen is used in both cases and its concentration in enriched air is higher than untreated air. Finally, the tar production is lower than air gasification as consequence of the higher temperature that cracks more efficiently the

primary tars from pyrolysis [37].

A second solution discussed in this work consists of a porous media used to upgrade the syngas. In fact, syngas has a variable CO_2 content depending on gasification process as well as several boundary conditions. This value ranges from 10% to 30% and it reduces significantly the higher heating value of the syngas [37]. A solution to overcome this issue is to adopt a pressure-swing selective synthetic zeolite filter. This system is placed before the gas storage in order to separate carbon dioxide from syngas [38, 39]. The filter can be constantly regenerated using a rotary valve packaged into modules as described by Tagliabue et al. [40]. Literature investigation about zeolite filtration outlines several works. Bacsik et al. studied the biogas CO_2-CH_4 separation through zeolites [41]. Kacem et al. investigated the pressure swing adsorption for CO_2/N_2 and CO_2/CH_4 separation using activated carbon and several types of zeolites [42]. Dirar et al. investigated intrinsic adsorption properties of CO2 on 5A and 13X zeolite [43].

The syngas obtained from gasification is stored and then used in a SOFC unit able to produce electrical and thermal energy. The number of stacks within the cell is optimized taking into account the optimal electrical current density. The chosen number guarantees a good efficiency, however the gas discharged from the cell still contains some chemical energy. For this reason, this work suggests to convert this residual energy in a micro gas turbine (MGT). The syngas storage allows the generation unit to operate in its optimal point, furthermore it prevent the power plant shoutting down during the maintenance operations of the gasifier. This management preserves the SOFC and MGT reliability. However, it is difficult to design the stor-

age capacity because an oversize storage rises the systems costs, while an undersized capacity reduces the time gained for the maintenance. For this reason, the storage was designed taking into account the tanks pressure, the electrical power production of the SOFC-MGT unit and the time required for scheduled stops of the gasifier for maintenance operations.

The mathematics of the whole system was developed starting from literature. The overall model has been implemented in Matlab Simulink^{TM} software environment in order to simulate the behavior of the system under different conditions over a year long simulation.

2. System modeling

The basic system layout is reported in Figure 1. The most relevant components are:

- **Downdraft gasifier:** The gasifier is equipped with a subsystem for the syngas filtering and cooling with water scrubber and electrostatic filters.
- **Syngas storage:** It consists of a tank of a total volume of 650 m^3.
- **SOFC unit:** This subsystem consists of 10875 solid oxide cells and it is connected to the electrical grid by a power inverter.
- **Micro gas turbine (MGT):** this turbo-machinery is used to convert the last part of chemical energy content in the syngas purged by the SOFC.

This work investigates the effect of the implementation of the following sub-systems to the basic scheme:

- **PPO membrane filter module:** The PPO sub-system consists of the membrane filter and a compressor that increases the pressure of the air before the PPO membrane filter to about 1 MPa. The oxygen enriched air is sent to the gasifier at atmospheric pressure. A flow of nitrogen is purged from the PPO module.

- **Zeolite (ZEO) filter module:** the zeolite (ZEO) filter module is placed after the first syngas compressor. There is a further syngas compression stage ahead the storage tanks because the ZEO module works at 0.5 MPa of pressure as described in Section 2.3, while the pressure in the storage is often higher.

The syngas is used as fuel in the SOFC stack. In this device, the fuel reforming occurs at the anode and there is a recirculation of the 20% of the anode exhaust to increase the fuel reforming performance [18, 22]. The anode exhaust is used to preheat the syngas, then it is finally burned in the MGT burner together with the cathode exhaust. The air required for the electrochemical reaction is compressed and preheated in the recuperator of the MGT as well as in the air preheater of the SOFC.

The SOFC stack generates DC current which is converted into AC current by an inverter and it is sent to the electrical grid. The MGT drags the air compressor and the remaining mechanical energy is converted into electrical energy by an alternator.

2.1. PPO module modeling

Polymeric membranes allow to separate different gaseous components depending on the pore size and pressure applied to the filter [31]. In this work a membrane is used to separate nitrogen from air. The membranes widely used for this purpose are: Matrimid, Polyphenylenoxide (PPO) and Polydimethylsiloxan (PDMS) [31]. As showed in Figure 2, in membranes the inlet air flow is divided in permeate and retentate molar flows. The inlet flow (Q_{air} [mol/s]) has a pressure p_{feed} [atm] and it is composed of x_{O_2Feed} and x_{N_2Feed} molar fractions of oxygen and nitrogen. The permeate molar flow (Q_P [mol/s]) has a pressure $p_{permeate}$ [atm] and it is composed of y_{O_2} and y_{N_2} molar fractions of oxygen and nitrogen. The retentate molar flow (Q_R [mol/s]) has a pressure p_{feed} [atm] and it is composed of $x_{O_2Retentate}$ and $x_{N_2Retentate}$ molar fractions of oxygen and nitrogen.

Each membrane behavior is identified through two parameters: the selectivity (α) and the permeability to oxygen (γ). The first factor represents the attitude of the membrane to attract oxygen, the second quantifies the attitude of the membrane to be crossed by it. High selectivity and permeability ensure great filtering performance in terms of high value of y_{O2} and a small membrane surface area is required to filter a given amount of air. Table 1 presents the parameters of Matrimid, PPO and PDSM membranes.

The choice of a PPO membrane is a compromise in terms of acceptable values of selectivity and permeability. In order to simulate the behavior of the membranes, a mathematical model has been implemented from Melin and Rautenbach [31]. The model is based on the following assumptions:

- Air is considered a binary gas mixture with 21% oxygen and 79% ni-

trogen.

- Steady state conditions.
- Isotherm conditions.
- Isobaric conditions.
- Perfect gas law.
- Constant permeability.
- Perfect mixing conditions on upstream and downstream sides.
- Concentration polarization at the membrane is neglected.
- Pressure loss in the porous support layer is neglected.
- The permeate can drain off freely.

The calculation of the permeate composition is made with the following formula taken from the work of Melin and Rautenbach [31]:

$$y_{O_2} = \frac{1}{2}\left[1 + \phi * \left(x_{O_2Feed} + \frac{1}{\alpha - 1}\right)\right] - \sqrt{\left[\frac{1}{2}\left[1 + \phi * \left(x_{O_2Feed} + \frac{1}{\alpha - 1}\right)\right]\right]^2 - \frac{\alpha * \phi * x_{O_2Feed}}{\alpha - 1}} \tag{1}$$

$$y_{N_2} = 1 - y_{O_2} \tag{2}$$

where ϕ [-] is the feed-permeate pressure ratio given by the following equation:

$$\phi = p_{feed}/p_{permeate} \tag{3}$$

Figure 3 reports the permeate composition over pressure ratio for the three membrane types considered. It can be seen that only a certain maximum of oxygen ratio can be achieved because all the graphs are leveling off. Therefore a pressure ratio of 1 MPa was chosen for further calculations as suggested in Melin and Rautenbach [31] and the $p_{retentate}$ was fixed at 1 atm.

