

This is a pre print version of the following article:

Analytical modeling of the shape memory effect in SMA beams with rectangular cross section under reversed pure bending / Radi, E.. - In: JOURNAL OF INTELLIGENT MATERIAL SYSTEMS AND STRUCTURES. - ISSN 1045-389X. - 32:18-19(2021), pp. 2214-2230. [10.1177/1045389X20988789]

Terms of use:

The terms and conditions for the reuse of this version of the manuscript are specified in the publishing policy. For all terms of use and more information see the publisher's website.

25/04/2024 05:43

(Article begins on next page)

Analytical modelling of the shape memory effect in SMA beams with rectangular cross section under reversed pure bending

Journal:	<i>Journal of Intelligent Material Systems and Structures</i>
Manuscript ID	JIM-20-366.R1
Manuscript Types:	Original Article
Date Submitted by the Author:	n/a
Complete List of Authors:	Radi, Enrico; Università degli Studi di Modena e Reggio Emilia Facoltà di Ingegneria Sede di Reggio Emilia, DISMI
Keyword:	Shape Memory, Analytical modeling, Pure bending, Cyclic loading, Rectangular cross-section, Martensite reorientation
Abstract:	<p>An analytical model is developed for a prismatic SMA beam with rectangular cross section subjected to alternating bending at temperature below the austenitic transformations. The loading path consists in a loading-unloading cycle under bending and reversed bending. Two opposite martensitic variants take place, whose volume fractions evolve linearly with the axial stress. Different Young's moduli are taken for the austenitic and martensitic phases. As the bending moment is increased, the martensitic transformation starts from the top and bottom and then it extends inwards. If the maximum applied bending moment is large enough, then the complete Martensitic transformation takes place at the upper and lower parts of the cross section. During unloading and reversed bending, reorientation of the Martensite variants into the opposite ones takes place starting from the boundary between the fully martensitic region and the intermediate transforming region. Special attention is devoted to calculate analytically the axial stress and Martensite variant distributions within the cross section at each stage of the process. A closed form moment-curvature relation is provided for loading and elastic unloading and in integral form for the rest of the process. The approach is then validated by comparison with analytical results available in the literature.</p>

SCHOLARONE™
Manuscripts

Analytical modelling of the shape memory effect in SMA beams with rectangular cross section under reversed pure bending

Enrico Radi

*Dipartimento di Scienze e Metodi dell'Ingegneria, Università di Modena e Reggio Emilia,
Via Amendola 2, I-42122 Reggio Emilia, Italy. Email: enrico.radi@unimore.it*

Abstract. An analytical model is developed for a prismatic SMA beam with rectangular cross section subjected to alternating bending at temperature below the austenitic transformations. The loading path consists in a loading-unloading cycle under bending and then under reversed bending. Two opposite martensitic variants take place, whose volume fractions evolve linearly with the axial stress. Different Young's moduli are taken for the austenitic and martensitic phases. As the bending moment is increased, the martensitic transformation starts from the top and bottom and then it extends inwards. If the maximum applied bending moment is large enough, then the complete Martensitic transformation takes place at the upper and lower parts of the cross section. During unloading and the following reversed bending, reorientation of the Martensite variant into the opposite one takes place starting from the boundary between the fully martensitic region and the intermediate transforming region. Special attention is devoted to calculate analytically the axial stress and Martensite variant distributions within the cross section at each stage of the process. A closed form moment-curvature relation is provided for loading and elastic unloading and in integral form for the rest of the process. The approach is then validated by comparison with analytical results available in the literature.

Keywords: Analytical modeling, Pure bending, Rectangular cross-section, Shape-memory alloy, Phase transformation, Martensite reorientation, Cyclic loading.

1. Introduction

Due to their peculiar characteristics, such as the shape memory effect and the superelastic behavior, SMA beams, rods and wires are effectively employed in smart sensors and actuators, as well as in energy dissipating devices for the control of structural vibrations due to wind or seismic excitations. Indeed, a large hysteresis loop similar to that exhibited by ductile metals is observed in a martensitic SMA bar cyclically loaded at low temperatures, which is due to the reorientation process between

1
2 martensitic variants rather than to phase transformation or dislocation glide mechanisms. As a
3 consequence, SMAs are able to display a much higher fatigue resistance than plastically deformed
4 metals and thus they can efficiently replace elastic-plastic hysteretic devices in passive control and
5 seismic retrofit of building and bridges (Dolce et al., 2000; Dolce and Cardone, 2001; DesRoche and
6 Smith, 2004; Song et al., 2006; Ozbulut et al., 2011; Fang and Wang, 2020). A practical example of
7 application of the SMA energy dissipation properties is given by the innovative yielding dissipater
8 device recently proposed by Zibasokhan et al. (2019) for seismic protection of concentrically braced
9 structures, which is able to transform the axial force into pure bending in the dissipating plates. The
10 device is fabricated by a set of ductile steel plates under pure bending, and it can be efficiently
11 improved by exploiting the shape memory effect of SMA.

12
13 Usually, dissipating SMA device are cyclically loaded alternately under tension and compression.
14 However, the occurring of buckling in slender SMA bars and wires under compression restricts their
15 applications and requires additional devices to prevent it. Therefore, the special properties of SMA
16 bars are better exploited under bending rather than under tension and compression. In order to
17 overcome the buckling problem, Choi et al. 2009 proposed the use of a superelastic SMA bars in
18 bending as seismic dampers and restrainers for bridges and proved their ability in reducing the
19 openings at the internal hinges and the pounding force on abutments. Later, Choi et al. (2019)
20 investigated the self-centering and damping capacity of SMA bars in bending. They showed that a
21 martensitic SMA bar exploiting the shape memory effect displays a higher energy dissipation and
22 thus a better seismic efficiency than a superelastic SMA bar, while the latter provides better
23 displacement recovery and self-centering capability. Although a residual strain usually remains in a
24 martensitic SMA bar after unloading, it can be easily removed upon heating.

25
26 The dissipation capabilities of SMA seismic devices under cyclic loading of alternating sign
27 remarkably increase if the shape memory effect is exploited, rather than the superelastic behavior.
28 Indeed, a larger amount of energy is dissipated during each cyclic reorientation process between
29 positive and negative martensitic variants if no intermediate austenitic transformation is triggered
30 (Wilson and Wesolowsky, 2005). In these applications, a clear understanding of the fatigue behavior
31 of SMA is necessary to improve their safety. To this aim an accurate evaluation of the maximum
32 stress level under cyclic loading of alternating sign becomes highly important.

33
34 The problem of bending of a SMA beam was investigated numerically by many authors by means of
35 finite element simulation, e.g. Auricchio and Sacco (1997), Auricchio et al. (2011), and Poorasadion,
36 et al. (2015) or by numerical procedures based on the partition of the beam cross-section into a number
37 of thin layers (De la Flor et al., 2011). Analytical approaches have been also tempted by some authors,
38 but they are limited to a loading-unloading cycle and have not been extend to reversed loading. In
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60

1 particular, Mirzaeifar et al. (2013) provided explicit expressions for the stress and martensitic volume
2 fraction distributions both in circular and rectangular cross sections upon a superelastic loading-
3 unloading cycle and used these expressions for obtaining closed-form relations between bending
4 moment and curvature. They also took into account for the tension-compression asymmetry on the
5 bending response of SMAs and compared the theoretical predictions with the results of three-point
6 bending tests on an SMA beam and finite element investigations. Ostadrahimi et al. (2015) presented
7 an analytical solution for pure bending of SMA beams with rectangular cross section as well as
8 symmetric behavior in tension and compression at high (pseudo-elasticity) and low (shape memory
9 effect) temperatures. They assumed the same Young's modulus for both phases, thus obtaining
10 piecewise linear stress variation within the cross section. Eshghinejad and Elahinia (2015) also
11 derived an analytical expression for the bending moment in a superelastic SMA beam loaded at the
12 tip and evaluated its deflection by assuming linear stress-strain relations in all regions and using a
13 semi-analytical approach. Viet et al. (2018) worked out an analytical solution for the problem of SMA
14 cantilever beams subjected to tip load throughout a full loading-unloading cycle. The analysis was
15 based on Timoshenko beam theory and was later extended to account for tensile-compressive
16 asymmetry in SMA response (Viet et al., 2019). **The asymmetric tension-compression behavior of**
17 **the SMA has been observed and modelled under direct bending by Rejzner et al. (2002), Fahimi et**
18 **al., (2019), and Viet et al. (2019).**

19 Most of these analyses investigate the superelastic behavior of SMA beams in order to exploit the
20 self-centering mechanism, and thus they are restricted to temperatures higher than the start
21 temperature of the austenitic transformation A_s . In this case, the reverse austenitic transformation is
22 completed before the complete unloading. Therefore, these works do not take into consideration the
23 transformation between the two Martensite variants, which may occur during unloading and reversed
24 loading at temperature lower than A_s . The shape memory effect of SMA beams, **which is essential for**
25 **application to dampers and dissipating devices**, is indeed observed under cyclic loading at
26 temperature lower than the start temperature of the austenitic transformation A_s , e.g. for the NiTiInol
27 alloy (Ni₅₅Ti) considered by Brinson (1993) this effect occurs at room temperature. In this case,
28 during unloading the axial stress changes its sign in some parts of the beam cross section and it may
29 trigger the Martensite **reorientation** process. Such transformation then continues under reversed
30 bending. However, no complete and detailed analytical study of a SMA beam under reversed bending
31 has been performed up to now. Recently, Radi (2020) performed an analytical investigation of the
32 shape memory effect in SMA circular rod under cyclic torsional loading by adopting a **3D** SMA
33 constitutive model that incorporates two opposite Martensite variants. He also analyzed the
34 transformation and reorientation processes into multiple martensitic variants in a previous work on
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60

1 the response of SMA thick-walled cylinders under internal pressure (Radi, 2018).

2
3 The present study extends the previous investigations to pure bending of SMA beams with rectangular
4 cross section. In particular, closed-form solutions are obtained here for the axial stress and distribution
5 of Martensite volume fractions at each step of a cyclic bending process of alternating sign, performed
6 at constant temperature T lower than A_s . These analytical results are then used for calculating the
7 moment-curvature relation for a SMA beam cross section subjected to direct and reversed bending.
8

9 This achievement is possible because a simple 1D phenomenological SMA constitutive model is
10 adopted here, which assumes a linear evolution law with the axial stress for both Martensite variants.
11

12 **The simplifications adopted here preserve the basic features of SMA materials and they are required**
13 **for achieving a closed form solution to the problem of reversed pure bending of SMA beams.**
14 **Obviously, more refined constitutive models have been proposed in the last years. However, they**
15 **necessarily require the adoption of numerical procedures, also for simulating simple mechanical**
16 **problems.** The constitutive model developed here originates from those proposed for multi-variants
17 Martensite (Brinson, 1993; Brinson and Huang, 1996; Govindjee and Kasper, 1997, 1999; De la Flor
18 et al., 2011; Marfia and Rizzoni, 2013; Rizzoni et al., 2013; Rizzoni and Marfia, 2015; Fahimi et al.,
19 2019) and recently adopted by Radi (2020) for modelling cyclic torsional loading. **It is able to**
20 **simulate the Martensite reorientation process occurring when a transition from tensile to compressive**
21 **stress, or vice versa, takes place. Here, the Martensite reorientation process under reverse bending is**
22 **taken into consideration analytically for the first time.**

23 **The constitutive model is the 1D reduction of a 3D model already used in Radi (2018). It is**
24 **sufficiently accurate for the present analysis because the stress field under pure bending is 1D. An**
25 **equivalent reduction is performed also in other investigations of the pseudoelastic effect in SMA**
26 **beam under bending, e.g. in Mirzaeifar et al. (2012), Ostadrahimi et al. (2015), Viet et al. (2018,**
27 **2019). Obviously, a 3D strain field arises in the beam so that the beam cross section can change his**
28 **shape by expanding in the compressed zone and contracting in the tensile one, due also to the**
29 **martensitic transformation and reorientation. This effect can be explicitly considered in the present**
30 **analysis by specifying the strain components in the plane of the cross section under 1D stress field.**
31 **However, the analysis has been focused here on the derivation of the analytical relation between**
32 **bending moment and curvature during the full cyclic process taking into account for martensitic**
33 **reorientation, rather than focusing on the cross section deformation.**

34 Since no variation of temperature due to the thermal-mechanical coupling of SMA has been
35 considered, then the isothermal solutions found here holds for very slow loading-unloading rates only.
36 The fully coupled thermal-mechanical behaviors of SMA beams subjected to cyclic loading
37 conditions is generally very complicated to be investigated analytically. Due to the complex heat
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60

diffusion process it would necessary require the adoption of a purely numerical procedure.

