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# 1 Highlights

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- 4 • Variational derivation through the Love hypothesis leads to the Bishop-Love equation;
- 5 • This is not asymptotically equivalent to the Love equation;
- 6 • The Love hypothesis naturally emerges from a two-modal kinematics by multiscale analysis;
- 7 • This approach provides a correction term of the same order as that in the Love equation;
- 8 • The traditional ill-posedness coming from nonstandard boundary conditions is remedied.

# Revisiting the Love hypothesis for introducing dispersion of longitudinal waves in elastic rods

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## ABSTRACT

We re-examine the Love *equation*, which forms the first historical attempt at improving on the classical wave equation to encompass for dispersion of longitudinal waves in rods. Dispersion is introduced by accounting for lateral inertia through the Love *hypothesis*. Our aim is to provide a rigorous justification of the Love *hypothesis*, which may be generalized to other contexts. We show that the procedure by which the Love equation is traditionally derived is misleading: indeed, proper variational dealing of the Love hypothesis in a two-modal kinematics (the Mindlin-Herrmann system) leads to the Bishop-Love equation instead. The latter is not asymptotically equivalent to the Love equation, which is in fact a long wave low frequency approximation of the Pochhammer-Chree solution. However, the Love hypothesis may still be retrieved from the Mindlin-Herrmann system, by a slow-time perturbation process. In so doing, the linear KdV equation is retrieved. Besides, consistent approximation demands that a correction term be added to the classical Love *hypothesis*. Surprisingly, in the very special case of isotropic linear elasticity, this correction term produces no effect in the correction term of the Lagrangian, so that, to first order, the same Bishop-Love equation is the Euler-Lagrange equation corresponding to a family of Love-like hypotheses, all being different by the correction term. Remarkably, ill-posedness coming from non-standard (namely non static) natural boundary conditions is now amended.

## 1. Introduction

The theory describing propagation of longitudinal waves in elastic rods, based on the seminal works of D’Alambert, Bernoulli, Euler and Lagrange (Oliveira et al., 2020), retains great significance, both from the practical as well as from the theoretical standpoint. Modern non-destructive testing procedures are being developed which rely on a deeper understanding on the mechanics of wave propagation, also in connection with the idea of generalized continua (Nobili and Volpini, 2021). As it is well known, the celebrated wave equation represents the prototype for nondispersive phenomena, since it neglects any effect transversal to the direction of wave propagation. In this sense, the wave equation is perfectly unidirectional and it describes a rod with vanishingly thin cross-section. Rayleigh is credited as the first who came to recognize the importance of accounting for transversal effects (Rayleigh, 1894). Shortly later, elaborating on this idea, Love (1927) introduced what is now known as the Rayleigh-Love equation (sometimes simply the Love’s equation, or, as in Hutchinson and Percival (1968), Love’s modified wave equation), that describes dispersive longitudinal waves in thin elastic rods. This model, which represents the forefather of several successive attempts in the literature, accounts for dispersion through the Love *hypothesis*, which stipulates that *inertial* effects attached to the transversal motion of the cross-section are to be considered. It is important to emphasize that, as Love explicitly points out, only inertial effects are considered, while the elastic response remains unaltered (i.e. totally unidirectional). Indeed, following Hutchinson and Percival (1968), “Love’s equation includes the radial inertia of the bar, which adds the effect of dispersion to the description of the wave phenomenon and allows the consideration of shorter wavelengths than does the simple wave equation”. The resulting Love equation remains attractive for its simplicity and favorably compares with the exact solution developed by Pochhammer (1876) and, shortly later, independently, by Chree (1889), for a circular cross-section. Besides, Hutchinson and Percival (1968) offer experimental support for the capability of the Love equation to accurately describe the propagation of fundamental modes, while higher modes can be only interpreted through the Pochhammer-Chree solution. Yet, the Love equation cannot accommodate the boundary conditions on the free lateral surface of the rod and, in this sense, it should be regarded as an approximation,

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the limits of which should be well investigated. Nonetheless, the idea behind the Love hypothesis stands at the basis of several refined models of longitudinal wave propagation, a nice account of which may be found in Shatalov et al. (2011). Among these, the Mindlin-Herrmann model (Mindlin, 1951) stands out because it represents the first attempt to develop, in a rigorous manner, a refined model starting from a restricted kinematics (here, the Euler-Bernoulli kinematics), through the so-called Kirchhoff method. More recently, the Love hypothesis has been applied outside the linear framework, where it properly belongs, to incorporate the lateral motion of the cross-section when developing nonlinear models. As a case in point, Samsonov (1994) considers the Murnaghan model for compressible materials and the Love hypothesis because it is “the first term of a transverse displacement expansion in a power series with respect to the small longitudinal strain [...] and remains valid for long waves, while one should consider the Herrmann and Mindlin model for a possible refinement of the correlation between longitudinal strain and transverse displacement”. Accordingly, it is suggested that the Love hypothesis is the leading order term in a small strain expansion, whose refinement is the Mindlin-Herrmann model. Yet, this interpretation does not match the original idea developed by Love, which, instead, calls upon the Love hypothesis only for inertial effects. Besides, as we shall show in this paper, the Love hypothesis is the leading term approximation in a multiscale analysis of the Mindlin-Herrmann system, the latter being asymptotically different from the Love equation in the long wave regime. The same approach by which the Love hypothesis is carried over to the nonlinear framework is undertaken by Dai and Huo (2002), in analogy with Ostrovskii and Sutin (1977), Sørensen et al. (1984) and Clarkson et al. (1986). The Love hypothesis is again retrieved by Dai and Fan (2004) for incompressible elastic materials under finite cylindrical deformations from an asymptotic procedure in the small parameter given by the axial displacement  $h$  over the typical wavelength  $l$ . The same result is illustrated by Dai and Huo (2000) for compressible materials. As a workaround, Wright (1985) employs the incompressibility constraint to connect transversal and longitudinal motion without the need for the Love hypothesis, the incompatibility of the two assumptions being shown by Amendola and Saccomandi (2021). Furthermore, Samsonov et al. (1998) shows experimental results on soliton formation which support dependence on the cross-section geometry and therefore discourage the adoption of the Love hypothesis. It then appears that it is important to precisely frame the range of validity of the Love hypothesis and clear-cut its origin, so that its adoption and generalization may be rigorously justified. This is precisely the aim of this paper, which revisits the traditional derivation of the Love hypothesis in Sec.2 and then moves, in Sec.3, to illustrate how it also comes from a multiscale analysis of the Mindlin-Herrmann system. The corresponding variational principle is illustrated in Sec.4 and results are finally drawn in Sec.5.