The Matrimid membrane is able to produce the highest oxygen ratio of 0.58 % vol. in the permeate, however PPO membrane presents a good value of oxygen ratio (0.49 % vol.) and an acceptable value of permeability, therefore this membrane is adopted in the simulations. The active area of the membrane can be assessed from the molar flow of oxygen required for the gasification Q_{PO_2} [mol/s]:

$$A_{membrane} = \frac{Q_{PO_2}}{\gamma * (x_{O_2Feed} * p_{feed} + y_{O_2} * p_{permeate})} \tag{4}$$

The molar flow of nitrogen Q_{PN_2} [mol/s] and the total permeate molar flow Q_P [mol/s] is given by the following equations:

$$Q_{PN_2} = \frac{\gamma}{\alpha} * [p_{feed} * (1 - x_{O_2Feed}) + p_{permeate} * (1 - y_{O_2})] \tag{5}$$

$$Q_P = Q_{PN_2} + Q_{PO_2} \tag{6}$$

The molar flow of the inlet air Q_{air}, the retentate molar flow Q_R and the retentate composition ($x_{O_2Retentate}$ and $x_{N_2Retentate}$) are calculated setting to zero the amount of oxygen in the retentate flow as suggested by Melin and

Rautenbach[31]. Thus, a mass balance equation can be applied to estimate Q_{air} and Q_R:

$$Q_{air} * x_{O_2Feed} = Q_P * y_{O_2} \rightarrow Q_{air} = \frac{Q_P * y_{O_2}}{x_{O_2Feed}} \tag{7}$$

$$Q_{air} = Q_P + Q_R \rightarrow Q_R = Q_{air} - Q_P \tag{8}$$

Finally, the electrical power consumption to pressurize the inlet air flow is calculated as a polytropic compression by Equation 15 assuming $T_{in} = 20$ ^{o} C; $m = 1.2$ and $\eta_{comp} = 90$ %.

2.2. Gasifier modeling

In this work, the gasification process is simulated using a black-box model based on Barman's work [44]. The model is validated for downdraft gasifiers; it is based on the following gasification equation:

$$\begin{aligned} CH_xO_yN_z + wH_2O + m\left(O_2 + 3.76N_2\right) \rightarrow \\ n_{H_2}H_2 + n_{CO}CO + n_{CO_2}CO_2 + n_{H_2O}H_2O \\ +n_{CH_4}CH_4 + \left(z/2 + 3.76m\right)N_2 + n_{tar}CH_pO_q \end{aligned} \tag{9}$$

where $CH_xO_yN_z$ is the equivalent chemical formula of "dry and ash free" (daf) biomass; CH_pO_q is the equivalent chemical formula of tar [45]; w $[mol/mol_{bio}]$ is the specific molar amount of the biomass moisture; m $[mol/mol_{bio}]$ is the specific molar amount of oxygen calculated starting from the equivalence ratio ER as suggested by Jarungthammachote and Dutta[46]; $n_{H_2}, n_{CO}, n_{CO_2}, n_{H_2O}, n_{CH_4}$, n_{tar} $[mol/mol_{bio}]$ are the specific molar amounts of $H_2, CO, CO_2, H_2O, CH_4$ and tar which constitute the syngas.

This model is used and discussed in several other works [47, 48, 49]. It consists of a chemical and a thermal sub-models that converge to the final composition of the gas. The first step is to choose an initial temperature T [K] and calculate the equilibrium constant of the following reactions:

- **K1:** Water-gas shift $CO + H_2O \leftrightarrow CO_2 + H_2$
- **K2:** Hydrogasification $C + 2H_2 \leftrightarrow CH_4$
- **K3:** Methane steam reforming $CH_4 + H_2O \leftrightarrow CO + 3H_2$

The system of equations 10 reported below is composed of three chemical balances calculated from Equation 9 (carbon, hydrogen and oxygen) and the three equilibrium constants for water-gas, hydrogasification and methane reforming reactions. The system is solved with the Newton-Raphson method.

$$\begin{cases} n_{CO} + n_{CO_2} + n_{CH_4} + n_{tar} - 1 = 0 \\ 2n_{H_2} + 2n_{H_2O} + 4n_{CH_4} + pn_{tar} - x - 2w = 0 \\ n_{CO} + 2n_{CO_2} + n_{H_2O} + qn_{tar} - w - 2m - y = 0 \\ K_1 = \frac{n_{CO_2} * n_{H_2}}{n_{CO} * n_{H_2O}} \\ K_2 = \frac{n_{CH_4} * \frac{\dot{n}_{tot,wet}}{\dot{n}_{bio,daf}}}{n_{H_2}^2} \\ K_3 = \frac{n_{CO} * n_{H_2}^3}{\left(\frac{\dot{n}_{tot,wet}}{\dot{n}_{bio,daf}}\right)^2 n_{H_2O} n_{CH_4}} \end{cases} \tag{10}$$

Once the molar specific amounts of the syngas species are evaluated, it is possible to solve the thermodynamic energy balance of the system reported in the following equation:

$$\sum_{j=react} n_j * HF_j^0 = \sum_{i=prod} n_i * \left(HF_i^0 + \Delta H_{T,i}\right) \tag{11}$$

where n_j [moles] and HF_j^0 [kJ/kmol] are the specific moles amount and standard heat of formation of the j-th reagent (biomass, air and moisture); n_i [moles] and HF_i^0 [kJ/kmol] are the specific moles amount and the standard heat of formation of the i-th product (H_2, CO, CO_2, H_2O ,CH_4 and N_2) and $\Delta H_{T,i}$ is the enthalpy difference between any given state and the standard state for the i-th product. $\Delta H_{T,i}$ can be calculated starting from the specific heat of the product:

$$\Delta H_{T,i} = \int_{298.15}^{T} C_p(T)\, dT = \left| aT + b\frac{T^2}{2} + c\frac{T^3}{3} + d\frac{T^4}{4} \right|_{298.15}^{T} \tag{12}$$

where the coefficient a,b,c and d are defined for each gas by Jarungthammachote and Dutta[46]. In order to find the equilibrium temperature T_{new}, the system is considered adiabatic and the the Newton-Raphson method is applied to the equations. If $abs(T - T_{new}) < 0.1$ K then the calculated equilibrium temperature and molar specific gases amounts are the final results; otherwise, a new iteration is done in order to satisfy the previous condition. The model is implemented in Python and the input are the biomass equivalent molecule, the equivalence ratio ER and the initial temperature. The temperature input is used only as a starting point for the iterating system; after few cycles the temperature converges to the ones that satisfy both the chemical and thermal sub-systems. About the ER, a value of 0.335

is assumed. This value is consistent with air blown gasification parameters [50, 37] and it is confirmed by the low tar content in the syngas. Poplar wood chips properties and gasifier model parameters are summarized in Table 1.

2.3. ZEO module modeling

The zeolite filter is able to reduce the total syngas molar flow of about 20% - 30 % by the adsorption of CO_2. Zeolite 5A is chosen because it has a great selectivity for carbon dioxide in comparison with the other gases that constitute syngas [38]. The gas adsorption in porous solids has been described by the Langmuir equation [38, 39]:

$$q_i = \frac{q_{mi} * B_i * p_i}{1 + \sum_{j=1}^{n} B_j * p_j} \tag{13}$$

where q_i [mmol/g] is the adsorbed amount of the component i; q_{mi} [mmol/g] is the saturation adsorbed amount of the component i; B_i [1/kPa] is the Langmuir constant of the component i; p_i [kPa] is the equilibrium partial pressure of the component i; B_j [1/kPa] is the Langmuir constant of the component j; p_j [kPa] is the equilibrium partial pressure of the component j; i and j are the gas species of the syngas. Table 1 reports the Langmuir constants and the saturation adsorbed amounts for Zeolite 5A, while Figure 4 depicts the adsorption trends of the syngas gases as function of pressure. It can be noted the high CO_2 selectivity of the zeolite in comparison with others gases.