This paper is organized as follows. The 1D constitutive model for SMA beams under pure bending is presented in Section 2. Different elastic Young's moduli are considered for the two phases and the elastic behavior of the SMA is assumed to depend on the volume fraction of Austenite and Martensite according to the Reuss scheme for the elastic response of a composite. Moreover, the model can simulate the martensitic reorientation process during unloading and reversed bending. Closed form solutions for the axial stresses and Martensite fractions within the cross section at each step of the first loading-unloading process are presented in Section 3, together with the corresponding relation between the applied bending moment and the beam curvature obtained by integrating the contribution of the axial stress within the cross-section. Similar closed form solutions are obtained in Section 4 for the reversed bending and subsequent elastic unloading. The results are then plotted in Section 5 and the effects of the constitutive parameters on the distribution of axial stresses and Martensite volume fractions within the cross-section are discussed therein. The analytical results are then validated against some analytical results for a loading-unloading cycle provided in the technical literature. Unfortunately, neither analytical nor experimental results can be found for the Martensite reorientation process under reversed bending loading. Conclusions are then drawn in Section 6. With respect to previous similar works, **the fully analytical solution presented here significantly extends the range of validity to a full cycle of alternating sign of the applied bending moment.** The accurate knowledge of the full stress field during the complete process is indeed the only way to ensure good limitation of the stress level for the safe and accurate design of SMA devices under bending.

2. 1D constitutive model for a SMA beam under pure bending

Let x and y denote the principal centroidal axes of the rectangular cross section of a prismatic beam having width b and height $2a$. According to the classical Euler-Bernoulli theory, the axial strain ε under pure bending is proportional to the beam curvature χ and is a linear function of the distance y from the neutral axis of the cross section, which coincides with the x -axis, namely

$$\varepsilon = \chi y, \quad \text{for } -a \leq y \leq a. \quad (2.1)$$

By assuming tension-compression symmetry for simplicity, a symmetric distribution of the axial stress σ along the height is expected, so that the neutral fibre always coincides with the centroidal x -axis. Therefore, reference is made only to the upper half of the cross section ($y \geq 0$) in the following. The bending moment M_x applied to the beam cross section can be calculated by taking the moment about the neutral axis of the stress distribution along the height, namely

$$M_x = 2b \int_0^a \sigma y dy. \quad (2.2)$$

According to Govindjee and Kasper (1997, 1999) and Rizzoni and Marfia (2015), let ξ^+ and ξ^- denote the volume fractions of Martensite stretched in the positive (tensile) and negative (compressive) directions, respectively. Then, the effective volume fraction of Martensite ξ is defined by the difference $\xi = \xi^+ - \xi^-$ and the total volume fraction of Martensite is given by the sum $\xi_{\text{tot}} = \xi^+ + \xi^-$, where $-1 \leq \xi \leq 1$ and $0 \leq \xi_{\text{tot}} \leq 1$. Moreover, the 1D rate constitutive relationships between the axial stress σ , the axial strain ε in (2.1) and the effective volume fraction of Martensite ξ are assumed in the following linear form

$$\varepsilon = \frac{\sigma}{E(\xi_{\text{tot}})} + \varepsilon_L \xi, \quad \xi = \begin{cases} \frac{1 + \xi_0}{\sigma_f - \sigma_s} \sigma & \text{for } |\sigma_s| \leq |\sigma| \leq |\sigma_f|, \\ 0 & \text{otherwise,} \end{cases} \quad (2.3)$$

where ε_L is the maximum transformation strain attained under uniaxial loading when the solid is composed of fully oriented Martensite, ξ_0 is the effective volume fraction Martensite at the beginning of each transformation, $E(\xi_{\text{tot}})$ is the Young's modulus of the SMA material, which is assumed to depend on the total Martensite volume fraction according to the Reuss scheme for the elastic response of a composite, namely

$$\frac{1}{E(\xi_{\text{tot}})} = \frac{1 - \xi_{\text{tot}}}{E_A} + \frac{\xi_{\text{tot}}}{E_M}, \quad (2.4)$$

being E_A and E_M the Young's moduli of the two phases. In eqn (2.3)₂, σ_s and σ_f denote the critical axial stresses for the start and finish martensitic transformations at temperature T , respectively, and they are defined by

$$\sigma_s = \sigma_s^{cr} + C_M (T - M_s), \quad \sigma_f = \sigma_f^{cr} + C_M (T - M_s), \quad (2.5)$$

where C_M is the slope of the martensitic transformation lines in the uniaxial stress-temperature phase diagram sketched in Fig. 1, and σ_s^{cr} and σ_f^{cr} are the uniaxial critical stresses for the start and finish of the martensitic transformation at temperature M_s (Brinson and Huang, 1996).

Before loading, the SMA beam is assumed in the austenitic phase, so that $\xi = \xi_{\text{tot}} = \xi_0 = 0$. As the beam is loaded in bending, a single Martensite variant is produced in the upper half of the cross section, according to the integrated form of the evolution law (2.3)₂

$$\xi = \xi^+ = \begin{cases} 0, & \text{for } \sigma \leq \sigma_s, \\ \frac{\sigma - \sigma_s}{\sigma_f - \sigma_s}, & \text{for } \sigma_s \leq \sigma \leq \sigma_f, \\ 1, & \text{for } \sigma \geq \sigma_f. \end{cases} \quad (2.6)$$

During unloading and reversed bending, the effective and total Martensite volume fractions follows from the integration of the linear evolution law (2.3)₂ as

$$\xi = \xi^+ - \xi^- = \begin{cases} \xi_0, & \text{for } \sigma \geq -\sigma_s, \\ \xi_0 + (1 + \xi_0) \frac{\sigma + \sigma_s}{\sigma_f - \sigma_s}, & \text{for } -\sigma_f \leq \sigma \leq -\sigma_s, \\ -1, & \text{for } \sigma \leq -\sigma_f, \end{cases} \quad (2.7)$$

and

$$\xi_{\text{tot}} = \xi^+ + \xi^- = \begin{cases} \xi_0, & \text{for } \sigma \geq -\sigma_s \\ 1 - (1 - \xi_0) \frac{\sigma + \sigma_f}{\sigma_f - \sigma_s}, & \text{for } -\sigma_f \leq \sigma \leq -\sigma_s \\ 1, & \text{for } \sigma \leq -\sigma_f \end{cases} \quad (2.8)$$

respectively, where ξ_0 is the effective volume fraction Martensite at the beginning of each stage. Eqns (2.7) and (2.8) agree with the 1D constitutive relations for the multivariant Martensite volume fractions considered by Govindjee and Kasper (1997, 1999), De la Flor (2011), Rizzoni et al. (2012) and Radi (2020).

3. Loading-unloading cycle under pure bending

In the initial state of Austenite, the beam displays linear elastic behavior and thus the axial stress within the cross section is given by the following linear function of the beam curvature

$$\frac{\sigma}{\sigma_s} = \kappa \frac{y}{a}, \quad \text{for } 0 \leq \kappa \leq 1, \quad (3.1)$$

where

$$\kappa = \frac{E_A}{\sigma_s} \chi a, \quad (3.2)$$

is the normalized beam curvature. Consequently, the martensitic transformation starts at the top of the cross section, namely at $y = a$, when the axial stress attains the critical stress σ_s therein, namely

for $M_x = M_s$, where

$$M_s = \frac{2}{3} b a^2 \sigma_s. \quad (3.3)$$

Let

$$\mu = \frac{M_x}{M_s} = \frac{3}{a^2} \int_0^a \frac{\sigma}{\sigma_s} y dy, \quad (3.4)$$

denotes the normalized bending moment applied to the cross section, then the following normalized linear relation holds between bending moment and beam curvature under pure elastic loading

$$\mu = \kappa, \quad \text{for } 0 \leq \kappa \leq 1. \quad (3.5)$$

If the bending moment is increased, then the martensitic transformation takes place at the upper part of the cross section, namely at $y_s \leq y \leq a$, where

$$y_s = \frac{a}{\kappa}, \quad (3.6)$$

and it propagates inward. According to eqns (2.3) and (2.4), the stress and beam curvature in the transforming region are related by the linear rate relation

$$\frac{\sigma_s}{E_A} \frac{y}{a} \kappa = \left(\frac{1-\xi}{E_A} + \frac{\xi}{E_M} + \frac{\varepsilon_L}{\sigma_f - \sigma_s} \right) \kappa, \quad \text{for } -y_s \leq y \leq y_s, \quad (3.7)$$

which can be integrated starting from the occurring of the martensitic transformation at height y , by using eqn (2.6), namely

$$\kappa \frac{y}{a} - 1 = \frac{1}{\sigma_s} \int_{\sigma_s}^{\sigma} \left(1 + \delta - \frac{\Gamma}{\beta} + \frac{\Gamma}{\beta} \frac{\sigma}{\sigma_s} \right) d\sigma, \quad \text{for } y_s \leq y \leq a, \quad (3.8)$$

where the following non-dimensional parameters have been introduced

$$\beta = \frac{\sigma_f - \sigma_s}{\sigma_s}, \quad \delta = \frac{\varepsilon_L E_A}{\sigma_f - \sigma_s}, \quad \Gamma = \frac{E_A - E_M}{E_M}. \quad (3.9)$$

The integration of eqn (3.8) then provides a quadratic equation for the axial stress σ

$$\left(1 + \delta - \frac{\Gamma}{\beta} \right) \left(\frac{\sigma}{\sigma_s} - 1 \right) + \frac{\Gamma}{2\beta} \left(\frac{\sigma^2}{\sigma_s^2} - 1 \right) = \kappa \frac{y}{a} - 1, \quad \text{for } y_s \leq y \leq a, \quad (3.10)$$

which admits the following solution for the axial stress within the cross section

$$\frac{\sigma}{\sigma_s} = \begin{cases} \kappa \frac{y}{a}, & \text{for } 0 \leq y \leq y_s, \\ 1 + B \left[\sqrt{1 + \frac{2}{B_1} \left(\kappa \frac{y}{a} - 1 \right)} - 1 \right], & \text{for } y_s \leq y \leq a, \end{cases} \quad (4.10)$$

where

$$B = \frac{\beta}{\Gamma} (1 + \delta), \quad B_1 = \frac{\beta}{\Gamma} (1 + \delta)^2. \quad (3.11)$$

According to eqns (2.6) and (4.10), the distribution of the Martensite volume fraction within the cross section is given by

$$\xi = \begin{cases} 0, & \text{for } 0 \leq y \leq y_s, \\ \frac{B}{\beta} \left[\sqrt{1 + \frac{2}{B_1} \left(\kappa \frac{y}{a} - 1 \right)} - 1 \right], & \text{for } y_s \leq y \leq a. \end{cases} \quad (3.12)$$

Both the axial stress and the volume fraction of Martensite display a nonlinear variation with the y coordinate in the transforming region for $y_s \leq y \leq a$, which becomes linear for $\Gamma = 0$, namely for equal Young's moduli of the two phases.