## 2. Mathematical background

To obtain in a direct way an unimodal (i.e. encompassing a single dependent field) dispersive equation for longitudinal waves in rod, within the framework of linear elasticity, two approaches are possible. The first is connected to the derivation of the wave equation from a discrete lattice: We consider an infinite elastic chain of equidistant particles, with lattice spacing  $a$ , in equilibrium and acted upon by linear springs of identical stiffness. In the continuum limit, we justify a Taylor expansion with respect to  $a$  and, to second order, we obtain the classical dispersive linear wave equation: the Boussinesq’s equation. This approach can be extended to the nonlinear setting in several ways (Maugin, 1999). The second possibility relies on the use of the axiomatic theory of continuum mechanics for deducing a dispersive wave equation such as, for example, the *Love hypothesis*, which then leads to the *Love equation*.

The classical derivation of the Love equation (L) is contained in Section 278, Chapter XX, page 428, of the book by A.E.H.Love (1927). Essentially, the same derivation may be found in the book by Graff (Graff, 2012, §2.5.3, p.116) or by Miklowitz (Miklowitz, 1978, §7.1.1.2).

Let us briefly review this derivation, which often goes under the name of the *Love-Rayleigh rod theory*. To obtain the linear Love equation, the first step is to assume the *Navier-Bernoulli* (NB) hypothesis: during deformation, plane cross-sections remain planar and normal to the rod axis (Achenbach, 1973).

Let us consider a rod that, in a reference configuration, is a circular cylinder of radius  $A$  and let us introduce cylindrical coordinates in the current configuration  $\mathbf{x} = r\mathbf{e}_r + \theta\mathbf{e}_\theta + z\mathbf{e}_z$  and, equally, cylindrical coordinates in the reference configuration  $\mathbf{X} = R\mathbf{E}_R + \Theta\mathbf{E}_\Theta + Z\mathbf{E}_Z$ , with  $0 \leq R \leq A$ . In this framework, the NB hypothesis consists of assuming the following axisymmetric time dependent two-modal motion (Wright, 1981, Eq.(12))

$$r = R + RU(Z, T), \quad \theta = \Theta, \quad z = Z + W(Z, T). \quad (1)$$

Indeed, displacement is described by a two-term powers series expansion in the radial coordinate of the axisymmetric problem. We assume that the determining equation for the functions  $U(Z, T)$  and  $W(Z, T)$  may be obtained directly

108 as the Euler-Lagrange equations associated with the Lagrangian density  $\mathcal{L} = \mathcal{T} - \mathcal{V}$ . Here, the kinetic energy density  
 109 per unit length is given by (Graff, 2012, Eq.(2.5.49))

$$\mathcal{T} = \int_0^A \int_0^{2\pi} \frac{\rho}{2} (W_T^2 + R^2 U_T^2) R d\Theta dR, \quad (2)$$

where  $\rho$  is the mass density in the reference configuration. It is understood that a coordinate subscript implies differentiation with respect to the relevant variable, i.e.  $W_T = \partial W / \partial T$ . In the linear framework, the "potential energy" is obtained considering the isotropic strain-energy density per unit volume

$$\mathcal{W} = \mu \operatorname{tr}(\epsilon^2) + \frac{1}{2} \lambda \operatorname{tr}^2(\epsilon),$$

110 where  $\mu$  and  $\lambda$  are the usual Lamé parameters and

$$\epsilon = \frac{1}{2} [\nabla \mathbf{u} + (\nabla \mathbf{u})^T], \quad (3)$$

111 is the infinitesimal strain tensor (by  $\nabla$  we denote the two-dimensional gradient operator). Here,  $\mathbf{u} = \mathbf{x} - \mathbf{X}$  clearly  
 112 denotes the displacement vector. Within the NB assumption, we have that

$$u_r(R, Z, t) = RU(Z, T), \quad u_\theta = 0, \quad u_z(Z, T) = W(Z, T), \quad (4)$$

113 whence the kinetic energy density is given by

$$\mathcal{T} = \frac{\pi A^2 \rho}{4} (2W_T^2 + A^2 U_T^2). \quad (5)$$

Similarly, we obtain

$$[\epsilon] = \begin{bmatrix} U & 0 & \frac{1}{2} R U_Z \\ 0 & U & 0 \\ \frac{1}{2} R U_Z & 0 & W_Z \end{bmatrix},$$

114 whereupon the strain-energy density easily follows

$$\mathcal{W} = \mu \left( 2U^2 + W_Z^2 + \frac{1}{2} R^2 U_Z^2 \right) + \frac{1}{2} \lambda (2U + W_Z)^2. \quad (6)$$

115 Integrating over the cross section

$$\mathcal{V} = \int_0^A \int_0^{2\pi} \mathcal{W} R d\Theta dR, \quad (7)$$

116 we obtain the potential energy per unit length

$$\mathcal{V} = \pi A^2 \left[ 2(\mu + \lambda)U^2 + 2\lambda U W_Z + \left( \mu + \frac{1}{2} \lambda \right) W_Z^2 + \frac{\mu A^2}{4} U_Z^2 \right]. \quad (8)$$