The mass of zeolite required for adsorbing all the carbon dioxide of the syngas depends on the molar flow of the dry syngas, its CO_2 molar fraction and kinetic constant of adsorption. The ZEO filter module can be constantly regenerated using a rotary valve packaged into modules as described in [40].

The mass of zeolite that needs to be regenerated every cycle with duration of t_{cycle} can be calculated as follows:

$$m_{zeo} = t_{cycle} * \dot{n}_{DG} * \frac{1 + \sum_{j=1}^{n} B_j * p_j}{q_{m,CO_2} * B_{CO_2} * p_{ads} * x_{CO_2}} \tag{14}$$

where p_{ads} [kPa] is the total pressure of the syngas inside the ZEO filter. A constant temperature of the zeolite filter and of the inlet syngas of 303 K is assumed and the pressure of the inlet syngas is set to 500 kPa as suggested in [38, 39]. The cycling time of regeneration depends on kinetic CO_2 adsorption constant. In this study a plausible time of 60 seconds is assumed and future work will investigate this aspect. Zeolites adsorption generates heat, Ranjani et al. [51] suggests that 64-70 kJ are released for every mole of CO_2 adsorbed. This heat needs to be discharge by the ZEO module in order to keep the temperature constant at 303 K. In this preliminary study, no attention was paid to the ZEO module heat balance. Furthermore, the gas filtering subsystem considered in this work is based on the power plant described by Allesina et al. [50]. It was designed with the idea of coupling the gasifier with an internal combustion engine. Since the minimum presence of tars could negatively affect the performance of the zeolite adsorber, syngas purification unit should be properly designed. A potential alternative to water scrubber is oil scrubber with subsequent stripping of tars [52, 53].

2.4. Compressor and storage system modeling

The modeling of the syngas compression is carried out considering it as a polytropic transformation. The electrical power required for compression is given by Pedrazzi et al. [54]:

$$P_{comp} = \frac{\dot{n}_{gas} L_{comp,is}}{\eta_{comp}} = \frac{\dot{n}_{gas}}{\eta_{comp}} \frac{zRT_{in}}{z-1} \left[1 - \left(\frac{p_{out}}{p_{in}} \right)^{\frac{z-1}{z}} \right] \tag{15}$$

where z is the polytrophic coefficient, R is the universal gas constant equal to 8.314 J mol^{-1} K^{-1}, T_{in} is the gas inlet temperature (25°C for syngas compressor 1 and 30°C for syngas compressor 2), p_{in} and p_{out} [atm] are the gas inlet and outlet pressures, $\dot{n}_{gas}$ [mol/s] is the gas molar flow and η_{comp} is the compressor efficiency available from manufacturer's data [54]. The maximum pressure value inside the storage system is a fundamental parameter required todesign the tanks and the compressor properly. Assuming ideal gas and a constant syngas storage temperature $T_s = 25$ ^{o}C, the pressure inside the tanks is calculated by the ideal gas law:

$$p_s = \frac{nRT_s}{V} \tag{16}$$

where n [mol] are the moles of syngas inside the tanks and V [m^3] is the storage total volume. Assuming a value of the initial syngas moles n_{in} inside the storage, the moles of syngas at the time τ [s] are given by:

$$n = n_{in} + \int_0^{\tau} \left(\dot{n}_{in,s}(t) - \dot{n}_{out,s}(s) \right) dt \tag{17}$$

where $\dot{n}_{in,s}(t)$ and $\dot{n}_{out,s}(t)$ [mol/s] are the inlet and the outlet molar flow at the instantaneous time t [s]. Table 2 reports the model parameters of the storage and compressor sub-systems. The total volume of storage and the initial syngas amount in the tank are reduced of about 50% in comparison with the conventional system without PPO and ZEO modules as investigated in [55, 56]. This result is reached thanks to the PPO adoption that decreases

the molar flow of dry syngas of about the 20% - 30%, while the filtration in the ZEO module further reduces the syngas molar flow of about another 20% - 30% as shown in the results.

2.5. SOFC modeling

The SOFC model used in this study is based on the work of Bang-Møller and Rokni [18]. This model does not take into account the recirculation of gas at the cell anode. This feature may strongly compromise the fuel cell efficiency in case of the presence of gases that do not take part in the electro-chemical, shift and reforming reactions. Unfortunately, syngas contains considerable amounts of CO_2 and N_2. To overcome this issue, the model previously cited is implemented with the reforming model presented by Rami Salah El-Emam et al. [22]. As described by Rami Salah El-Emam, the electro-chemical reactions take place in both the anode and the cathode of the cell (Eq.22), while the reforming and the monoxide water shift occur only near the anode (Eqs. 18, 19). Equation 22 presents the overall electro-chemical reaction that is divided into two sub-reactions: the hydrogen reacts with the oxygen ions to form water and electrons according to Eq. 20 at the anode, while, at the cathode, the oxygen from inlet air reacts with the electrons from the anode (Eq. 21) to form oxygen ions that flow to the anode through the solid oxide electrolyte.

$$CH_4 + H_2O \rightarrow CO + 3H_2 \tag{18}$$

$$CO + H_2O \rightarrow CO_2 + H_2 \tag{19}$$

$$H_2 + O^{2-} \rightarrow H_2O + 2e^- \tag{20}$$

$$\frac{1}{2}O_2 + 2e^- \rightarrow O^{2-} \tag{21}$$

$$H_2 + \frac{1}{2}O_2 \rightarrow H_2O \tag{22}$$

The mathematical modeling of reforming and electrochemical reactions is explained in References [22] and [18]. Using these models, it is possible to calculate the electrical power production and the electrical conversion efficiency for a given syngas inlet flow with a specific composition. The SOFC model parameters adopted in the simulations are reported in Table 2.

2.6. MGT modeling

Mathematical description of gas turbines is well described in literature. Details and assumptions of the present model can be found in Bang-Møller and Rokni work [18]. Characteristics of the turbine and others components connected to the MGT are listed in Table 2.

3. Simulation results and discussion

In this work four different cases are simulated. First of all, the basic system composed of a downdraft gasifier, a storage tank and a SOFC-MGT is simulated. After this step, the two possible solutions consisting of N_2 purging from air or CO_2 separation from syngas are discussed separately. Finally, the complete system provided with PPO module and ZEO module is simulated.

3.1. Case I (Gasifier + SOFC + MGT)

The SOFC-MGT unit constantly produces energy all over the year of simulation in order to preserve the stability of the cells and their gaskets, which are very sensitive to thermal stresses [57]. The syngas molar flow consumed by the SOFC-MGT unit is calculated by Equation 23 that considers the cycling working of the DG:

$$\dot{n}_{syngas-SOFC} = \frac{h_{operation}\dot{n}_{DG}}{h_{operation} + h_{maintenance}} \tag{23}$$

Figure 5 depicts the overall model implemented in Matlab Simulink^{TM} software environment. Table 3 reports the simulation results. Gasifier cold efficiency is about 79%, this value is confirmed by literature that suggests an efficiency of 70% - 80% for air-blown downdraft gasifier [37, 4, 44]. Syngas composition consists of about 19% vol. of H_2 and 15% vol. of CO, the higher heating value of 4.75 MJ/Nm^3 is similar to the results reported by Basu [37] for this kind of gasifier. SOFC-MGT unit has a constant electrical power production of 197.43 kW all over the simulated year. The auxiliary consumption of the whole system strongly depends on tank pressurization level. The average annual value is 34.24 kW. For this reason, the net average power production is reduced to 163.19 kW and the electrical efficiency of the system is 25.43%.