A further increment of the bending moment applied to the cross section then causes the occurring of the complete martensitic transformation at $y = a$, where $\xi = 1$. Correspondingly, the normalized beam curvature and the height of start martensitic transformation are given by

$$\kappa_1 = 1 + \left(\frac{\Gamma}{2} + 1 + \delta \right) \beta, \quad y_1 = \frac{a}{\kappa_1}, \quad (3.13)$$

as they follow from eqns (3.12) and (3.6), respectively. The introduction of the axial stress (4.10) in the balance condition (3.4)₁ then yields the normalized moment-curvature relation, which holds during this stage of loading

$$\mu(\kappa) = \frac{1}{5\kappa^2} \left[5 + B B_1 (B_1 - 5) - \frac{15}{2} (B - 1) (\kappa^2 - 1) - \frac{B}{\sqrt{B_1}} (B_1 - 2 - 3\kappa)(B_1 - 2 + 2\kappa)^{3/2} \right], \quad (3.14)$$

namely for $1 \leq \kappa \leq \kappa_1$.

The axial stress at $y = a$ attains the critical value σ_f under the normalized bending moment $\mu_1 = \mu(\kappa_1)$. If the bending moment is increased, then the fully transformed region propagates inwards. Within this region, the rate eqn (3.7) can be integrated starting from the occurring of the complete martensitic transformation at height y , by using the conditions $\xi = 1$, thus obtaining

$$\frac{\sigma - \sigma_f}{\sigma_s} = \frac{1}{1 + \Gamma} \left(\kappa \frac{y}{a} - \kappa_1 \right), \quad \text{for } y_f \leq y \leq a, \quad (3.15)$$

where the height

$$y_f = \frac{\kappa_1}{\kappa} a, \quad (3.16)$$

denotes the front of finish martensitic transformation, where $\sigma = \sigma_f$.

During the last stage of the loading process, the cross section is partitioned into an inner purely austenitic inner region for $|y| \leq y_s$, an intermediate transforming region for $y_s \leq |y| \leq y_f$, and an outer

purely martensitic region for $y_f \leq |y| \leq a$. From eqn (4.10), (3.12), and (3.15), the corresponding distributions of the axial stress and Martensite volume fraction within the upper half of the cross section are given by

$$\frac{\sigma}{\sigma_s} = \begin{cases} \kappa \frac{y}{a} & \text{for } 0 \leq y \leq y_s, \\ 1 + B \left[\sqrt{1 + \frac{2}{B_1} \left(\kappa \frac{y}{a} - 1 \right)} - 1 \right] & \text{for } y_s \leq y \leq y_f, \\ 1 + \beta + \frac{1}{1 + \Gamma} \left(\kappa \frac{y}{a} - \kappa_1 \right) & \text{for } y_f \leq y \leq a, \end{cases} \quad (3.17)$$

and

$$\xi = \begin{cases} 0 & \text{for } 0 \leq y \leq y_s, \\ \frac{B}{\beta} \left[\sqrt{1 + \frac{2}{B_1} \left(\kappa \frac{y}{a} - 1 \right)} - 1 \right] & \text{for } y_s \leq y \leq y_f, \\ 1 & \text{for } y_f \leq y \leq a, \end{cases} \quad (3.18)$$

respectively. Therefore, during the loading process both the axial stress and the Martensite volume fraction vary linearly with y across the inner austenitic and the outer martensitic regions, and display a weak nonlinear variation within the intermediate transforming region.

During the last stage of the loading process, the normalized bending moment μ then follows from (3.4)₁ and (3.17) as a nonlinear function of the normalized beam curvature κ

$$\mu(\kappa) = \frac{C}{\kappa^2} + \frac{\kappa}{1 + \Gamma} + \frac{3}{2} \left(1 + \beta - \frac{\kappa_1}{1 + \Gamma} \right), \quad \text{for } \kappa_1 \leq \kappa \leq \kappa_{\max}, \quad (3.19)$$

where

$$C = \frac{\kappa_1^3}{2(1 + \Gamma)} - \frac{1}{2} [1 - 3B + 3(B + \beta)\kappa_1^2] - \frac{B}{5} \sqrt{1 + \frac{2}{B_1} (\kappa_1 - 1) (B_1 - 3\kappa_1 - 2)(B_1 + 2\kappa_1 - 2)} + \frac{B}{5} B_1 (B_1 - 5), \quad (3.20)$$

Note that for equal Young's moduli, namely for $\Gamma = 0$, the distributions of axial stress (3.17) and effective Martensite volume fraction (3.18) within each region of the upper half of the cross section become linear in y , in agreement with the findings of Ostadrahimi et al. (2015), namely

$$\frac{\sigma}{\sigma_s} = \begin{cases} \frac{y}{a} \kappa, & \text{for } 0 \leq y \leq y_s, \\ 1 + \frac{1}{1+\delta} \left(\frac{y}{a} \kappa - 1 \right), & \text{for } y_s \leq y \leq y_f, \\ 1 + \beta + \left(\frac{y}{a} \kappa - \kappa_1 \right), & \text{for } y_f \leq y \leq a, \end{cases} \quad (3.21)$$

and

$$\xi = \begin{cases} 0, & \text{for } 0 \leq y \leq y_s, \\ \frac{1}{\beta(1+\delta)} \left(\frac{y}{a} \kappa - 1 \right), & \text{for } y_s \leq y \leq y_f, \\ 1, & \text{for } y_f \leq y \leq a, \end{cases} \quad (3.22)$$

where y_s and y_f are given by (3.6) and (3.16) calculated for $\Gamma = 0$.

Let $\kappa_{\max} = a/y_s$ and $\mu_{\max} = \mu(\kappa_{\max})$ denote the normalized beam curvature at the end of the loading process and the corresponding normalized bending moment, respectively. Moreover, let σ_{\max} and ξ_{\max} denote the distributions along the height of the beam cross section of axial stress and volume fraction of Martensite at the same stage, which follow from (3.17) and (3.18) for $\kappa = \kappa_{\max}$, respectively.

3.1 Unloading

The Martensite distribution does not vary during elastic unloading as well as the heights y_s and y_f , which are given by (3.6) and (3.16) for $\kappa = \kappa_{\max}$. The integration of the rate constitutive equation (2.3) for $\xi = \xi_{\max}(y)$, and thus $\dot{\xi} = 0$, by using the Reuss scheme (2.4), then yields the axial stress during elastic unloading as a function of the normalized curvature

$$\frac{\sigma}{\sigma_s} = \frac{\sigma_{\max}}{\sigma_s} - \frac{\kappa_{\max} - \kappa}{1 + \Gamma \xi_{\max}} \frac{y}{a}, \quad \text{for } 0 \leq y \leq a. \quad (3.23)$$

The corresponding moment-curvature relation follows from the introduction of the stress field (3.23) in the balance condition (3.4)₁

$$\mu = \mu_{\max} - (\kappa_{\max} - \kappa) \frac{3}{a^3} \int_0^a \frac{y^2}{1 + \Gamma \xi_{\max}} dy. \quad (3.24)$$

The change of variable $t = 1 + \Gamma \xi_{\max}(y)$ in the integral in eqn (3.24), by using (3.18) for $\xi_{\max}(y)$, then gives

$$\mu = \mu_{\max} - (\kappa_{\max} - \kappa) m, \quad (3.25)$$

where

$$m = \frac{1}{\kappa_{\max}^3} \left\{ 1 + \frac{\kappa_{\max}^3 - \kappa_1^3}{1 + \Gamma} + \frac{3\beta^3}{4\Gamma^3} \int_1^{1+\Gamma} \left[(t + \delta)^2 - (1 + \delta)^2 + 2 \frac{\Gamma}{\beta} \right]^2 \left(1 + \frac{\delta}{t} \right) dt \right\}, \quad (3.26)$$

and the integral in (3.26) is calculated analytically in Appendix A. Note that $m \rightarrow 1$ as $\Gamma \rightarrow 0$.

The elastic incremental behavior of the bar ends when the axial stress (3.23) reaches the negative critical stress $-\sigma_s$ at $y = y_f$, where $\xi_{\max} = 1$ and $\sigma_{\max} = \sigma_f$, namely for $\kappa = \kappa_2$ and $\mu = \mu_2$, where

$$\kappa_2 = \kappa_{\max} - (1 + \Gamma)(2 + \beta) \frac{\kappa_{\max}}{\kappa_1}, \quad \mu_2 = \mu_{\max} - (1 + \Gamma)(2 + \beta) \frac{\kappa_{\max}}{\kappa_1} m. \quad (3.27)$$

Indeed, Martensite reorientation takes place before the complete unloading of the cross section if $\mu_2 > 0$, namely if the maximum beam curvature κ_{\max} is larger than a limit value κ_{\lim} given by the largest positive real root of the following cubic equation obtained from the introduction of eqns (3.19) and (3.26) in (3.27)₂:

$$\left(\frac{1}{1 + \Gamma} - \frac{2 + \beta}{\kappa_1} \right) \kappa_{\lim}^3 + \frac{3}{2} \left(1 + \beta - \frac{\kappa_1}{1 + \Gamma} \right) \kappa_{\lim}^2 = (2 + \beta) \left[\frac{1 + \Gamma}{\kappa_1} \left(1 + \frac{3\beta^3}{4\Gamma^3} I \right) - \kappa_1^2 \right] - C, \quad (3.28)$$

where the constant C is defined in (3.20) and I denotes the integral calculated in Appendix A.

If $\kappa_{\max} < \kappa_{\lim}$ then the unloading process is entirely elastic and when the bending moment is completely released the residual beam curvature is

$$\kappa_{\text{res}} = \kappa_{\max} - \mu_{\max} / m. \quad (3.29)$$

Conversely, if $\kappa_{\max} > \kappa_{\lim}$ then Martensite reorientation takes place before complete unloading according to eqn (2.7) for $\xi_0 = \xi_{\max}$. In this case, two new regions where Martensite reorientation occurs spread out from the boundary between the intermediate transforming regions and the fully martensitic outer regions at $y = y_f$. Let us denote with y' and y'' the lower and upper heights delimiting these new regions, with $y' \leq y_f \leq y''$, which are defined by the condition that the axial stress at $y = y'$ and $y = y''$ must coincide with the negative critical stress $-\sigma_s$. Therefore, the following two relations between κ , y' and y'' follow from eqn (3.23)

$$\sigma_{\max}(y') - \sigma_s \frac{\kappa_{\max} - \kappa}{1 + \Gamma \xi_{\max}(y')} \frac{y'}{a} = -\sigma_s, \quad \sigma_{\max}(y'') - \sigma_s \frac{\kappa_{\max} - \kappa}{1 + \Gamma} \frac{y''}{a} = -\sigma_s. \quad (3.30)$$

The introduction of eqn (3.21) for $\sigma_{\max}(y')$ with $\kappa = \kappa_{\max}$ in eqn (3.30)₁ then yields the normalized beam curvature κ as a function of the height y' :

$$\kappa = \kappa_{\max} - [2 + \beta \xi_{\max}(y')] [1 + \Gamma \xi_{\max}(y')] \frac{R}{y'}, \quad \text{for } y' \leq y \leq y_f. \quad (3.31)$$