117 Two Euler-Lagrange equations naturally emerge

$$\frac{\partial}{\partial T} \frac{\partial \mathcal{L}}{\partial W_T} + \frac{\partial}{\partial Z} \frac{\partial \mathcal{L}}{\partial W_Z} = 0, \quad \frac{\partial}{\partial T} \frac{\partial \mathcal{L}}{\partial U_T} + \frac{\partial}{\partial Z} \frac{\partial \mathcal{L}}{\partial U_Z} - \frac{\partial \mathcal{L}}{\partial U} = 0. \quad (9)$$

118 namely (see (Shatalov et al., 2011, Eq.(65)) or (Graff, 2012, §8.3.3) where, however,  $u$  is our  $U/A$ )

$$\begin{aligned} (\lambda + 2\mu)W_{ZZ} + 2\lambda U_Z &= \rho W_{TT}, \\ \mu A^2 U_{ZZ} - 8(\lambda + \mu)U - 4\lambda W_Z &= \rho A^2 U_{TT}. \end{aligned} \quad (10)$$

119 In the framework of linear elasticity, equations (10) have been first derived by Mindlin and Herrmann (MH) (Mindlin,  
 120 1951), whence this system is usually named after them. Once acknowledging for different dimensional reduction,

121 Eqs.(10) correspond to (20) of Wright (1981), to which we refer for a nice discussion in terms of wave propagation. A  
 122 critique of the MH-equations is presented in many papers, see for example Whiston (1986), on the ground that, for the  
 123 assumed displacement (1), it is not possible to satisfy the load free condition at the mantle.

124 The Love (L-) *hypothesis* assumes a linear relationship between the radial displacement and the longitudinal strain  
 125 i.e

$$U = -\nu_0 W_Z, \quad (11)$$

where

$$\nu_0 = \frac{\lambda}{2(\lambda + \mu)} = \frac{1}{2} \frac{\kappa^2 - 2}{\kappa^2 - 1},$$

126 is the Poisson's ratio and  $\lambda$  and  $\mu$  are the Lamé parameters of linear elasticity. Here, we let  $c_L = \sqrt{(\lambda + 2\mu)/\rho}$   
 127 and  $c_S = \sqrt{\mu/\rho}$ , respectively the speed of longitudinal and shear body waves, alongside their ratio  $\kappa = c_L/c_S =$   
 128  $\sqrt{2(1 - \nu_0)/(1 - 2\nu_0)}$ . In the practical range  $0 < \nu < \frac{1}{2}$ , this ratio is always greater than  $\sqrt{2}$  and it becomes unbounded  
 129 for incompressible materials. Under (11), the dependence of  $\mathcal{T}$  and  $\mathcal{V}$  with respect to  $U, U_Z$  and  $U_T$  is replaced by  
 130 dependence with respect to  $W_Z, W_{ZZ}$  and  $W_{ZT}$  instead. Hence, it is now  $\mathcal{L}^* = \mathcal{L}^*(W_Z, W_T, W_{ZZ}, W_{ZT})$ , with  
 131 namely

$$\mathcal{L}^* = \frac{\pi A^2 \rho}{4} (2W_T^2 + A^2 \nu_0^2 W_{ZT}^2) - \pi A^2 \left\{ \left[ 2(\lambda + \mu)\nu_0^2 - 2\lambda\nu_0 + \frac{\lambda}{2} + \mu \right] W_Z^2 + \frac{\mu A^2 \nu_0^2}{4} W_{ZZ}^2 \right\}. \quad (12)$$

132 Carrying out the usual variational procedure we obtain the single partial differential equation describing the dynamics  
 133 of the rod

$$W_{ZZ} + \frac{\nu_0^2 K^2}{c_B^2} (W_{TTZZ} - c_S^2 W_{ZZZZ}) = \frac{W_{TT}}{c_B^2}, \quad (13)$$

where  $E = \mu(3\lambda + 2\mu)/(\lambda + \mu)$  is Young's modulus,  $K^2 = A^2/2 = I_2/S$  is the (square of the) polar radius of gyration  
 of the cross-section (whose area is  $S$  and whose polar moment of inertia is  $I_2 = \pi A^4/2$ ) and we have let the beam  
 longitudinal wavespeed

$$c_B = \sqrt{\frac{E}{\rho}} = c_s \sqrt{\frac{3\kappa^2 - 4}{\kappa^2 - 1}}.$$

134 Equation (13) is sometimes referred to as the Bishop-Love (BL) or the Rayleigh-Bishop equation (Shatalov et al.,  
 135 2011). Love's equation, as it appears in (Love, 1927, §278) or in (Graff, 2012, Eq.(2.5.61)) or in (Hutchinson and  
 136 Percival, 1968, Eq.(16)), is given by

$$W_{ZZ} + \frac{\nu_0^2 K^2}{c_B^2} W_{ZZTT} = \frac{W_{TT}}{c_B^2}. \quad (14)$$

137 Clearly, with respect to (13), this equation misses the fourth space derivative  $W_{ZZZZ}$  and the reason for this  
 138 discrepancy is that, in the literature, the potential energy considered for developing Love's equation (14) accounts  
 139 for the elongation term only, as in (Graff, 2012, Eq.(2.5.49)), namely

$$\mathcal{W} = \frac{E}{2} W_Z^2, \quad (15)$$

140 in contrast to the exact full strain-energy density of linear isotropic elasticity (6). In fact, Love specifically points out,  
 141 in his book, that transversal deformation is *considered only inasmuch as inertia effects are concerned*, statics being  
 142 already encompassed by the use of the Young's modulus in (15). It would therefore seem as the Love equation emerges  
 143 from a very special procedure, that is difficult to generalize.