3.2. Case II (PPO + Gasifier + SOFC + MGT)

Table 4 shows the results of the simulation of the system previously described and now equipped with the PPO module. The oxygen enriched air

flow is about 1.27 mol/s. This value is lower than 2.94 mol/s obtained without PPO membrane (Case I). Syngas composition is consistent with the work of Wang et al. [58], where oxygen-enriched air (50% oxygen and 50% nitrogen) is used as gasifying agent in a double stage downdraft gasifier fueled with pine sawdust pellets. Differences of 1-2% between the model outputs and Wang's results about CO and H_2 contents are achieved (29% vs. 27% for H_2 and 26% Vs. 25% for CO). The gasification with oxygen-enriched air assures high gasifier performance in terms of cold gas efficiency (92%), tar production (0.27 g/Nm^3) and syngas higher heating value (7.55 MJ/Nm^3). The syngas outlet flow is 3.589 mol/s, consistently lower than Case I where syngas flow is 5.01 mol/s. The average equilibrium temperature of gasification in this case is 931 K. This value is only 36 K higher than Case I. Wang et al.[58] suggestes a peak temperature of about 1200 K with oxygen-enriched air. With this temperature, conventional material adopted in air gasifier can be used (i.e. stainless steel and refractory brick [2, 6]). In Case II, the overall net power production is 210.52 kW and the electrical efficiency is boosted to 32.81%. The average auxiliary consumption is 42 kW, 8 kW higher than Case I. This is due to the PPO module that uses air at 1 MPa pressure generated by an air compressor. The electrical consumption of the air compressor is 15.3 kW and it is fully compensated by the increasing of the gasifier efficiency and the SOFC-MGT unit efficiency.

3.3. Case III (Gasifier + ZEO + SOFC + MGT)

Table 5 resumes the simulation results of the system with the ZEO filtering module instead of PPO membrane. The filtered syngas has a higher heating value of 5.9 MJ/Nm^3. This value falls between Case I (4.75 MJ/Nm^3)

and Case II (7.55 MJ/Nm^3). The pressure of the storage tank ranges between 0.267-0.488 MPa, similar to the values obtained in Case II (0.266-0.462 MPa) and Case I (0.267-0.539 MPa). The zeolite mass required to perform continuosly the filtration is 23.742 kg. The value obtained is consistent with Tagliabue et al. work [40]. However, in future work, the CO_2 adsorbed by the ZEO module can be stored in order to create a carbon sequestration system. The power production and the net electrical efficiency of the system is low (148.74 kW of power production and 22.87% of electrical efficiency) as a consequence of the energy absorbed by the syngas compressor 1 (see Figure 1) to increase the pressure of the syngas to 0.5 MPa before the ZEO module. This electrical energy consumption is higher than Cases II and I, in addition the efficiency of the SOFC-MGT module fueled with the filtered syngas is lower. As shown in Table 5, the SOFC-MGT efficiency in Case III is about 34%, thus lower than Case II (42.08%) and Case I (37.46%).

3.4. Case IV (PPO + Gasifier + ZEO + SOFC + MGT)

The results about the fully equipped gasifier power system are reported in Table 6. A high power production (194.53 kW) and electrical efficiency (30.32%) is reached thanks to the high H_2 and CO amounts in the filtered syngas. In fact, the H_2 volume percentange reaches 41.53% and the CO volume percentange is boosted to 32.54%. As a consequence of this composition, the higher heating value of the syngas is 10.19 MJ/Nm^3, a value typical for oxygen-blown gasifiers [37]. Therefore, the SOFC-MGT unit syngas consumption is 2.696 mol/s. This value is about 45% lower than Case I (4.95 mol/s), 24% lower than Case II (3.545 mol/s) and 33% lower than Case III (4.02 mol/s). A pressure range of 0.266-0.415 MPa is achieved. In this

case power production and efficiency is lower than Case II as result of higher average auxiliary consumption (51.80 kW) and lower SOFC-MGT unit efficiency (38.41%). However, the utilization of the ZEO module has several advantages: separates the CO_2 and reduces the storage peaks pressure.

3.5. Performance and energy considerations

Figure 6 shows the electrical efficiency and the average power production in every scenario. Case II resulted the best in terms of energy conversion; the overall electrical efficiency reaches 32% and the power production is about 210 kW. These values are higher than commercial gasification power systems with internal combustion engines where the maximum electrical efficiency hardly reaches 25% [37, 4, 2]. This result is given by the PPO module that increases the gasifier efficiency to 92% (75% is the reference value for air blown gasifier [37]) and the SOFC-MGT module which has a higher electrical conversion efficiency (about 42%) compared to common engine-alternator generator units (about 27% [4, 59, 3]). Case II is the best in terms of energy balance as shown in Figure 7. These graphs do not consider the thermal energy that can be recovered from the gasifier or the SOFC-MGT unit. The highest energy loss occurs at the SOFC-MGT unit (about 52%), while auxiliary consumption of the blowers and the auxiliary equipment of the gasifier are low (9%). In Cases I and III, the low efficiency of the gasifier reduces the overall electrical performance of the system. In Cases III and IV the ZEO module consumes energy to separate the CO_2 from the gas, however no efficiency increase occours in the SOFC-MGT unit with a CO_2 free syngas and the final result is a lower power production. The system modeled in this work is obtained starting from a reference power plant described by Allesina et. al

[50] where IC engines are used instead of the SOFC-MGT unit. The author reports an experimental cold gasification efficiency of 67%. Considering an electrical IC engine-alternator unit efficiency of about 27%, as suggested by Puglia at al. [3], the total electrical efficiency is about 18%. This value is 30% lower than Case I and it is 45% lower than Case II. Another study made by Patuzzi et al. [60] reports the values of the net electrical efficiency of three different commercial biomass gasifier - IC engine power plants. The average efficiency is about 20%, this value is consistent with the one obtained for Allesina et al. [50].