By using eqn (3.22) for $\xi_{\max}(y')$ with $\kappa = \kappa_{\max}$, eqn (3.31) can be explicitly solved for y' as a function of the normalized beam curvature κ

$$\frac{y'}{a} = \left(\frac{1+2\delta}{\Gamma} - \frac{2}{\beta} \right) \frac{(\delta\beta - 2\Gamma)\kappa_{\max} - (1+\delta)\kappa\beta}{(\kappa_{\max} + \kappa)^2} \left\{ 1 - \sqrt{1 - \frac{2\beta\Gamma(\kappa_{\max} + \kappa)^2}{[(\delta\beta - 2\Gamma)\kappa_{\max} - (1+\delta)\beta\kappa]^2}} \right\}, \quad (3.32)$$

where $y_s \leq y' \leq y_f$. In the same way, the introduction in eqn (3.30)₂ of the stress field $\sigma_{\max}(y'')$ obtained from (3.17) for $\kappa = \kappa_{\max}$ then yields the height y'' as a function of κ

$$\frac{y''}{a} = \frac{1}{\kappa} [\kappa_1 - (1 + \Gamma)(\beta + 2)], \quad (3.33)$$

where $y_f \leq y'' \leq a$. Let us consider a material point at height y laying between y' and y_f . According to eqn (3.31), the reorientation of the primary Martensite variant into the opposite one starts there when $\kappa = \kappa_y$, where

$$\kappa_y = \kappa_{\max} - [2 + \beta \xi_{\max}(y)][1 + \Gamma \xi_{\max}(y)] \frac{a}{y}, \quad \text{for } y' \leq y \leq y_f. \quad (3.34)$$

Therefore, by subtracting eqn (3.34) from eqn (3.31) one has

$$\kappa_y - \kappa = [2 + \beta \xi_{\max}(y)][1 + \Gamma \xi_{\max}(y)] \frac{a}{y'} - [2 + \beta \xi_{\max}(y)][1 + \Gamma \xi_{\max}(y)] \frac{a}{y}, \quad \text{for } y' \leq y \leq y_f. \quad (3.35)$$

At the same time, for $\kappa = \kappa_y$, Martensite reorientation also starts at another material point at height y ranging between y_f and y'' , and thus κ_y must satisfy the following condition also

$$\kappa_y = [\kappa_1 - (1 + \Gamma)(\beta + 2)] \frac{a}{y}, \quad \text{for } y_f \leq y \leq y'', \quad (3.36)$$

according to (3.33). Then, eqns (3.33) and (3.36) yield

$$\kappa_y - \kappa = [\kappa_1 - (1 + \Gamma)(\beta + 2)] \left(\frac{a}{y} - \frac{a}{y''} \right), \quad \text{for } y_f \leq y \leq y''. \quad (3.37)$$

The introduction of relations (2.4) and (3.9) in the rate constitutive eqns (2.3) then yields the following rate equation,

$$E_A y \dot{\kappa} = [1 + \xi_{\text{tot}} \Gamma + \delta(1 + \xi_{\max})] \dot{\sigma}, \quad \text{for } y' \leq y \leq y'', \quad (3.38)$$

which holds for a material point at coordinate y experiencing the reorientation of the Martensite variant. Integration of the rate constitutive equation (3.38) from the start of the martensitic reorientation at height y , by using relations (2.8) for ξ_{tot} with $\xi_0 = \xi_{\max}$, then gives

$$\frac{y}{a} (\kappa - \kappa_y) = \frac{1}{\sigma_s} \int_{-\tau_s}^{\tau} \left[1 + \Gamma + \delta(1 + \xi_{\max}) - \Gamma(1 - \xi_{\max}) \frac{\sigma + \sigma_f}{\sigma_f - \sigma_s} \right] d\sigma, \quad \text{for } y' \leq y \leq y'', \quad (3.39)$$

being $-\sigma_s$, κ_y and ξ_{\max} the axial stress, the normalized beam curvature and the total volume fraction of Martensite at the beginning of the reorientation process, respectively. The calculation of the definite integral in (3.39) then yields the following quadratic equation for the axial stress σ during the Martensite reorientation process

$$\frac{\sigma^2}{\sigma_s^2} + 2 \left[1 - \beta \frac{1 + \delta + (\delta - \Gamma) \xi_{\max}}{\Gamma (1 - \xi_{\max})} \right] \left(\frac{\sigma}{\sigma_s} + 1 \right) - 1 - \frac{2\beta}{\Gamma} \left(\frac{\kappa_y - \kappa}{1 - \xi_{\max}} \right) \frac{y}{a} = 0, \quad \text{for } y' \leq y \leq y_f, \quad (3.40)$$

Therefore, the admissible solution of eqn (3.40) for $0 < \xi_{\max} < 1$ is

$$\frac{\sigma}{\sigma_s} = -1 - \beta \frac{1 + \delta + (\delta + \Gamma) \xi_{\max}}{\Gamma (1 - \xi_{\max})} \left\{ \sqrt{1 + \frac{2\Gamma (1 - \xi_{\max})(\kappa_y - \kappa)}{\beta [1 + \delta + (\delta + \Gamma) \xi_{\max}]^2} \frac{y}{a}} - 1 \right\}, \quad \text{for } y' \leq y \leq y_f. \quad (3.41)$$

The terms $\kappa_y - \kappa$ and y' follow from eqns (3.35) and (3.32), respectively, in terms of the beam curvature κ .

For $\xi_{\max} = 1$, eqn (3.39) provides the following result for the axial stress

$$\frac{\sigma}{\sigma_s} = -1 - \frac{\kappa_y - \kappa}{1 + \Gamma + 2\delta} \frac{y}{a}, \quad \text{for } y_f \leq y \leq y'', \quad (3.42)$$

where the quantities $\kappa_y - \kappa$ and y'' are given in eqns (3.37) and (3.33) in terms of κ .

During this stage, the rest of the cross section displays only elastic behavior. Therein, the axial stress is thus given by

$$\frac{\sigma}{\sigma_s} = \frac{\sigma_{\max}}{\sigma_s} - \frac{\kappa_{\max} - \kappa}{1 + \Gamma \xi_{\max}} \frac{y}{a}, \quad \text{for } 0 \leq y \leq y' \text{ and } y'' \leq y \leq a. \quad (3.43)$$

The distribution of effective Martensite in the regions where the reorientation of the Martensite variant occurs then follows from eqn (2.7) for $\xi_0 = \xi_{\max}$ as

$$\xi = \xi_{\max} + \frac{1 + \xi_{\max}}{\beta} \left(\frac{\sigma}{\sigma_s} + 1 \right), \quad \text{for } y' \leq y \leq y''. \quad (3.44)$$

where the ratio σ/σ_s follows from eqn (3.41) for $y' \leq y \leq y_f$ or eqn (3.42) for $y_f \leq y \leq y''$. In the rest of the cross section, the volume fraction of Martensite is still equal to ξ_{\max} .

Therefore, the axial stress and Martensite volume fraction display linear distribution along the height of the cross section in the inner austenitic region at $y \leq y_s$ only, according to eqns (3.43) and (3.44) for $\xi_{\max} = 0$, whereas their distributions in the rest of the cross section are clearly not linear.

As the bending moment is decreased or applied with the opposite sign, the boundaries y' and y'' moves inward and outward, respectively, and thus the boundary y'' may reach the outer surface when $y'' = a$, namely for $\sigma(a) = -\sigma_s$. According to eqn (3.33), this condition occurs for $\kappa = \kappa_3$, where

$$\kappa_3 = \kappa_1 - (1 + \Gamma)(\beta + 2), \quad \text{for } y_f \leq y'' \leq a. \quad (3.45)$$

During this stage, the axial stress and Martensite distributions are still provided by eqns (3.41)-(3.44). The introduction of the axial stress (3.41)-(3.43) in the balance condition (3.4)₁ then provides the normalized moment-curvature relation within the range $\kappa_3 \leq \kappa \leq \kappa_2$. In this case, the residual beam curvature when the bending moment is completely released is given by the solution of the

transcendent equation $\mu(\kappa_{\text{res}}) = 0$.

In the special case of equal Young's moduli of the two phases, namely for $\Gamma \rightarrow 0$, the axial stress in (3.41) assumes the simple expression

$$\frac{\sigma}{\sigma_s} = -1 - \frac{\kappa_y - \kappa}{1 + \delta + \delta \xi_{\text{max}}} \frac{y}{a}, \quad \text{for } y' \leq y \leq y_f, \quad (3.46)$$

where ξ_{max} is given by (3.22) for $\kappa = \kappa_{\text{max}}$.

4. Reversed bending

If an opposite bending moment is applied to the cross section after complete unloading and its magnitude is gradually increased, then the axial stress and Martensite distributions during this stage are still given by eqn (3.23) for $\kappa_2 \leq \kappa \leq \kappa_{\text{res}}$ and by eqns (3.41)-(3.44) for $\kappa_3 \leq \kappa < \kappa_2$. Indeed, eqns (3.41)-(3.44) hold true till the outer region fully made of the first variant Martensite disappears when $y'' = a$ namely for $\kappa = \kappa_3$. Actually, these equations provide the axial stress and Martensite distributions also for $\kappa < \kappa_3$. In this case, however, eqn (3.33) yields $y'' > a$. The introduction of the stress fields (3.41)-(3.43) in the balance condition (3.4)₁ then provides the moment-curvature relation for this stage of reversed bending, which continues till one of the following two conditions is met. Namely, either the axial stress reaches the critical stress $-\sigma_s$ for the start of the Martensite reorientation at height y' , i.e. for $y' = y_s$, or the axial stress reaches the critical stress $-\sigma_f$ for the finish of the Martensite reorientation at the top of the cross section, i.e. for $y_{-f} = a$. According to (3.31), the former condition occurs for $\kappa = -\kappa_{\text{max}}$, being $\xi_{\text{max}}(y_s) = 0$ and $\kappa_{\text{max}} = a/y_s$. According to (3.42) and using relations (3.33), (3.37), and (3.13), the latter condition, namely $\sigma(a) = -\sigma_f$, occurs for $\kappa = \kappa_4$, where

$$\kappa_4 = -\kappa_1 - \Gamma(\beta + 2). \quad (4.1)$$

If the magnitude of the negative bending moment is further increased, then a region fully made of the negative Martensite variant originates at the top of the cross section and propagates inwards with height y_{-f} defined by the condition $\sigma(y_{-f}) = -\sigma_f$, namely

$$\frac{y_{-f}}{a} = -\frac{\kappa_1 + (\beta + 2)\Gamma}{\kappa}, \quad \text{for } \kappa < \kappa_4, \quad (4.2)$$

according to (3.36) and (3.42). In this case, the distributions of the axial stress and the effective Martensite volume fraction are given by eqns (3.43) and (3.18) for $0 \leq y \leq y'$, by (3.41) and (3.44) for $y' \leq y \leq y_f$, and by (3.42) and (3.44) for $y_f \leq y \leq y_{-f}$, respectively, where the heights y' and y'' are defined in (3.33) as functions of κ . Integration of eqn (2.3) in the outer fully martensitic region where $\xi = -1$, starting from the finish of martensitic transformation at height y , by using (4.1) and (4.2), then

gives

$$\frac{\sigma}{\sigma_s} = -1 - \beta + \frac{1}{1+\Gamma} \left[\kappa_1 + (\beta + 2)\Gamma + \kappa \frac{y}{a} \right], \quad \text{for } y_{-f} \leq y \leq a. \quad (4.3)$$

In both cases, the introduction of the axial stress fields in (3.4)₁ then yields the corresponding bending moment-curvature relation.

Note from eqn (4.2) that for different Young's moduli, namely for $\Gamma > 0$, then for $\kappa = -\kappa_{\max}$ one has $y' = a \kappa_1/\kappa_{\max} = y_f < y_{-f}$. Therefore, the axial stress and Martensite distributions across the beam cross section for $\kappa = -\kappa_{\max}$ are not exactly opposite to those obtained from (3.21) and (3.22) for $\kappa = \kappa_{\max}$.

On the contrary, for equal Young's moduli of the two phases, namely for $\Gamma = 0$, then for $\kappa = -\kappa_{\max}$ one has $y' = y_f$ and $y_{-f} = y_f$, namely the axial stress and Martensite distributions are exactly opposite to those obtained for $\kappa = \kappa_{\max}$.

The introduction of the axial stress fields (4-38), (3.42), and (3.43) or (4.3) in the balance condition (3.4)₁ then yields the bending moment-curvature relation for the last stage of the reversed bending process.