144 It is possible to contrast the dispersion relation associated with Love's equation (14), namely

$$\omega^2 = c_B^2 k^2 \left( 1 - \frac{\nu_0^2 K^2}{c_B^2} \omega^2 \right), \quad (16)$$

145 against the exact dispersion relation obtained independently by Pochhammer and Chree (P-C) from the three  
 146 dimensional linear theory of elasticity, see (Graff, 2012, §8.2.2) or (Shatalov et al., 2011, Eq.(96)), i.e.

$$J_1(A\beta) \left( \frac{2\alpha(\beta^2 + k^2) J_1(A\alpha)}{A\beta} - \frac{(k^2 - \beta^2)^2 J_0(A\alpha)}{\beta} \right) - 4\alpha k^2 J_1(A\alpha) J_0(A\beta) = 0, \quad (17)$$

147 where  $J_n(k)$  are Bessel's function of the first kind (Abramowitz and Stegun, 1948, §9). Also,  $k$  is the wavenumber  
 148 along  $Z$ ,  $\omega$  is the angular frequency and

$$\alpha = \sqrt{\frac{\omega^2}{c_L^2} - k^2}, \quad \beta = \sqrt{\frac{\omega^2}{c_s^2} - k^2},$$

149 are the wavenumbers in the radial direction (for irrotational and solenoidal waves, respectively). Indeed, the Love  
 150 equation naturally emerges by taking a regular asymptotic expansion in the radius  $A$  of the first branch of the P-C  
 151 solution (Love, 1927, §201), namely

$$\omega^2 = c_B^2 \left[ k^2 + \frac{1}{2} K^2 \left( k^4 - \frac{(6\kappa^4 - 3\kappa^2 - 4)}{2c_B^2 \kappa^2 (\kappa^2 - 1)} k^2 \omega^2 + \frac{(\kappa^4 + \kappa^2 - 1)}{2c_B^2 \kappa^2 (\kappa^2 - 1) c_S^2} \omega^4 \right) \right] + O(A^3), \quad (18)$$

152 and then plugging into the correction term the leading order equation  $\omega^2 = c_B^2 k^2$ . Extending the analysis to the first  
 153 correction in the speed, we get

$$c_B^2 k^2 = \omega^2 \left( 1 + \frac{1}{2} K^2 \frac{v_0^2}{c_B^2} \omega^2 \right)^2, \quad (19)$$

154 that reduces to Love's equation provided that  $k \sim \omega \ll 1$ , that is in the LWLF regime. Furthermore, looking at the  
 155 eigenform, we get

$$U = -v_0 W_Z + \frac{v_0 K^2}{\kappa^2 - 1} \left( \frac{v_0 c_S^2}{c_B^2 (c_B^2/c_S^2 - 1)} + \frac{\kappa^4 - 2\kappa^2 + 2}{4\kappa^2} \frac{R^2}{A^2} \right) W_{ZZZ} + O(A^3), \quad (20)$$

156 where the leading order term is precisely the Love hypothesis, while the  $O(A^2)$  correction reveals a  $O(R^2)$  contribution  
 157 which embodies the deviation from the plane cross-section assumption.

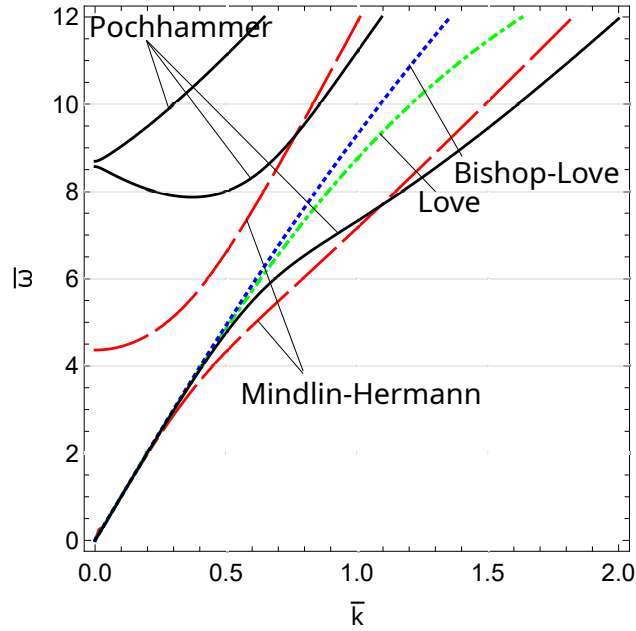
158 Similarly to Figure 2.27 of (Graff, 2012, p.120) or to Figure 1 of (Shatalov et al., 2011, p.208), this comparison  
 159 is illustrated in Fig.1 in terms of the frequency spectrum, and in Figs.2,3 in terms of the dispersion diagram.  
 160 Dimensionless wavenumber, frequency and wavespeed have been introduced in analogy with Graff (2012)

$$\bar{k} = (2\pi)^{-1} k A, \quad \bar{\omega} = \omega A / c_s, \quad \bar{c} = \frac{\omega}{k c_B} = \frac{c}{c_B},$$