4. Conclusions

The biomass fueled system with PPO module (Case II) shows the higher electrical efficiency of about 33%. The reasons behind this result are various. First of all, oxygen-enriched air boosts the gasifier cold efficiency from 79% (Case I with air) to 92% (Cases II and IV with oxygen-enriched air). In addition, the SOFC-MGT unit presents a higher efficiency (about 42%) compared to IC engine-alternator unit (about 27%), ORC cycle (about 20%) or EFGT cycle (about 20%). In Cases III and IV, the zeolites adsoption module consumes energy to increases the higher heating value of the syngas but not the performance of the SOFC-MGT system, this reduces the overall system efficiency. The energy balances of four cases investigated show that the greater losses are in the SOFC-MGT unit. This unit has the difficult task to convert the chemical energy of a gas fuel into electrical energy in an efficient way. An efficiency of about 50% is reached with natural gas, in this study the maximum electrical efficiency is about 42% using a syngas

produced with an oxygen-enriched air as gasifying agent. This difference is given by the presence of several inert gases into the syngas that reduces the electrochemical conversion of the SOFC. The removal or the conversion of these gases into syntethic natural gases (SNG) is possible and, in this way, the efficiency of the SOFC-MGT unit will be similar to the value reach for natural gas one. But, cost and energy self-consumption of the upgrading process are very high and not convenient for this kind of power plants. Cases III and IV has a lower efficiency compared to Case II, however, with the ZEO module, it is possible to seperate the CO_2 content of the syngas with environmental benefits in case the module is coupled with a CO_2 sequestration system. Future work will consider exergy calculations and experimental tests on a micro-scale power system (5-20 kW of electrical power) with PPO module and SOFC module in order to validate modeling results and to assest system durability. In addition, economical net present value analysis will be done to estimate the economic sustainability of the power plant.

Nomenclature

$\dot{m}$	mass flow [kg/s]
$\dot{n}$	molar flow [mol/s]
τ	time [s]
ASH	ash content of the biomass [%]
B	Langmuir constant [1/kPa]
C	carbon

C_p specific heat [J/(mol K)]

DG downdraft gasifier

e electron

$EFGT$ external firing gas turbine

ER equivalence ratio [ad]

H hydrogen

H_T enthalpy [kJ/kmol]

HF^0 standard heat of formation [kJ/kmol]

HHV higher heating value [MJ/Nm^3 or MJ/kg]

IC internal combustion

K equilibrium constant [ad]

L work [kJ]

M total moisture content of the biomass [%]

m specific molar amount of oxygen [mol/mol_{bio}]

m_{tar,Nm^3} volumetric tar amount [g/Nm^3]

$MCFC$ molten carbonate fuel cell

MGT micro gas turbine

MW molecular weight [g/mol]

N nitrogen

n specific molar amount of gases and tar $[mol/mol_{bio}]$

O oxygen

ORC organic rankine cycle

P power [kW]

p pressure [atm]

$PDSM$ polydimethylsiloxan

PPO polyphenylene oxide

Q molar flow [mol/s]

q adsorbed amount [mmol/g]

R universal gas constant [J/(mol K)]

$SOFC$ solide oxide fuel cell

T temperature [K]

t time [s]

V volume [m^3]

w specific molar amount of biomass moisture $[mol/mol_{bio}]$

x molar fraction

y molar fraction

z polytrophic coefficient

ZEO zeolite

α selectivity

Δ difference

γ permeability [mol m^{-}2 s^{-}1 bar^{-}1

ϕ pressure ratio

Subscripts

ads adsorption

ar as received

bio biomass

$comp$ compressor

daf dry ash free

db dry basis

g gas

in inlet

m saturation

out outlet

P permeate

p	hydrogen coefficient of tar
$prod$	product
q	oxygen coefficient of tar
R	retentate
$react$	reactant
s	storage
x	hydrogn coefficient of the biomass
y	hydrogen coefficient of the biomass
z	nitrogen coefficient of the biomass

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modeling of energy conversion effectiveness in a gasification power plant. *International Journal of Heat and Technology*, 30(1):41–44, 2012.

Figure captions and tables

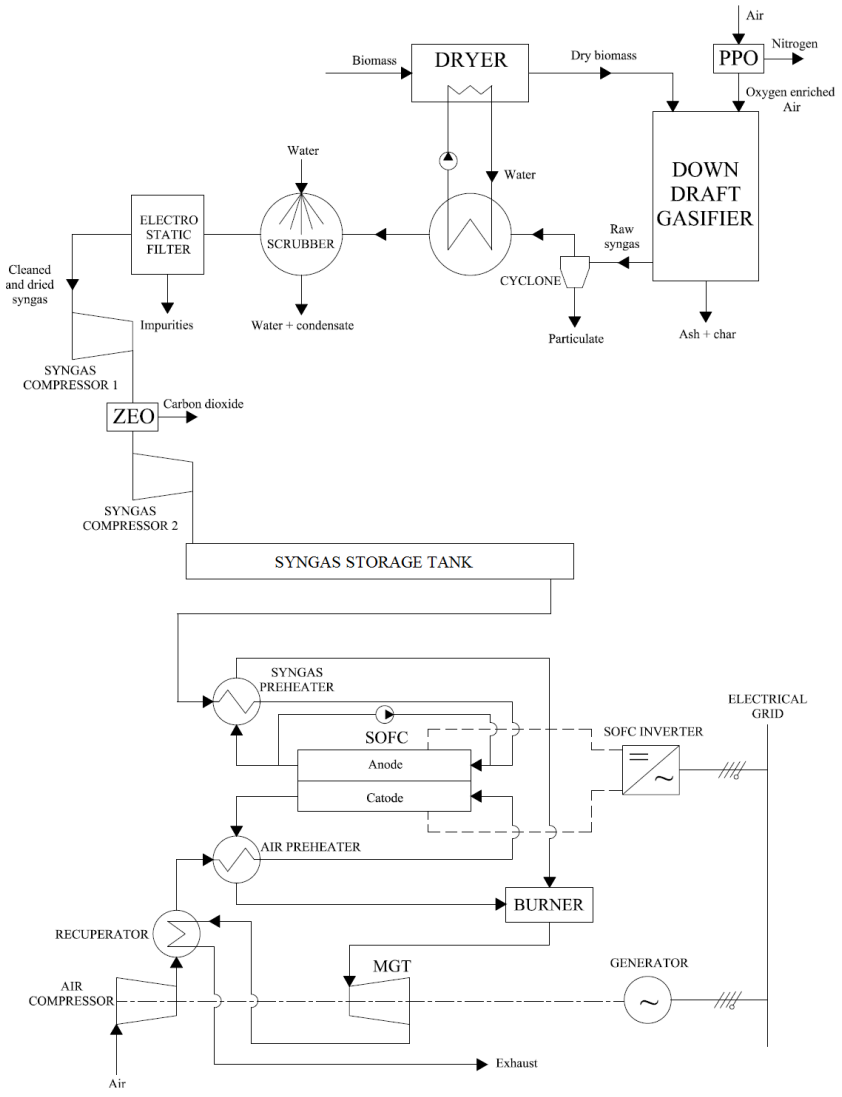

Figure 1: DG-SOFC-MGT hybrid system with zeolite CO_2 adsorption and oxygen-enriched air layout