Let σ_{\min} and ξ_{\min} denote the distributions of axial stress and effective volume fraction of Martensite along the height of the beam cross section at the end of reversed bending for $\kappa_{\min} = -\kappa_{\max}$. They follow from (3.41)-(3.44) and (4.3), by using (3.13), (3.34), and (3.36), as

$$\frac{\sigma_{\min}}{\sigma_s} = \begin{cases} -\frac{y}{a} \kappa_{\max}, & \text{for } 0 \leq y \leq y_s, \\ -1 - \beta \frac{1 + \delta + (\delta + \Gamma) \xi_{\max}}{\Gamma (1 - \xi_{\max})} \left\{ \sqrt{1 + 2\Gamma(1 - \xi_{\max})} \frac{2\kappa_{\max} y/a - (2 + \beta \xi_{\max})(1 + \Gamma \xi_{\max})}{\beta [1 + \delta + (\delta + \Gamma) \xi_{\max}]^2} - 1 \right\}, & \text{for } y_s \leq y \leq y_f, \\ -\frac{1}{1 + \Gamma + 2\delta} \left[\left(\delta - \frac{\Gamma}{2} \right) (\beta + 2) + \kappa_{\max} \frac{y}{a} \right], & \text{for } y_f \leq y \leq \min\{y_{-f, \min}, a\}, \\ -1 - \beta - \frac{y - y_{-f, \min}}{(1 + \Gamma)a} \kappa_{\max}, & \text{for } \min\{y_{-f, \min}, a\} \leq y \leq a, \end{cases} \quad (4.4)$$

and

$$\xi_{\min} = \begin{cases} 0, & \text{for } 0 \leq y \leq y_s, \\ \xi_{\max} + \frac{1 + \xi_{\max}}{\beta} \left(\frac{\sigma_{\min}}{\sigma_s} + 1 \right), & \text{for } y_s \leq y \leq \min\{y_{-f, \min}, a\}, \\ -1, & \text{for } \max\{y_{-f, \min}, a\} \leq y \leq a, \end{cases} \quad (4.5)$$

where

$$y_{-f,\min} = \frac{\kappa_1 + (\beta + 2)\Gamma}{\kappa_{\max}} a. \quad (4.6)$$

4.1 Elastic unloading after reversed bending

The integration of the rate constitutive equation (2.3) for $\dot{\xi} = 0$, being $\xi = \xi_{\min}$, by using (2.4) for $\xi_{\text{tot}} = \xi_{\max}$, then yields the axial stress during the subsequent elastic unloading process

$$\frac{\sigma}{\sigma_s} = \frac{\sigma_{\min}}{\sigma_s} + \frac{\kappa_{\max} + \kappa}{1 + \Gamma} \frac{y}{\xi_{\max}(y) a}, \quad \text{for } 0 \leq y \leq a. \quad (4.7)$$

The corresponding applied bending moment is

$$\mu = \mu_{\min} + (\kappa_{\max} + \kappa) m, \quad (4.8)$$

according to (3.4)₁ and (4.7). The elastic unloading of the beam ends when $\mu = 0$, for $\kappa = \kappa'_{\text{res}}$ where

$$\kappa'_{\text{res}} = -\kappa_{\max} - \mu_{\min} / m.$$

The elastic behavior of the beam ends when the axial stress reaches the positive critical stress σ_s at $y = \min\{y_{-f,\min}, a\}$, namely for $\kappa = \kappa_5$ where

$$\kappa_5 = \begin{cases} -\frac{\kappa_1 - \beta - 2}{\kappa_1 + (\beta + 2)\Gamma} \kappa_{\max}, & \text{if } y_{-f,\min} < a, \\ -\frac{(1 + \Gamma)(\beta\Gamma - 2 - 8\delta - 2\beta\delta) + 4\delta\kappa_{\max}}{2(1 + \Gamma + 2\delta)}, & \text{if } a \leq y_{-f,\min}. \end{cases} \quad (4.9)$$

A further increase in the applied bending moment will trigger Martensite reorientation into the positive variant at height $y = \min\{y_{-f,\min}, a\}$.

5. Results

The results presented in the following make reference to the NiTiInol constitutive parameters at room temperature $T = 298^\circ\text{K}$ considered by Brinson (1993), which are reported in Table 1. The corresponding parameters defined in Sections 3 and 4 are $\beta = 0.4575$, $\delta = 64.1286$ and $\Gamma = 1.5475$.

The distribution of the austenitic and martensitic phases varying the applied bending moment during loading are plotted in Fig. 2 together with the variations of the fronts of start and finish martensitic transformation, y_s and y_f . This figure also provides the distribution of the two phases along a SMA cantilever beam loaded by a unit transversal force applied at the tip, where the bending moment increases linearly from the loaded tip to the built-in end.

The distributions of the axial stress and effective volume fraction of Martensite along the height of the upper-half cross section at each step of loading and reversed loading are plotted in Fig. 3 and 4,

1
2 respectively, for $\mu_{\max} = 2, 3,$ and 4. These curves correspond to the end of the loading process for κ
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60

respectively, for $\mu_{\max} = 2, 3,$ and 4. These curves correspond to the end of the loading process for $\kappa = \kappa_{\max}$, the end of elastic unloading for $\kappa = \kappa_2$, the complete unloading for $\kappa = \kappa_{\text{res}}$, the reversed bending for κ equal to $\kappa_3, 0, \kappa_4,$ and $-\kappa_{\max}$, and the subsequent complete unloading for $\kappa = \kappa'_{\text{res}}$.

The variation of the axial stress and Martensite volumetric fraction along the height of the cross section during first loading are piecewise linear in the inner fully austenitic region and in the outer fully martensitic region, whereas they are weakly non-linear in the intermediate transforming regions, since different Young's moduli are considered for the two phases. Note that in the last stage of loading (solid black lines), the axial stress significantly increases in the upper fully martensitic region, where the yield stress of the SMA material could be rapidly accomplished at the top surface, in agreement with the findings of Eshghinejad and Elahinia (2015).

During the subsequent elastic unloading, the axial stress decreases linearly with the height y and no phase transformation or Martensite reorientation occur, till the negative critical stress $-\sigma_f$ is attained at y_f . This condition is accomplished for $\kappa = \kappa_2$ and $\mu = \mu_2$ defined in (3.27). Therefore, for $\kappa < \kappa_2$ the reorientation of the Martensite variant is triggered, starting from the region at height y_f . This process occurs during unloading only if the maximum bending moment applied to the cross section is larger than a limit value. For the Brinson SMA material at the considered room temperature, the (normalized) limit bending moment is $\mu_{\text{lim}} = 3.617$, this value is obtained by introducing the solution $\kappa_{\text{lim}} = 42.22$ of eqn (3.28) in eqn (3.19). The results plotted in Figs. 3a and 3b for $\mu_{\max} = 2$ and 3, respectively, show indeed that the unloading process is entirely elastic and after complete unloading, namely for $\kappa = \kappa_{\text{res}}$ (dashed red lines), a wide region is subject to residual negative axial stress, whose magnitude however is not large enough for triggering Martensite reorientation. Conversely, the results obtained in Fig. 3c for $\mu_{\max} = 4 > \mu_{\text{lim}}$ show that Martensite reorientation takes place at height y_f during unloading and spreads inwards and outwards as the applied bending moment is further decreased. In this region, the axial stress σ at the end of unloading displays a weak and limited nonlinear variation with the coordinate y , according to (3.41), being actually almost constant and a bit more negative than $-\sigma_s$ (red dashed line in Fig. 3c for $\kappa = \kappa_{\text{res}}$). It may be also observed that at the end of unloading after first loading, the axial stress vanishes at five points within the cross section. The maximum residual axial stress is attained at the top surface and it increases remarkably with μ_{\max} . For $\mu_{\max} < \mu_{\text{lim}}$ Martensite reorientation takes place during reversed bending, always starting from height y_f .

Under reversed bending, the axial stress tends to be negative and almost uniform in the upper half of the cross section till the negative critical stress $-\sigma_f$ is attained at the top for $\kappa = \kappa_4$ (see the lines for κ equal to $\kappa_3, 0, \kappa_4$ in Fig. 3). However, if the magnitude of the applied negative bending is further

1
2 increased, then the magnitude of the negative axial stress rapidly increases at the top of the cross
3 section (see the dash-dotted blue lines for $\kappa = -\kappa_{\max}$ in Fig. 3). For different Young's moduli of the
4 two phases, the distributions of the axial stress at the end of the reversed bending for $\kappa = -\kappa_{\max}$ (dash-
5 dotted blue lines) are not exactly opposite to those obtained for $\kappa = \kappa_{\max}$ (solid black lines). The axial
6 stress is indeed opposite, but its magnitude is smaller than that observed at the end of direct loading.
7 The distributions of residual axial stress at complete unloading subsequent to reversed bending,
8 namely for $\kappa = \kappa'_{\text{res}}$, are plotted in Fig. 3 as dotted black lines. Again, the axial stress vanishes at five
9 points within the cross section, the maximum magnitude of the residual axial stress is attained at the
10 top surface and it increases remarkably with μ_{\max} . Note that for the values of μ_{\max} considered in these
11 figures the complete unloading of the cross section after reversed bending occurs under rate elastic
12 behavior, since the maximum residual axial stress is lower than the critical stress σ_s everywhere.

13 The distributions of the effective Martensite volume fraction $\xi = \xi^+ - \xi^-$ along the height plotted in
14 Fig. 4 turn out to be slightly nonlinear within the transforming region, during the first loading process
15 also, although it is very close to a linear trend. Clearly, the total amount of Martensite transformed
16 within the cross section increases with the maximum bending moment μ_{\max} applied at the end of
17 loading. As the bending moment is completely removed, namely for $\kappa = \kappa_{\text{res}}$, if $\mu < \mu_{\text{lim}}$ then the
18 Martensite distribution does not change (see Figs. 4a and 4b), being the unloading process entirely
19 elastic, whereas if $\mu > \mu_{\text{lim}}$ then the production of a limited amount of the secondary Martensite variant
20 can be observed (dashed red line in Fig. 4c).

21 As the bending moment is decreased and then applied with the reversed sign, the size of the region
22 where Martensite reorientation takes place, namely where $\sigma < -\sigma_s$, increases. At first it reaches the
23 top surface of the cross section for $\kappa = \kappa_3$ and then it tends to recover the entire region where the
24 martensitic transformation occurred under direct bending, namely the upper region over the height y_s .
25 Note that when the beam curvature is completely removed, namely for $\kappa = 0$ (dashed green lines in
26 Fig. 4), the effective Martensite volume fraction is still positive within the cross section. No backward
27 Austenitic transformation is activated under reversed bending, being $T < A_s$. However, a significant
28 amount of the primary (positive) Martensite variant undergoes the reorientation process into the
29 secondary (negative) Martensite variant and thus the effective volume fraction of Martensite ξ
30 decreases. Obviously, a similar but opposite Martensite reorientation occurs in the lower half of the
31 cross section. Also the distributions of the effective Martensite volume fraction ξ at the end of
32 reversed bending for $\kappa = -\kappa_{\max}$ (dash-dotted blue lines) are opposite, but smaller than those observed
33 at the end of direct bending for $\kappa = \kappa_{\max}$ (solid black lines), thus denoting that the initial Martensite
34 variant is still present within the cross section at the end of reversed bending.

The partition of the cross section at the end of first unloading, namely for $\kappa = \kappa_{res}$, varying the maximum applied bending moment μ_{max} is plotted in Fig. 5. In this plot, the region below the curve y_s (solid black line) is in a purely austenitic state; the transformation region between the curves y_s, y_f (solid blue line), y' , and y'' (dashed and das-dotted red lines) is made of a mixture of austenite and single variant Martensite; finally, in the region between the curves y' and y'' the reorientation of the Martensite variant occurred during unloading.