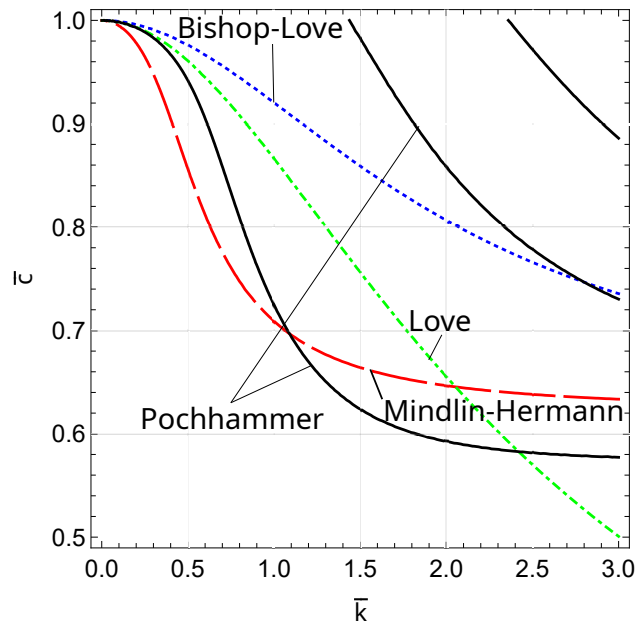
161 and so is the parameter value  $\nu = 0.29$ . These Figures show the curves from the P-C (17), Love (14), Bishop-Love (13)  
 162 and MH (10) models. It is clear that all equations are good low-frequency long-wavelength (LFLW) approximations  
 163 of the first branch of the P-C solution, which, however, fail already beyond small wavenumbers. Besides, Fig.3 reveals  
 164 that, as anticipated, the Love model best captures the LWLF regime. In contrast, the two mode MH-system and the  
 165 BL model provide a qualitatively accurate picture for large wavenumbers, given that they both plateau Graff (2012). Of  
 166 course, all such models are doomed to fail for it is known that, to obtain a good approximation of the exact solution, at  
 167 least four modes in the Taylor expansion of the axisymmetric deformation field needs to be considered Shatalov et al.  
 168 (2011).

169 Despite its shortcomings, the Love hypothesis is widely used and not only within the framework of the linear  
 170 theory of elasticity, whereto it properly belongs, but also in the nonlinear setting, see, for instance Dai and Fan (2004),  
 171 and references therein, or Ostrovskii and Sutin (1977), Sørensen et al. (1984), where, only apparently, a more general  
 172 approach is taken.

173 The aim of this paper is to provide a rigorous re-examination and justification of the Love hypothesis, moving from  
 174 the Navier-Bernoulli approximation, which may be easily extended to the nonlinear regime. This process will lead to  
 175 a *refined* Love hypothesis, whose merits will be apparent.



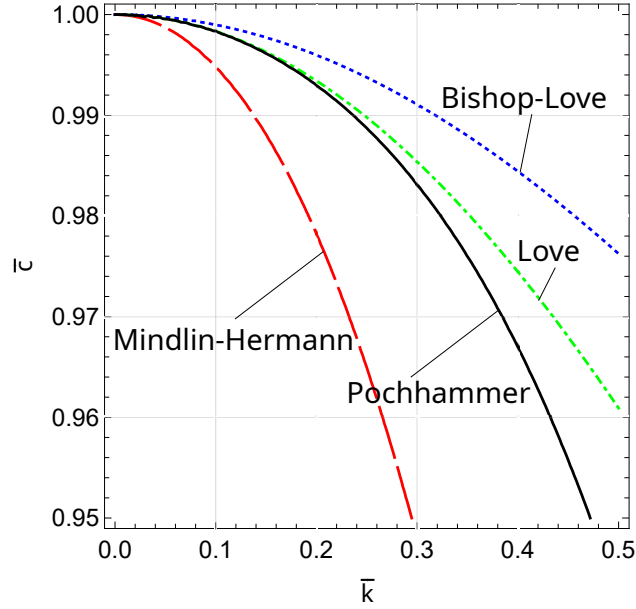
**Figure 1:** Dimensionless P-C frequency spectrum (black, solid) compared to that obtained from the Love (green, dash-dot), Bishop-Love (blue, dotted) and Mindlin-Herrmann (red, dashed) models ( $\nu = 0.29$ ,  $\delta = 0.2$ ).



**Figure 2:** Dimensionless P-C dispersion diagram (black, solid) compared to that obtained from the Love (green, dash-dot), Bishop-Love (blue, dotted) and Mindlin-Herrmann (red, dashed) model ( $\nu = 0.29$ ,  $\delta = 0.2$ ).

### 176 3. From the Mindlin-Herrmann system to Love equation

We begin by considering the relationship among the L-equation and the MH-system. For this, we introduce the dimensionless coordinate  $\zeta = Z/l$  and the time scale  $\mathfrak{T} = l/c$ , where  $l$  is any characteristic length, such as the rod length, and  $c$  is any speed, which we choose to be  $c = c_S$  for convenience. The dimensionless time is therefore



**Figure 3:** Low-frequency long-wave range in the P-C dispersion diagram (black, solid) compared to that obtained from the Love (green, dash-dot), Bishop-Love (blue, dotted) and Mindlin-Herrmann (red, dashed) model ( $\nu = 0.29$ ,  $\delta = 0.2$ ).

$t = T/\mathfrak{L}$ . We also set  $\delta = A^2/l^2 \ll 1$  and  $(U, W) = (u, l\omega)$ . In dimensionless form, equations (10) read

$$4(\kappa^2 - 1)u + 2(\kappa^2 - 2)w_\zeta - \frac{1}{2}\delta(u_{\zeta\zeta} - u_{tt}) = 0, \quad (21a)$$

$$2(\kappa^2 - 2)u_\zeta + \kappa^2 w_{\zeta\zeta} - w_{tt} = 0. \quad (21b)$$

177 By solving (21b), we obtain

$$u_\zeta = -\frac{\kappa^2}{2(\kappa^2 - 2)}w_{\zeta\zeta} + \frac{1}{2(\kappa^2 - 2)}w_{tt}, \quad (22)$$

178 and plugging this into Eq.(21a), differentiated with respect to  $\zeta$ , we obtain a single partial differential equation in terms  
179 of  $w$

$$\frac{c_B^2}{c_S^2}w_{\zeta\zeta} - \frac{\delta}{8(\kappa^2 - 1)}(\partial_{\zeta\zeta} - \partial_{tt})(\kappa^2\partial_{\zeta\zeta} - \partial_{tt})w = w_{tt}, \quad (23)$$