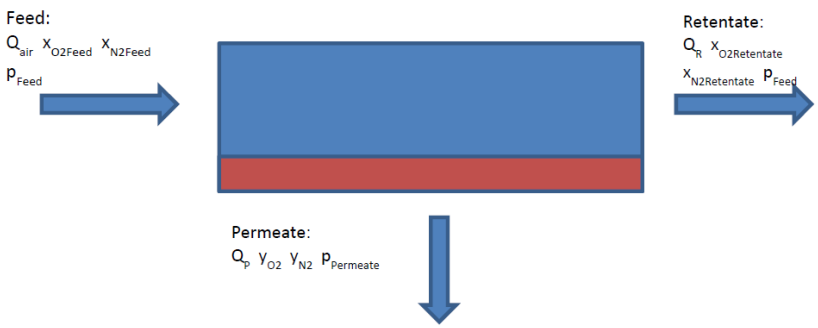

Figure 2: Oxygen enriched air membrane separator principle

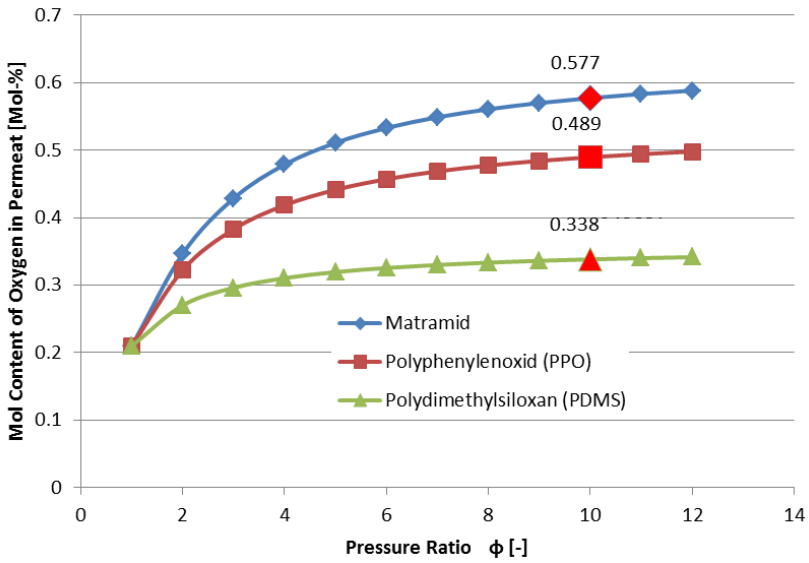

Figure 3: Characteristics of the separation membranes

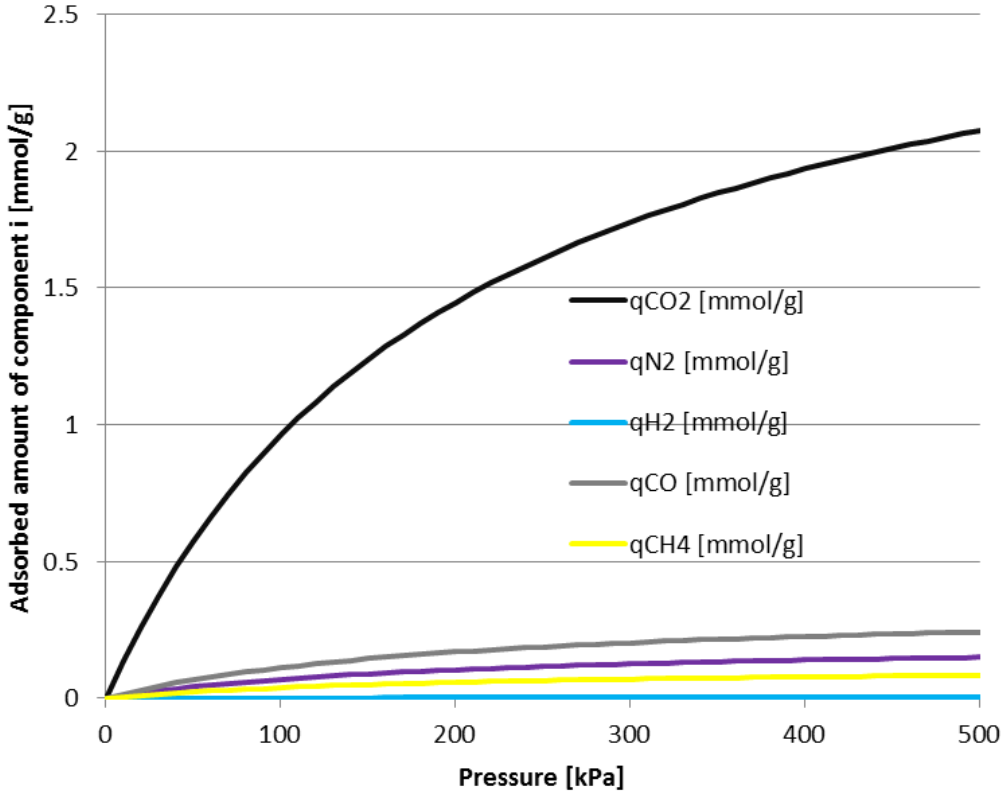

Figure 4: Zeolite 5A adsorbing curve Vs. pressure

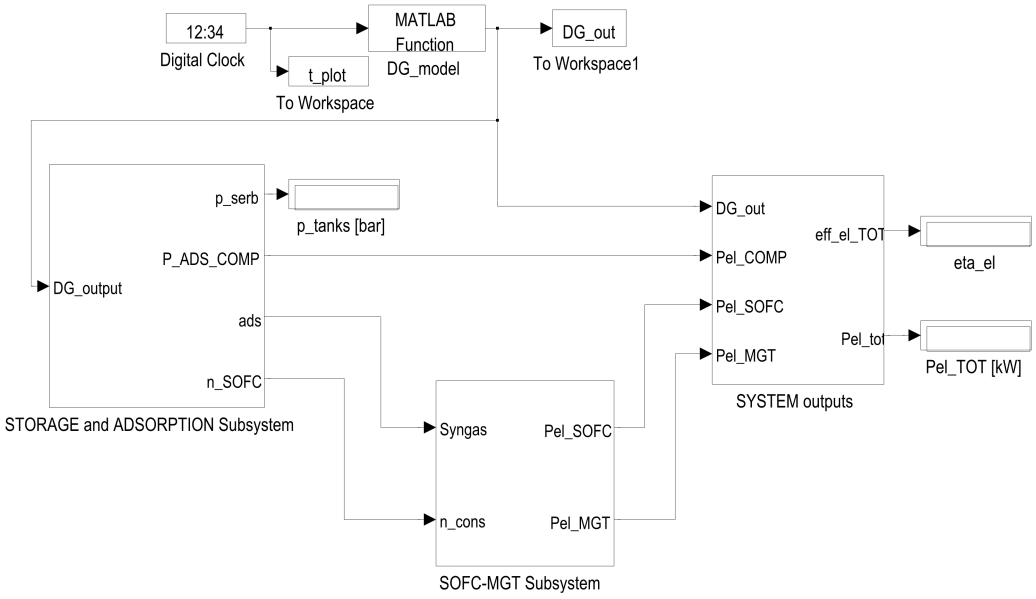

Figure 5: DG-SOFC-MGT hybrid system with zeolite CO_2 adsorption and oxygen-enriched air implemented in Matlab Simulink^{TM}