The partition of the cross section at the end of reversed bending, namely for $\kappa = -\kappa_{max}$, varying the maximum applied bending moment μ_{max} is also reported the same plot. In this case, $y' = y_s$ and $y_f < y_{-f,min} < a < y''$. Therefore, the region below the curve y_s still is in a purely austenitic state; the region between the curves y_s and $y_{-f,min}$ (dashed green line), is made of a mixture of austenite and both Martensite variants; finally, the region over the curve $y_{-f,min}$ is entirely made of the secondary Martensite variant. The latter distribution does not change during the subsequent elastic unloading.

The closed form relations between the normalized applied bending moment μ and beam curvature κ under the direct and reversed bending cyclic process are plotted in Fig. 6 for $\mu_{max} = 2, 3$, and 4.

Due to the lower Young's modulus of Martensite with respect to that of Austenite, the slope of the last part of the loading process as well as that of the elastic unloading process is clearly smaller than the slope of the initial austenitic loading process. This occurrence makes the residual beam curvature after complete unloading as well as the area enclosed by each cycle a little bit smaller than those obtained under the simplifying assumption of equal Young's moduli of the two phases (Ostadrahimi et al., 2015). Therefore, such a simplifying assumption overestimates the shape memory effect and the energy dissipation capabilities of SMA, as already observed under torsional loading (Radi, 2020).

5.1 Validation by comparison with available results

In order to validate the present analysis, a comparison with some analytical results available in the technical literature is provided in Fig. 7. To this aim, the axial stress distributions in a rectangular cross section of height $2a = 2$ mm and width $b = 2$ mm subject to an increasing bending moment at constant temperature $T = 30$ °C given in Fig. 12a of Eshghinejad and Elahinia (2015) (blue lines) are compared with those obtained in the present work (red lines). The constitutive parameters considered by Eshghinejad and Elahinia (2015) at temperature $T = 30$ °C $> A_f$ are given in Tab. 2. The curves are very close, although a slight discrepancy can be noticed for the higher levels of loading due to the difference between the adopted SMA constitutive models. Eshghinejad and Elahinia (2015) assumed indeed linear stress distributions in all regions, whereas slightly nonlinear stress distributions are

found in the present analysis, as due to the different Young's moduli of the two phases.

In addition, the tip displacement of a SMA cantilever beam caused by a tip force F in a loading-unloading cycle from 0 to 10 N obtained from the present formulation is compared in Fig. 8 with that provided by Eshghinejad and Elahinia (2015) in their Fig. 8c. The constitutive parameters at temperature $T = -5^\circ\text{C} < A_s$ considered therein are reported in Tab. 2 (note that the value assumed for ε_L can not be found in their paper and it has been supplied by the authors by private communication).

The tip displacement calculated numerically by double integrating the differential equation for a cantilever Euler-Bernoulli beam, built-in at the end at $x = L = 30$ mm, namely

$$w = \frac{L^2 \sigma_s}{a E_A} \int_0^1 d\xi \int_\xi^1 \kappa\left(\frac{3FL\eta}{2ba^2\sigma_s}\right) d\eta, \quad (5.1)$$

where $\kappa = \kappa(\mu)$ denotes the inverse relation between normalized bending moment and curvature defined in Section 3 for first loading and elastic unloading. In this case also, the results are reasonably close and a discrepancy can be noticed for the higher levels of loading due to the differences between the two SMA constitutive models. In particular, during the martensitic transformation the present model turns out to be a bit stiffer than that developed by Eshghinejad and Elahinia (2015).

A further comparison is made in Fig. 9 with the analytical and FEM results provided by Ostradrahimi et al. (2015) for the bending moment-curvature relation of a rectangular cross section with $a = 0.5$ mm and $b = 1$ mm. These results are obtained under direct loading and elastic unloading at temperature $T = -40^\circ\text{C}$ lower than $M_s = -34^\circ\text{C}$ and thus also lower than A_s . The corresponding material parameters are reported in Tab. 3. The analytical model developed by these authors assumes the same Young's moduli for both phases, namely $\Gamma = 0$. In this case the stress-strain relations become linear also in the transformation region. The analytical results obtained from the present approach for the particular case of $\Gamma = 0$ are practically coincident with those obtained by Ostradrahimi et al. (2015) and very close to the FEM predictions. A slight difference can be observed at the end of elastic unloading because the model considered in Ostradrahimi et al. (2015) allows for reverse austenitic transformation before complete unloading, whereas for the present model the reverse phase transformation can not take place at temperature lower than A_s .

Unfortunately, no analytical or numerical investigations are available in the technical literature for validating the present model under the reverse bending process, in particular for the temperature range originating the shape memory effect considered here.

6. Conclusions

A simple 1D constitutive model is adopted for modelling the isothermal response of a SMA beam

1
2 with rectangular cross section under direct and reversed pure bending. The model takes into account
3 for different Young's moduli of the two phases by adopting the Reuss scheme of composite materials
4 for the description of the SMA elastic behavior. Two opposite Martensite variants can take place
5 according to the sign of the axial stress. Their volumetric fractions are assumed to evolve linearly
6 with the axial stress, so that the linear rate constitutive equations for SMA can be easily integrated in
7 closed form within each step. Moreover, the axial stress and the Martensite distribution across the
8 beam cross section can be calculated analytically at each step of the cyclic process. In particular, the
9 distributions of axial stress and effective Martensite volume fraction in the transformed regions of the
10 cross section are slightly nonlinear as due to the different Young's moduli of the two phases. The
11 analytical or numerical integration of the contribution of the axial stress within the cross section then
12 yields the bending moment applied to the cross section as a function of the beam curvature both under
13 bending and reversed bending.

22 We found here that the response of the cross section under reversed bending is not symmetrical with
23 respect to the first bending loading, namely the stress field and the Martensite distribution at the end
24 of negative reloading is not exactly opposite to those observed at the end of loading, although a
25 symmetric tension-compression constitutive behavior has been assumed. The difference is due to the
26 different Young's moduli of the two phases. Indeed, the response becomes perfectly symmetric for Γ
27 = 0, namely for $E_A = E_M$. In this case indeed the distributions of stress and Martensite variants at the
28 end of the loading process and at the end of the negative loading process are equal but opposite in
29 sign. With some additional analytical complications, the model can be extended to account also for
30 asymmetric tension-compression behavior of the SMA by assuming different magnitudes of the
31 positive and negative critical stresses.

32 Here, the analysis has been developed only for the first cycle of direct and reverse loading. In
33 principle, it can be extended to subsequent cycles, of course with increasing difficulties. Future
34 investigations may be extended to multiple loading cycles, general bending, and different temperature
35 ranges. Note that the response during repeated loading cycles of the same amplitude does not change
36 if the elastic modulus of the SMA material is assumed constant, namely for $\Gamma = 0$. In this case, indeed,
37 the response observed in the first cycle is exactly reiterated in subsequent cycles of the same
38 amplitude. The present results are also sufficiently accurate under general bending if the shear stress
39 is much smaller than the axial stress, as it generally occurs for slender beam with compact cross
40 section. In this case indeed the shear stress attains the largest values in proximity of the cross section
41 centroid, where no transformation is triggered, and thus a weak effect on the phase transformation
42 condition is expected from the contribution of the shear stress. Finally, the framework used here for
43 modelling Martensite reorientation can be adopted also for modelling the reverse austenitic
44

1 transformation which may occur during unloading at temperatures higher than A_s .
2
3 The exact closed form solution provided here is particularly valuable for analyzing and understanding
4 the role played by the constitutive parameters in the shape memory effect of SMA beams during a
5 bending cycle of reversed sign. Each step of the derivation of the analytical solution is clearly
6 described in the paper and can be easily checked. Besides providing a reliable evaluation of the actual
7 and residual stresses and strains in SMA beam under direct and reverse bending, the analytical results
8 here obtained have a number of additional advantages. Indeed, they can be exploited for the accurate
9 design of innovative seismic dissipating devices and actuators realized by SMA beams loaded in
10 bending and subjected to alternating loading. They can support designers in the calibration process
11 of numerical models able to describe SMA macroscopic effects. They are also useful for validating
12 the accuracy of numerical procedures based on more refined constitutive models employed in the
13 modeling of SMA beams under complex cyclic loading.
14
15
16
17
18
19
20
21
22
23

24 **Acknowledgements.**

25 Support from the Italian "Gruppo Nazionale di Fisica Matematica" INdAM-GNFM is gratefully
26 acknowledged.
27
28
29
30
31
32

33 **References**

- 34 Auricchio F, Morganti S, Reali A, Urbano M (2011) Theoretical and experimental study of the shape
35 memory effect of beams in bending conditions. *Journal of Materials Engineering and*
36 *Performance* 20(4-5): 712-718.
37
38 Auricchio F, Sacco E (1997) A Superelastic Shape-Memory-Alloy Beam Model. *Journal of*
39 *Intelligent Material Systems and Structures* 8(6): 489-501.
40
41 Brinson LC (1993) One-dimensional constitutive behavior of shape memory alloys: thermo-
42 mechanical derivation with non-constant material functions and redefined Martensite internal
43 variable. *Journal of Intelligent Material Systems and Structures* 4(2): 229-242.
44
45 Brinson LC, Huang MS (1996) Simplifications and comparisons of shape memory alloy constitutive
46 models. *Journal of Intelligent Material Systems and Structures* 7: 108-114.
47
48 Choi E, Lee DH, Choei NY (2009) Shape memory alloy bending bars as seismic restrainers for
49 bridges in seismic areas. *International Journal of Steel Structures* 9(4): 261-273.
50
51 Choi E, Mohammadzadeh B, Kim HS (2019) SMA bending bars as self-centering and damping
52 devices. *Smart Materials and Structures* 28: 025029.
53
54
55
56
57
58
59
60

- 1
2 De la Flor S, Urbina C, Ferrando F (2011) Asymmetrical Bending Model for NiTi Shape Memory
3 Wires: Numerical Simulations and Experimental Analysis. *Strain* 47: 255-267
4
5 DesRoche R, Smith B (2004) Shape memory alloys in seismic resistant design and retrofit: a critical
6 review of their potential and limitations. *Journal of Earthquake Engineering* 8: 415-429.
7
8 Dolce M, Cardone D, Marnetto R (2000) Implementation and testing of passive control devices based
9 on shape memory alloys. *Earthquake Engineering and Structural Dynamics* 29: 945-968.
10
11 Dolce M, Cardone D (2001) Mechanical behavior of shape memory alloy for seismic applications 1.
12 Martensite and Austenite NiTi bars subject to torsion. *International Journal of Mechanical*
13 *Sciences* 43: 2631-2656.
14
15 Eshghinejad A, Elahinia M (2015) Exact Solution for Bending of Shape Memory Alloy Beams.
16 *Mechanics of Advanced Materials and Structures* 22: 829-838.
17
18 Fang C, Wang W (2020) Shape memory alloys for seismic resilience. Springer. Singapore.
19
20 Fahimi P, Eskandari AH, Baghani M, Taheri A (2019) A semi-analytical solution for bending
21 response of SMA composite beams considering SMA asymmetric behavior. *Composites Part B:*
22 *Engineering* 163: 622-633.
23
24 Govindjee S, Kasper ER (1997) A shape memory alloy model for Uranium-Niobium accounting for
25 plasticity. *Journal of Intelligent Material Systems and Structures* 8: 815-823.
26
27 Govindjee S, Kasper ER (1999) Computational aspects of one-dimensional shape memory alloy
28 modeling with phase diagrams. *Computational Methods in Applied Mechanics and Engineering*
29 171: 309-326.
30
31 Liang C, Rogers CA (1990) One-dimensional thermomechanical constitutive relations for shape
32 memory materials *Journal of Intelligent Material Systems and Structures* 1(2): 207-234.
33
34 Marfia S, Rizzoni R (2013) One-dimensional constitutive SMA model with two Martensite variants:
35 Analytical and numerical solutions. *European Journal of Mechanics A/Solids* 40:166-185.
36
37 Mirzaeifar R, DesRoches R, Yavari A, Gall K (2013) On superelastic bending of shape memory alloy
38 beams. *International Journal of Solids and Structures* 50: 1664-1680.
39
40 Ostadrahimi A, Arghavani J, Poorasadion S (2015) An analytical study on the bending of prismatic
41 SMA beams. *Smart Materials and Structures* 24: 125035.
42
43 Ozbulut OE, Hurlebaus S, Desroches R (2011) Seismic response control using shape memory alloys:
44 a review. *Journal of Intelligent Material Systems and Structures* 22(14): 1531-1549.
45
46 Panoskaltsis VP, Bahuguna S, Soldatos D (2004) On the thermomechanical modelling of shape
47 memory alloys. *International Journal of Nonlinear Mechanics* 39(5): 709-722.
48
49
50
51
52
53
54
55
56
57
58
59
60