180 where  $c_B$  is the speed of elongation waves in rods. Eq.(23) may be recast in terms of dimensional variables

$$W_{ZZ} - \frac{K^2 c_S^2}{4c_B^2(\kappa^2 - 1)}(\partial_{ZZ} - c_S^{-2}\partial_{TT})(\kappa^2\partial_{ZZ} - c_S^{-2}\partial_{TT})W = c_B^{-2}W_{TT}. \quad (24)$$

181 This equation has already been determined in Wright (1981) and it may be rewritten as

$$W_{ZZ} + \frac{\kappa^4 - 1}{(\kappa^2 - 2)^2} \frac{v_0^2 K^2}{c_B^2} W_{ZZTT} - \frac{K^2 c_S^2}{4c_B^2(\kappa^2 - 1)} (\kappa^2 W_{ZZZZ} + c_S^{-4} W_{TTTT}) = c_B^{-2} W_{TT}, \quad (25)$$

182 so that it can be easily compared with Love's equation (13) and with the Bishop-Love equation (14). It is easily seen  
183 that they do not correspond, even in the static case. It is concluded that the unimodal problem emerging from the MH  
184 model does not reduce to either Love or Bishop-Love model. However, a hunch to a possible connection is obtained  
185 by solving (21a), whence

$$u = -v_0 w_\zeta - \delta \frac{1}{8(\kappa^2 - 1)} (u_{tt} - u_{\zeta\zeta}). \quad (26)$$

186 To leading order, this is indeed Love's hypothesis (11), which is then supplemented by a  $O(\delta)$  correction term  
187 proportional to the deviation from the shear wave speed. Indeed, such refined Love hypothesis will come naturally  
188 in the next Section from a multiscale analysis.

**189 3.1. Slow-time perturbation**

In a multiscale approach, we introduce the slow time  $\tau = \delta t$  and the moving coordinate  $\xi = \zeta - \hat{c}t$ , hence the dimensionless speed of the moving coordinate system is  $\hat{c}$ ,

$$u(\zeta, t) = \phi(\xi, \tau), \quad w(\zeta, t) = \psi(\xi, \tau).$$

Thus, the MH-system (21) becomes

$$-4(\kappa^2 - 1)\phi + (4 - 2\kappa^2)\psi_\xi - \frac{1}{2}(\hat{c}^2 - 1)\delta\phi_{\xi\xi} + \hat{c}\delta^2\phi_{\xi\tau} - \frac{1}{2}\delta^3\phi_{\tau\tau} = 0, \quad (27a)$$

$$(\kappa^2 - \hat{c}^2)\psi_{\xi\xi} + 2(\kappa^2 - 2)\phi_\xi + 2\hat{c}\delta\psi_{\xi\tau} - \delta^2\psi_{\tau\tau} = 0, \quad (27b)$$

190 whose solution is sought in asymptotic series

$$\phi = \phi_0 + \delta\phi_1 + \delta^2\phi_2 + \dots, \quad \psi = \psi_0 + \delta\psi_1 + \delta^2\psi_2 + \dots \quad (28)$$

191 To leading order, we obtain the compatibility condition

$$\hat{c} = \pm c_B/c_S, \quad (29)$$

192 whence the dimensional moving frame speed  $\hat{c}c_S$  equals  $c_B$ , that is the longitudinal wavespeed in rods. Also, we get

$$\phi_0 = -v_0\psi_{0\xi}, \quad (30)$$

193 which is the leading term in Love's hypothesis (11). Carrying on the analysis, we find that Love's hypothesis is *refined*  
194 up to  $O(\delta)$  terms through

$$\phi_1 = -v_0 \left( \psi_{1\xi} - \delta \frac{c_B^2/c_S^2 - 1}{8(\kappa^2 - 1)} \psi_{0\xi\xi\xi} \right) + O(\delta^2). \quad (31)$$

195 Besides, we obtain the governing equation for the travelling disturbance,

$$\frac{c_B}{c_S}\psi_{0\xi\tau} + \frac{v_0^2}{4} \left( \frac{c_B^2}{c_S^2} - 1 \right) \psi_{0\xi\xi\xi\xi} = 0. \quad (32)$$

196 Integrating in  $\xi$  and to leading order, Eq.(39) reduces to the well-known linear KdV equation, whose nonlinear form is  
197 similarly obtained by Dai and Fan (2004). This equation lends the time evolution of the longitudinal wave profile and,  
198 as it is well know, dispersion is introduced by the term  $W_{ZZZ}$ . Consequently, dispersion appears through  $(1 - c_S^2/c_B^2)$   
199 whereby the wave profile rests unchanged (hence no dispersion), inasmuch as  $c_B \approx c_S$ , that is bulk shear waves move  
200 with a speed close to that of longitudinal waves in the rod. This is never possible and the closer we can get is (for  
201 ordinary materials) for  $\kappa \rightarrow \sqrt{2}$ , so that  $1 - c_S^2/c_B^2 \rightarrow \frac{1}{2}$ . In contrast, when  $\kappa$  is extremely large, we get maximum  
202 dispersion for  $1 - c_S^2/c_B^2 \rightarrow 2/3$ . Accounting for (32), we can rewrite (30,31) consistently up to  $O(\delta)$  in the form

$$\phi_\xi = -v_0\psi_{\xi\xi} - \delta \frac{c_B}{c_S(\kappa^2 - 2)}\psi_{\xi\tau} + O(\delta^2), \quad (33)$$

203 which introduces an inertia-like correction.