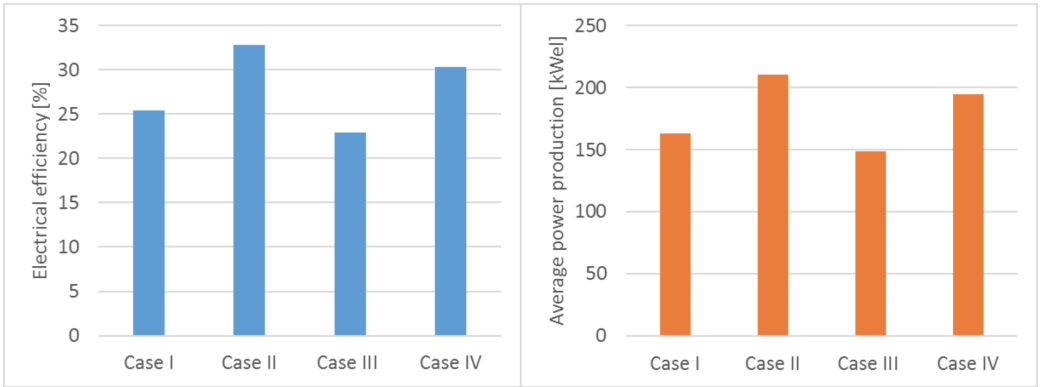

Figure 6: Efficiencies and eletrical production values of the studied cases

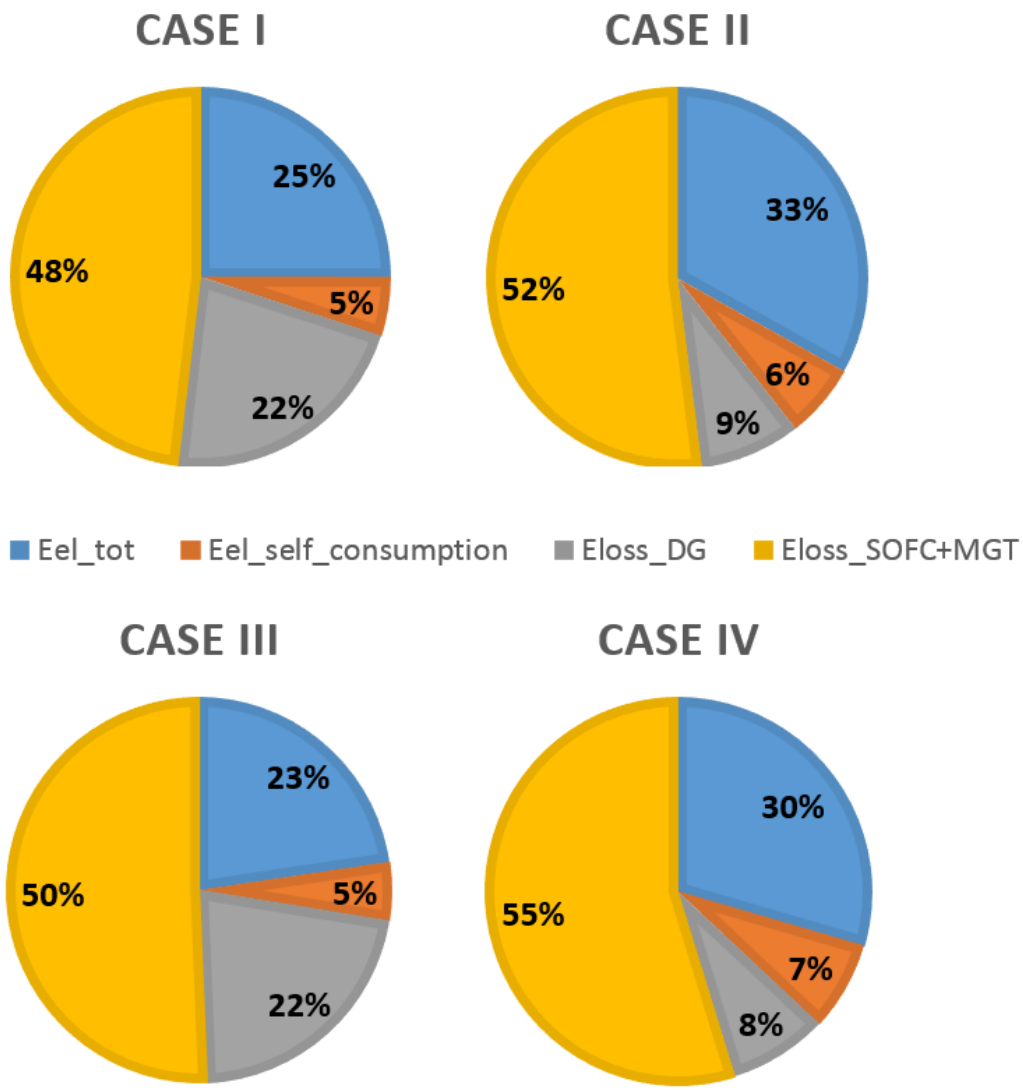

Figure 7: Energy balances of the studied cases

Table 1: Model parameters I

Membranes properties [31]		
Material	Selectivity	Oxigen Permeability
	α [ad]	γ [mol m^{-2} s^{-1} bar^{-1}]
Matrimid	6.7	62.0 x 10^{-5}
PPO	4.7	37.2 x 10^{-4}
PDMS	2.1	39.6 x 10^{-2}
Poplar wood chips properties [61]		
Description	Symbol	Value
Total moisture	M	10 %
Carbon content (as received)	C_{ar}	41.62 %
Hydrogen content (as received)	H_{ar}	5.30 %
Nitrogen content (as received)	N_{ar}	0.52 %
Oxygen content (as received)	O_{ar}	39.81 %
Ash content	ASH	2.75 %
Higher heating value (dry basis)	HHV_{db}	15.7 MJ/kg
Gasifier model parameters[48]		
Description	Symbol	Value
As received biomass consumption	$\dot{m}_{bio}$	187 kg/h
Nominal gasifier thermal power	$P_{th,gas}$	800 kW
Initial calculation temperature	T_{in}	900 K
Pressure	p	1 atm
Equivalence ratio	ER	0.335
Gasifier and filters auxiliary consumption	$P_{DG,self}$	12.5 kW
Cyclic operation hours	$h_{operation}$	360 h
Cyclic maintenance hours	$h_{maintenance}$	4 h
Zeolite 5A parameters of adsorption at 303 K [39]		
Component	B [1/kPa]	q_m [mmol/g]
CO_2	0.019500	3.91900
H_2	0.000361	0.54464
N_2	0.000837	2.62543
CH_4	0.002535	2.75403
CO	0.004350	2.75800

Table 2: Model parameters II

Storage and compressor model parameters		
Description	Symbol	Value
Politropic exponent of the syngas [54]	m	1.33
Syngas compressor efficiency [54]	η_{comp}	92 %
Storage tank temperature	T_s	298.15 K
Initial syngas amount in the tanks	n_{in}	$7 * 10^4$ mol
Total tanks volume	V	650 m^3
SOFC model parameters		
Description	Symbol	Value
Fuel utilization factor	U_f	0.85
Recirculation factor	r	0.2
Operating temperature	T_{sofc}	1073.15 K
Anode pressure loss	Δp_a	500 Pa
Cathode pressure loss	Δp_c	1000 Pa
Anode pressure loss	Δp_a	500 Pa
Current density	i	300 mA/cm^2
Active cell area	A_{cell}	81 cm^2
Cells for each stack	$n_{cell,stack}$	75 cells
Number of stacks	n_{stack}	145 stacks
Cathode air excess	$vent$	1.15
Pressure ratio	PR	2.5
Steam to carbon coefficient	STC	1.4
Electrochemical parameters taken from [18]		
MGT model parameters [18]		
Description	Symbol	Value
Politropic exponenet of the air	m	1.33
Turbine isoentropic efficiency	$\eta_{is,turb}$	84 %
Air compressor isoentropic efficiency	$\eta_{is,comp}$	75 %
Turbine mechanical efficiency	$\eta_{mec,turb}$	99 %
Air compressor mechanical efficiency	$\eta_{mec,comp}$	98 %
Recuperator effectiveness	η_{rec}	85 %
Burner efficiency	$\eta_{eff,burner}$	99 %
MGT generator efficiency	$\eta_{alt,MGT}$	95 %
Pressure ratio	PR	2.5