- Poorasadion S, Arghavani J, Naghdabadi R, Sohrabpour S (2015). Implementation of microplane model into three-dimensional beam element for shape memory alloys. *International Journal of Applied Mechanics* 7(6): 1550091.
- Radi E (2018) Evolution of multiple Martensite variants in a SMA thick walled cylinder under internal pressure. *International Journal of Solids and Structures* 155: 15-35.
- Radi E (2020) Exact solutions for isothermal cyclic torsional loading of a circular SMA bar exploiting the shape memory effect. *International Journal of Solids and Structures* Submitted.
- Rejzner J, LExcellent C, Raniecki B (2002) Pseudoelastic behaviour of shape memory alloy beams under pure bending: experiments and modelling. *International Journal of Mechanical Sciences* 44: 665-686.
- Rizzoni R, Marfia S (2015) A thermodynamical formulation for the constitutive modeling of a shape memory alloy with two martensite phases. *Meccanica* 50(4): 1121-1145.
- Rizzoni R, Merlin M, Casari D (2013) Shape recovery behaviour of NiTi strips in bending: experiments and modelling. *Continuum Mechanics and Thermodynamics* 25: 207-227.
- Song G, Ma N, Li HN (2006) Applications of shape memory alloys in civil structures. *Engineering Structures* 28(9): 1266-1274.
- Speicher M, Hodgson DE, DesRoche R, Leon RT (2009) Shape memory alloy tension/ compression device for seismic retrofit of buildings. *Journal of Materials Engineering and Performance* 18: 746-753.
- Viet NV, Zaki W, Umer R (2018) Analytical model for a superelastic Timoshenko shape memory alloy beam subjected to a loading-unloading cycle. *Journal of Intelligent Material Systems and Structures* 29(20): 3902-3922.
- Viet NV, Zaki W, Moumni Z (2019) A model for shape memory alloy beams accounting for tensile compressive asymmetry. *Journal of Intelligent Material Systems and Structures* 30(18-19): 2697-2715.
- Wilde K, Gardoni P, Fukino Y (2000) Base isolation system with shape memory alloy device for elevated highway bridges. *Engineering Structures* 22: 222-229.
- Wilson JC, Wesolowsky MJ (2005) Shape memory alloys for seismic response modification: a state-of-the-art review. *Earthquake Spectra* 21(2): 569-601.
- Zaki W (2012) An efficient implementation for a model of Martensite reorientation in martensitic shape memory alloys under multiaxial nonproportional loading. *International Journal of Plasticity* 37: 72-94.
- Zibasokhan H, Behnamfar F, Azhari M (2019) Experimental study of a new pure bending yielding dissipater. *Bulletin of Earthquake Engineering* 17(7): 4389-4410.

1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60

Appendix A

The integral in the definition of m in eqn (3.26) can be calculated as

$$\int_1^{1+\Gamma} [(t+\delta)^2 - p]^2 \left(1 + \frac{\delta}{t}\right) dt = \frac{1}{5} [(1+\Gamma)^5 - 1] + \frac{5}{4} \delta [(1+\Gamma)^4 - 1] - \frac{2}{3} [(1+\Gamma)^3 - 1] (p - 5\delta^2) \\ + [(1+\Gamma)^2 - 1] \delta (5\delta^2 - 3p) + \Gamma(5\delta - p) (\delta^2 - p) + \delta (p - \delta^2)^2 \ln(1+\Gamma),$$

where

$$p = (1+\delta)^2 - 2\frac{\Gamma}{\beta}$$

TABLES

T [°C]	E_A [GPa]	E_M [GPa]	σ_s [MPa]	σ_f [MPa]	ε_L
25	67	26.3	153	223	0.067

Table 1. Young's moduli of the two phases, Poisson coefficient, critical stresses and maximum residual transformation strain for Brinson SMA materials at room temperature.

T [°C]	E_A [GPa]	E_M [GPa]	σ_s [MPa]	σ_f [MPa]	ε_L
-5	73.2	30	25	125	0.0166
30	73.2	30	200	300	0.0166

Table 2. SMA constitutive parameters at temperatures $T = -5$ °C and $T = 30$ °C, from Eshghinejad and Elahinia (2015).

T [°C]	E_A [GPa]	E_M [GPa]	σ_s [MPa]	σ_f [MPa]	ε_L
-40	53	53	122.5	197.5	0.05

Table 3. SMA constitutive parameters at temperatures $T = -40$ °C from Ostradrahimi et al. (2015).

FIGURES

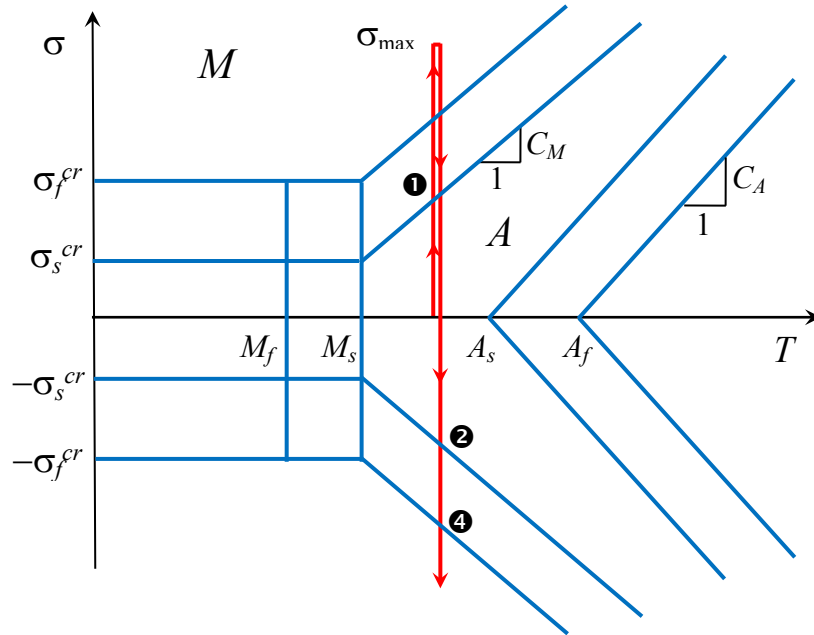


Fig 1. Threshold stresses for martensitic and austenitic transformations (blue lines) and isothermal loading-unloading process (red lines) at temperature T between M_s and A_s .

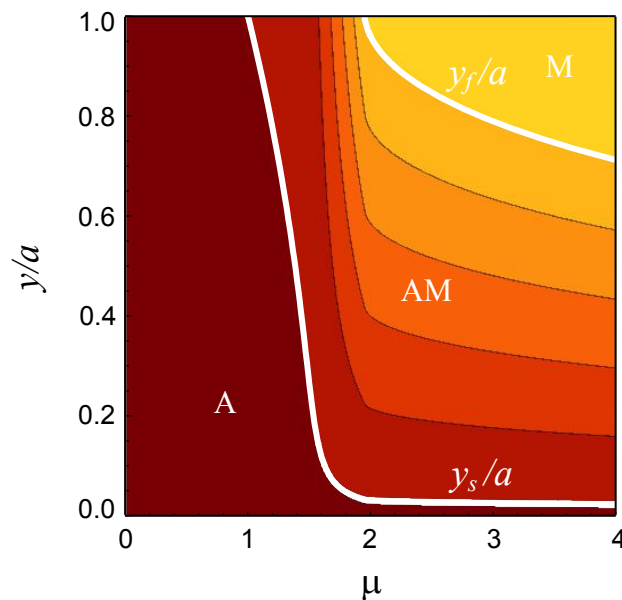
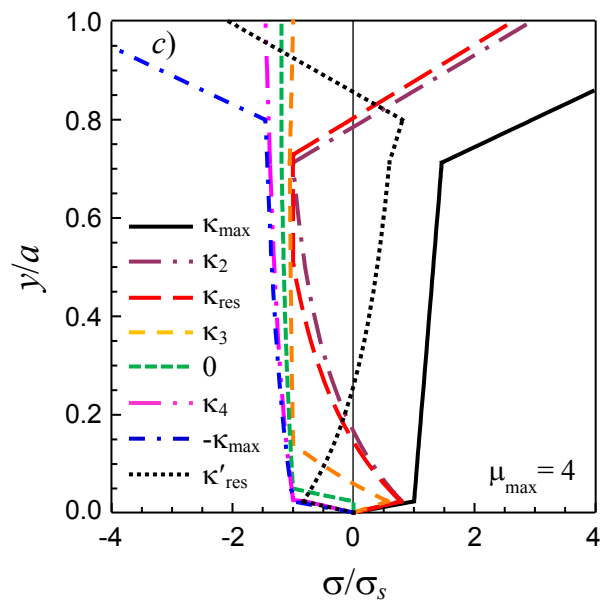
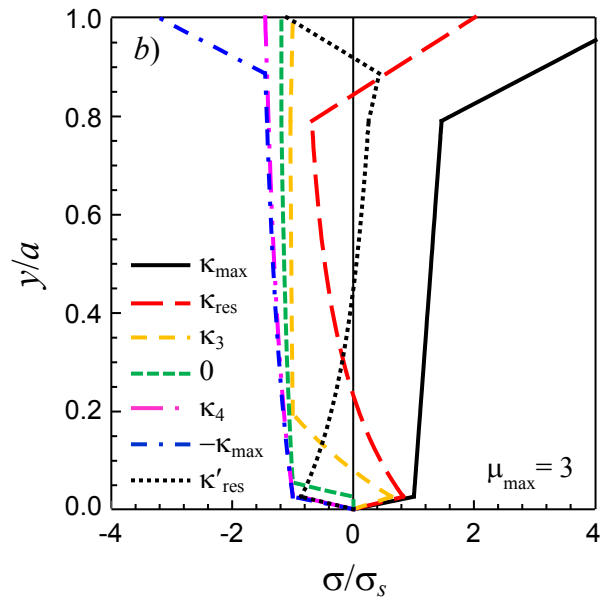
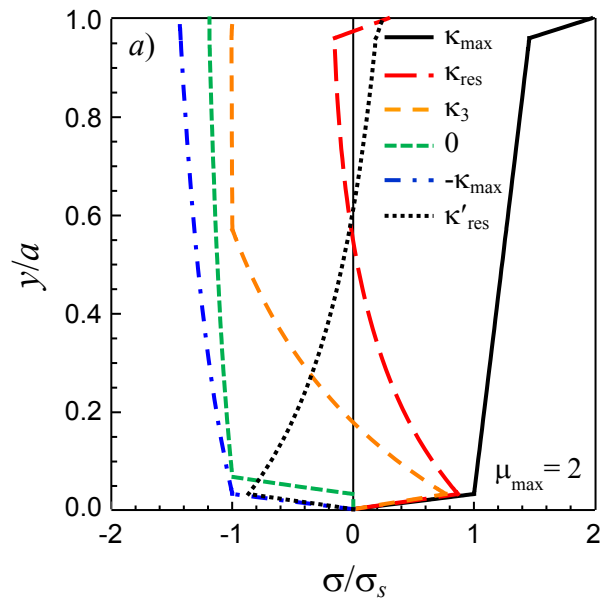
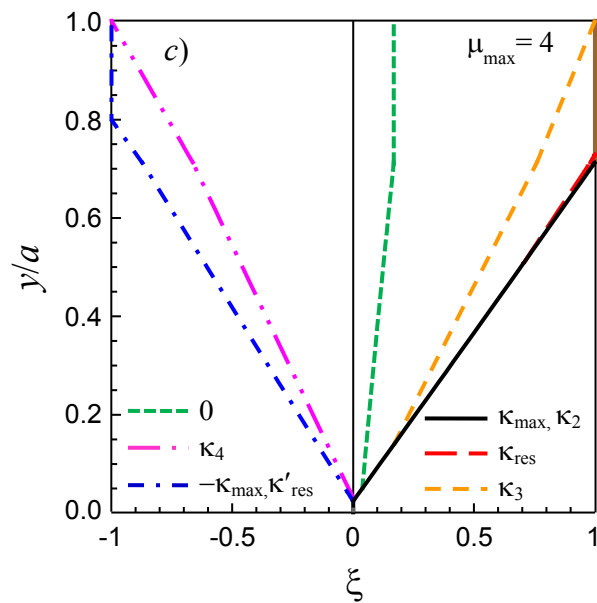
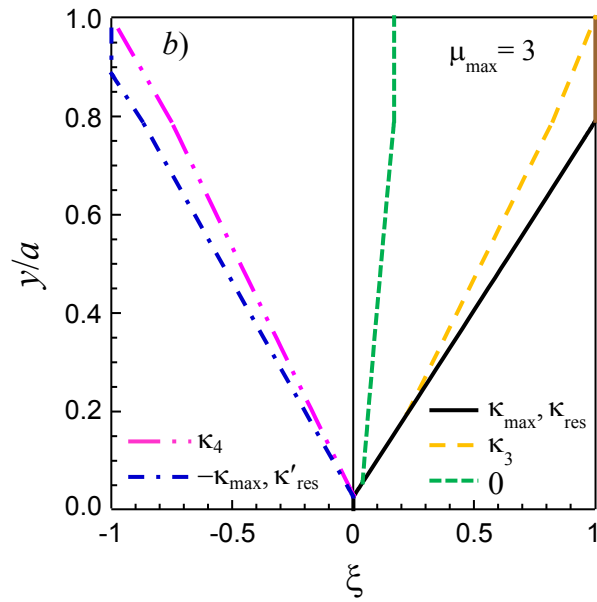
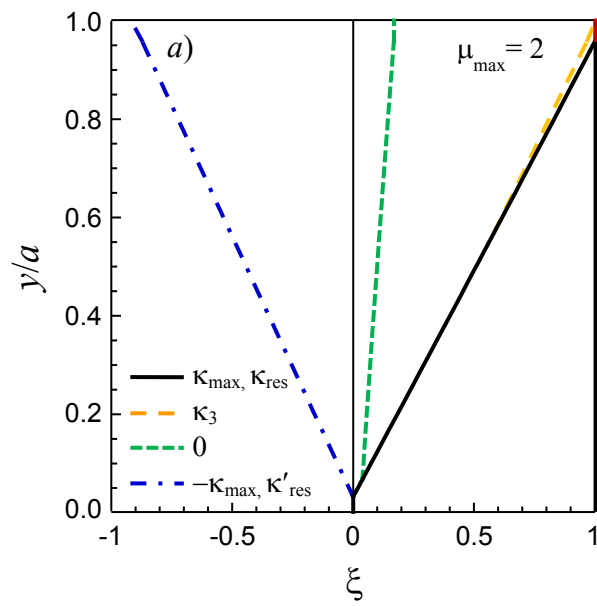