Moving back to the original dimensionless variables, we have, to leading order,

$$\partial_{\xi\tau} = \frac{1}{2} \frac{c_B}{c_S\delta} \left( \partial_{\zeta\zeta} - \frac{c_S^2}{c_B^2} \partial_{tt} \right)$$

204 whence Eq.(32) reads

$$\frac{c_B^2}{c_S^2} w_{\zeta\zeta} - w_{tt} + \frac{1}{2} \delta v_0^2 \left( \frac{c_B^2}{c_S^2} - 1 \right) w_{\zeta\zeta\zeta\zeta} = 0, \quad (34)$$

205 that is resemblant of Eq.(23). Besides, plugging the leading term of (34) into the correction term, two equivalent forms  
 206 are obtained, namely

$$\frac{c_B^2}{c_S^2} w_{\zeta\zeta} - w_{tt} + \frac{1}{2} \delta v_0^2 (w_{\zeta\zeta t} - w_{\zeta\zeta\zeta}) = 0, \quad (35)$$

207 and also

$$\frac{c_B^2}{c_S^2} w_{\zeta\zeta} - w_{tt} + \frac{1}{2} \delta v_0^2 \left( 1 - \frac{c_S^2}{c_B^2} \right) w_{\zeta\zeta t} = 0. \quad (36)$$

208 Likewise, Eq.(33) becomes

$$u_\zeta = -v_0 w_{\zeta\zeta} - \frac{1}{2(\kappa^2 - 2)} \left( \frac{c_B^2}{c_S^2} w_{\zeta\zeta} - w_{tt} \right), \quad (37)$$

209 whose structure resembles that of (26). However, this form is not very attractive because it cannot be integrated with  
 210 respect to  $\zeta$  and it fails to bring out the  $O(\delta)$  nature of the correction. Naturally, an asymptotically equivalent form is  
 211 readily obtained through plugging the leading term of (34) into the correction term of (37) and integrating

$$u = -v_0 w_\zeta + \frac{\delta v_0^2}{4(\kappa^2 - 2)} \left( \frac{c_B^2}{c_S^2} - 1 \right) w_{\zeta\zeta\zeta}, \quad (38)$$

212 In terms of dimensional variables, Eq.(34) lends

$$W_{ZZ} - c_B^{-2} W_{TT} + v_0^2 K^2 \left( 1 - \frac{c_S^2}{c_B^2} \right) W_{ZZZZ} = 0, \quad (39)$$

213 while Eqs.(35,36), read, respectively,

$$W_{ZZ} - c_B^{-2} W_{TT} + c_B^{-2} v_0^2 K^2 (W_{TTZZ} - c_S^2 W_{ZZZZ}) = 0. \quad (40)$$

214 and

$$W_{ZZ} - c_B^{-2} W_{TT} + c_B^{-2} v_0^2 K^2 \left( 1 - \frac{c_S^2}{c_B^2} \right) W_{TTZZ} = 0. \quad (41)$$

215 Clearly, Eq.(40) corresponds to the Bishop-Love model (13), while Eq.(41) is the refined Love equation, the difference  
 216 with (14) being given by the term in round brackets. As expected, all these models coincide to leading order, and in  
 217 fact they collapse onto the leading order term in the P-C solution. Furthermore, as it may be physically anticipated,  
 218 dispersion, regardless of the differential form it takes, always appears as a function of the relative mismatch between  
 219 the speed of longitudinal and radial waves through the factor  $c_B^2/c_S^2 - 1$ . This feature is missing from the Love model  
 220 because of the fulfillment of the boundary conditions in the P-C model, wherefrom it ultimately comes.

221 Consideration of the refined Love hypothesis (38) in dimensional form gives

$$U = -v_0 W_Z + \frac{K^2 v_0^2}{2(\kappa^2 - 2)} \left( \frac{c_B^2}{c_S^2} - 1 \right) W_{ZZZ}, \quad (42)$$

222 that is similar to the first order eigenform (20), provided that complete correspondence is impossible given that the  
 223 cubic dependence on the radius is not accessible within the NB kinematics (4). In fact, it is precisely the refined Love  
 224 hypothesis that allowed us to guess the form of the correction term in the P-C solution as a multiple of  $W_{ZZZ}$ .

Also, returning to dimensional variables in the asymptotic series (28), we have

$$W = W_0 + A^2 W_1 + O(A^3), \quad (43a)$$

$$U = -v_0 W_Z + \frac{K^2 v_0^2}{2(\kappa^2 - 2)} \left( \frac{c_B^2}{c_S^2} - 1 \right) W_{ZZZ} + O(A^3), \quad (43b)$$

which reminds of the refined assumption introduced in (Porubov and Samsonov, 1993, Eq.(1)), that we rewrite in our symbols,

$$W = W_0 + R^2 W_1 + O(R^3), \quad (44a)$$

$$U = -v_0 W_{0Z} + R^2 U_1 + O(R^3). \quad (44b)$$

225 This structure comes from introducing higher order terms in  $R$  and, in fact, it contains three unknown functions of  
 226  $Z$  and  $T$  (i.e. it is tri-modal), two of which, namely  $W_1$  and  $U_1$ , may be used to accommodate the zero boundary  
 227 conditions on the radial stress at the mantle (the zero hoop stress BC being trivially satisfied from the kinematics)  
 228 Porubov and Samsonov (1993),

$$W_1 = \frac{1}{2} v_0 W_{0ZZ} \quad U_1 = -\frac{v_0^2}{2(3-2v_0)} W_{0ZZZ}. \quad (45)$$

229 However, we have already seen in (20) that this solution form cannot fully represent the P-C solution, because it misses  
 230 out the correction term in the form  $A^2 W_{0ZZZZ}$ , which is of the same order as (if not bigger than) the  $R^2 U_1$  contribution.  
 231 In this respect, the expression for  $U_1$  in (45) may be seen as complementary to our refined assumption (42), which  
 232 instead provides only the  $O(A^2)$  part of the correction. Yet, we point out that, following the multiscale analysis, the  
 233 refined Love hypothesis provides an expansion for  $u$  that is now consistent up to  $O(\delta)$  terms, within the NB kinematics.  
 234 How this affects the Lagrangian (12), in comparison with the original Love assumption, is now discussed.