Table 3: Case I (Gasifier + SOFC + MGT) simulation results

Gasifier		
Description	Symbol	Value
H_2 syngas fraction	x_{H_2}	19.03 %
H_2O syngas fraction	x_{H_2O}	7.78 %
CO syngas fraction	x_{CO}	15.10 %
CH_4 syngas fraction	x_{CH_4}	1.18 %
CO_2 syngas fraction	x_{CO_2}	13.99 %
N_2 syngas fraction	x_{N_2}	42.92 %
Air inlet flow	Q_{air}	2.94 mol/s
Syngas molar flow	$\dot{n}_{syngas}$	5.01 mol/s
Syngas higher heating value	$HHV_{syngas,db}$	4.75 MJ/Nm^3
Specific volumetric tar production	m_{tar,Nm^3}	23.63 g/Nm^3
Gasifier cold gas efficiency	η_{cold}	78.98 %
Average temperature of gasification	T	895 K
SOFC + MGT		
Description	Symbol	Value
Syngas molar flow to SOFC-MGT unit	$\dot{n}_{SOFC}$	4.95 mol/s
SOFC electrical power production	P_{SOFC}	136.70 kW
MGT electrical power production	P_{MGT}	60.73 kW
Total SOFC-MGT electrical power production	$P_{SOFC+MGT}$	197.43 kW
SOFC+MGT electrical efficiency	$\eta_{SOFC+MGT}$	37.46 %
Overall system		
Description	Symbol	Value
Storage tank pressure range	p_{serb}	2.67-5.39 bar
Average electrical auxiliary consumption	P_{self}	34.24 kW_{el}
Average electrical total power production	P_{tot}	163.19 kW_{el}
Average total electrical efficiency	η_{tot}	25.43 %

Table 4: Case II (PPO + Gasifier + SOFC + MGT) simulation results

PPO module		
Air inlet flow	Q_{air}	2.97 mol/s
Permeate molar flow	Q_P	1.27 mol/s
Retentate molar flow	Q_R	1.69 mol/s
Molar fraction of O_2 in permeate	y_{O2}	48.9 %
Molar fraction of N_2 in permeate	y_{N2}	51.1 %
Electric power consumption	$P_{el,PPO}$	15.3 kW
Gasifier		
Description	Symbol	Value
H_2 syngas fraction	x_{H_2}	28.49 %
H_2O syngas fraction	x_{H_2O}	9.91 %
CO syngas fraction	x_{CO}	26.33 %
CH_4 syngas fraction	x_{CH_4}	1.66 %
CO_2 syngas fraction	x_{CO_2}	17.2 %
N_2 syngas fraction	x_{N_2}	16.41 %
Syngas molar flow	$\dot{n}_{syngas}$	3.589 mol/s
Syngas higher heating value	$HHV_{syngas,db}$	7.55 MJ/Nm^3
Specific volumetric tar production	m_{tar,Nm^3}	0.27 g/Nm^3
Gasifier cold gas efficiency	η_{cold}	92.0 %
Average temperature of gasification	T	931 K
SOFC + MGT		
Description	Symbol	Value
Syngas molar flow to SOFC-MGT unit	$\dot{n}_{SOFC}$	3.545 mol/s
SOFC electrical power production	P_{SOFC}	184.20 kW
MGT electrical power production	P_{MGT}	68.33 kW
Total SOFC-MGT electrical power production	$P_{SOFC+MGT}$	252.53 kW
SOFC+MGT eletrical efficiency	$\eta_{SOFC+MGT}$	42.08 %
Overall system		
Description	Symbol	Value
Storage tank pressure range	p_{serb}	2.67-4.62 bar
Average electrical auxiliary consumption	P_{self}	42.01 kW_{el}
Average electrical total power production	P_{tot}	210.52 kW_{el}
Average total electrical efficiency	η_{tot}	32.81 %

Table 5: Case III (Gasifier + ZEO + SOFC + MGT) simulation results

Gasifier (see Case I)		
ZEO		
Description	Symbol	Value
H_2 syngas fraction after adsoption	x_{H_2}	25.36 %
CO syngas fraction after adsoption	x_{CO}	17.08 %
CH_4 syngas fraction after adsoption	x_{CH_4}	1.43 %
CO_2 syngas fraction after adsoption	x_{CO_2}	0.39 %
N_2 syngas fraction after adsoption	x_{N_2}	55.73 %
Syngas molar flow after adsoption	$\dot{n}_{syngas}$	4.065 mol/s
Syngas higher heating value after adsoption	$HHV_{syngas,db}$	5.9 MJ/Nm^3
Active zeolite mass for every regeration cycle	m_{zeo}	23.742 kg
SOFC + MGT		
Description	Symbol	Value
Syngas molar flow to SOFC-MGT unit	$\dot{n}_{SOFC}$	4.020 mol/s
SOFC electrical power production	P_{SOFC}	138.50 kW
MGT electrical power production	P_{MGT}	44.00 kW
Total SOFC-MGT electrical power production	$P_{SOFC+MGT}$	182.5 kW
SOFC+MGT electrical efficiency	$\eta_{SOFC+MGT}$	34.33 %
Overall system		
Description	Symbol	Value
Storage tank pressure range	p_{serb}	2.66-4.88 bar
Average electrical auxiliary consumption	P_{self}	33.76 kW_{el}
Average electrical total power production	P_{tot}	148.74 kW_{el}
Average total electrical efficiency	η_{tot}	22.87 %

Table 6: Case IV (PPO + Gasifier + ZEO + SOFC + MGT) simulation results

PPO module (see Case II)		
Gasifier (see Case II)		
ZEO		
Description	Symbol	Value
H_2 syngas fraction after adsoption	x_{H_2}	41.53 %
CO syngas fraction after adsoption	x_{CO}	32.54 %
CH_4 syngas fraction after adsoption	x_{CH_4}	2.21 %
CO_2 syngas fraction after adsoption	x_{CO_2}	0.43 %
N_2 syngas fraction after adsoption	x_{N_2}	23.30 %
Syngas molar flow after adsoption	$\dot{n}_{syngas}$	2.726 mol/s
Syngas higher heating value after adsoption	$HHV_{syngas,db}$	10.19 MJ/Nm^3
Active zeolite mass for every regeration cycle	m_{zeo}	20.244 kg
SOFC + MGT		
Description	Symbol	Value
Syngas molar flow to SOFC-MGT unit	$\dot{n}_{SOFC}$	2.696 mol/s
SOFC electrical power production	P_{SOFC}	184.70 kW
MGT electrical power production	P_{MGT}	51.80 kW
Total SOFC-MGT electrical power production	$P_{SOFC+MGT}$	236.50 kW
SOFC+MGT electrical efficiency	$\eta_{SOFC+MGT}$	38.41 %
Overall system		
Description	Symbol	Value
Storage tank pressure range	p_{serb}	2.66-4.15 bar
Average electrical auxiliary consumption	P_{self}	51.80 kW_{el}
Average electrical total power production	P_{tot}	194.53 kW_{el}
Average total electrical efficiency	η_{tot}	30.32 %

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