Fig. 2. Distribution of Austenite and Martensite and variations of the fronts of finish and start martensitic transformation with the applied bending moment under loading, for Brinson SMA material.



1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60

Fig. 3. Distributions of the axial stress σ along the height of the cross section, for various values of the beam curvature κ and for $\mu_{\max} = 3, 4, \text{ and } 5$, for Brinson SMA material.



1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60

Fig. 4. Distributions of the effective Martensite volume fraction ξ along the height of the cross section, for various values of the beam curvature κ and for $\mu_{\max} = 3, 4, \text{ and } 5$, for Brinson SMA

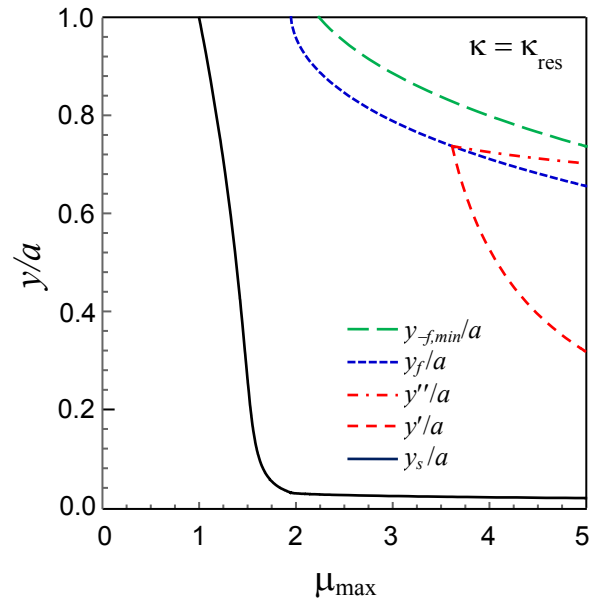


Fig. 5. Normalized variations with the maximum bending moment applied to the cross section of the fronts of finish and start martensitic transformation and of the upper and lower fronts of the region undergoing transformation between Martensite variants at first complete unloading and at the end of reversed bending, for Brinson SMA material.

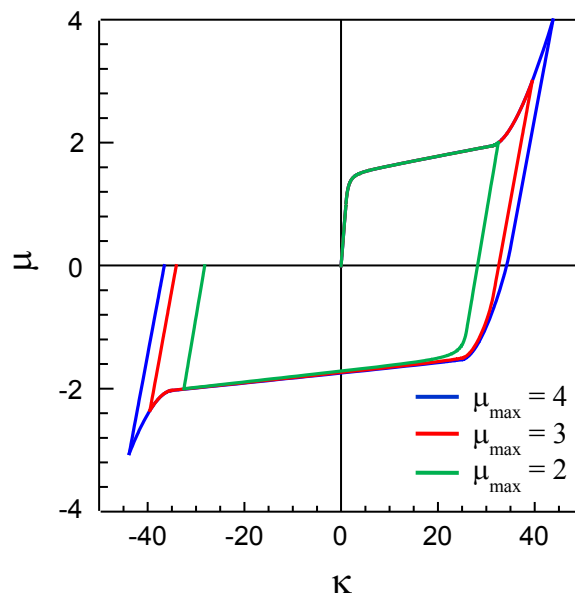


Fig. 6. Normalized cyclic variations of the applied bending moment with the beam curvature, under alternative loadings for $\mu_{\max} = 2, 3, \text{ and } 4$, for Brinson SMA material.

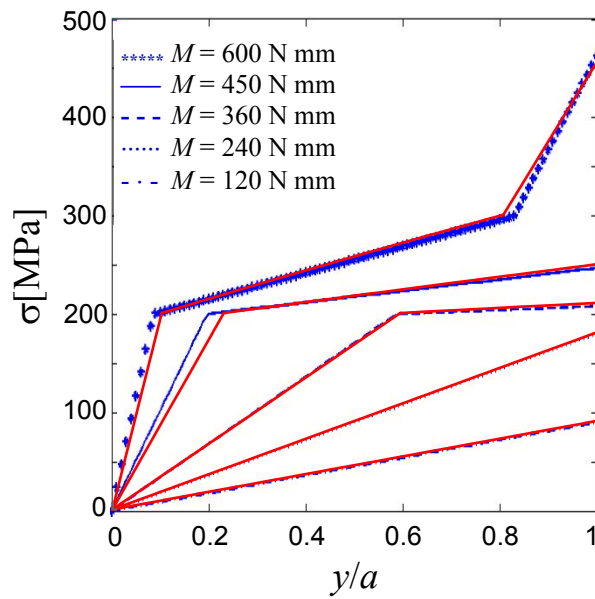


Fig. 7. Comparison between the axial stress distributions along the height of the beam provided by the present analysis (red lines) and those provided in Fig. 12a of Eshghinejad and Elahinia (2015) (blue lines) for Material I, for the loading process at temperature $T = 30^{\circ}\text{C}$.

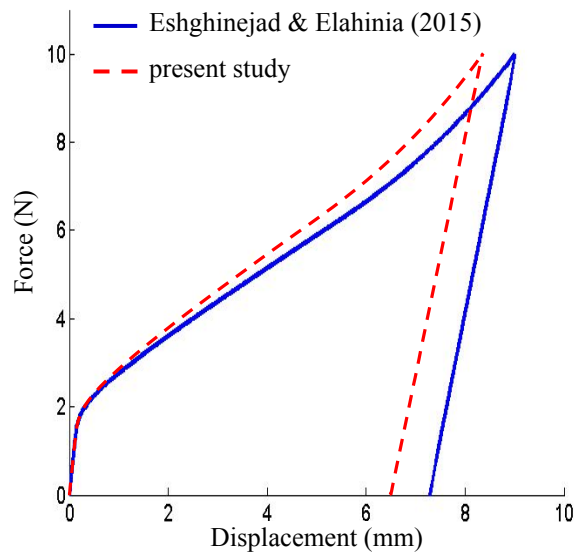


Fig. 8. Comparison between the force vs tip displacement relation of a SMA cantilever beam at $T = -5^{\circ}\text{C}$ provided by the present analysis (dashed red line) and those provided in Fig. 8c of Eshghinejad and Elahinia (2015) (solid blue line).

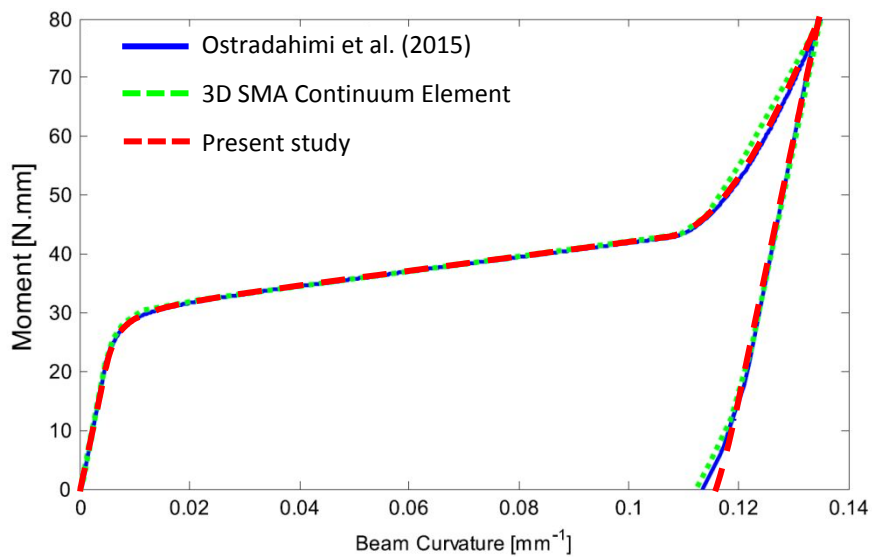


Fig. 9. Comparison between the moment-curvature relation of a SMA rectangular cross section with $a = 0.5$ mm and $b = 1$ mm provided by the present analysis (dashed red line) and those provided in Fig. 12 of Ostradahimi et al. (2015), obtained by their analytic model (solid blue line) and by FEM analysis (dashed green line).