#### 235 4. Unimodal refined variational model

236 It was shown that the variational procedure by which the Love equation is usually obtained, which makes use of  
 237 the Love hypothesis, really lends the BL equation instead (and this is because the Love hypothesis is meant for the  
 238 kinetic term only). The latter is not asymptotically equivalent to the Love equation, for it lacks the factor  $1 - c_S^2/c_B^2$  in  
 239 the correction term. One would therefore be lead to believe that the Lagrangian (12) is accurate only to leading order,  
 240 given that it was obtained by using the Love hypothesis, which lacks the correction term for  $U$ , i.e.  $U$  is only correct  
 241 to  $O(1)$ . However, it turns out that this is not the case and in fact the Lagrangian (12) is accurate up to  $O(\delta)$  terms  
 242 *regardless of the correction to the Love hypothesis*. In fact, we may say that the Lagrangian (12) accurately represents,  
 243 up to  $O(\delta)$ , a *family of Love-like assumptions*, which all differ by the correction term for  $U$ . This outcome follows from  
 244 the fact that, looking at (5,8), we see that the only terms where the correction to  $U$  appears are given by the first and  
 245 by the second term in the potential energy (8). However, it can be easily seen that, for any Love-like assumption, their  
 246 total contribution vanishes up to  $O(\delta)$ . Still, it should be emphasized that this cancellation seems entirely accidental  
 247 and it no longer takes place when, say, nonlinearity is taken into account.

248 To show that this is in fact the case, in the isotropic linear framework, we introduce the refined Love hypothesis  
 249 (33) into the system kinetic energy density

$$\mathcal{T} = \frac{1}{2} w_t^2 + \frac{1}{4} \delta v_0^2 w_{\zeta t}^2 - \frac{1}{2} \delta^2 \frac{v_0^2}{16(\kappa^2 - 1)} \left( \frac{c_B^2}{c_S^2} - 1 \right) w_{\zeta t} w_{\zeta \zeta \zeta t} + O(\delta^3), \quad (46)$$

250 as well as into the potential energy,

$$\mathcal{V} = \frac{1}{2} \frac{c_B^2}{c_S^2} w_{\zeta}^2 + \frac{1}{4} \delta v_0^2 w_{\zeta \zeta}^2 + \delta^2 \frac{v_0^2}{16(\kappa^2 - 1)} \left( \frac{c_B^2}{c_S^2} - 1 \right) \left( -w_{\zeta \zeta} w_{\zeta \zeta \zeta \zeta} + \frac{1}{2} \left( \frac{c_B^2}{c_S^2} - 1 \right) w_{\zeta \zeta \zeta}^2 \right) + O(\delta^3). \quad (47)$$

The Lagrangian density immediately follows

$$\begin{aligned} \mathcal{L} = & -\frac{1}{2} \frac{c_B^2}{c_S^2} w_{\zeta}^2 + \frac{w_t^2}{2} + \frac{1}{4} \delta v_0^2 (w_{\zeta t}^2 - w_{\zeta \zeta}^2) \\ & + \delta^2 \frac{v_0^2}{16(\kappa^2 - 1)} \left( \frac{c_B^2}{c_S^2} - 1 \right) \left[ -w_{\zeta t} w_{\zeta \zeta \zeta t} + w_{\zeta \zeta} w_{\zeta \zeta \zeta \zeta} - \frac{1}{2} \left( \frac{c_B^2}{c_S^2} - 1 \right) w_{\zeta \zeta \zeta}^2 \right] + O(\delta^3), \quad (48) \end{aligned}$$

251 and, as anticipated, it corresponds to Love Lagrangian up to  $O(\delta)$  terms. Naturally, the E-L equation is the BL equation  
 252 up to  $O(\delta)$  terms

$$-w_{\eta\eta} + \frac{c_B^2}{c_S^2} w_{\zeta\zeta} + \frac{1}{2} \delta v_0^2 (w_{\eta\eta} - w_{\zeta\zeta})_{\zeta\zeta} + \delta^2 \frac{v_0^2}{16(\kappa^2 - 1)} \left( \frac{c_B^2}{c_S^2} - 1 \right) \left[ \left( \frac{c_B^2}{c_S^2} - 1 \right) w_{\zeta\zeta} - 2w_{\eta\eta} \right]_{\zeta\zeta\zeta\zeta} = 0. \quad (49)$$

253 The natural boundary conditions holding at the rod ends, up to  $O(\delta)$ , read

$$\left( \frac{c_B^2}{c_S^2} w_{\zeta} + \frac{1}{2} \delta v_0^2 w_{\zeta\eta} \right) \mathfrak{d}w + \frac{1}{2} \delta v_0^2 (w_{\zeta\zeta} - w_{\zeta\zeta\zeta}) \mathfrak{d}w_{\zeta} = 0, \quad (50)$$

254 where  $\mathfrak{d}$  is the variation symbol, to avoid confusion with the small parameter  $\delta$ . Such conditions should be compared  
 255 with (Miklowitz, 1978, Eq.(7.23)) and we point out that the contribution of the strain variation  $\mathfrak{d}w_{\zeta}$  is there missing,  
 256 owing to the improper dealing of the strain energy. In particular, following Miklowitz (1978) to which we refer for  
 257 details, we observe that the dual condition on  $\mathfrak{d}w$  takes on an unexpected dynamic form which may lead to ill posedness.  
 258 However, using (34), we can equally write

$$\frac{c_B^2}{c_S^2} \left( w_{\zeta} + \frac{1}{2} \delta v_0^2 w_{\zeta\zeta} \right) \mathfrak{d}w + \frac{1}{2} \delta v_0^2 (w_{\zeta\zeta} - w_{\zeta\zeta\zeta}) \mathfrak{d}w_{\zeta} = 0, \quad (51)$$

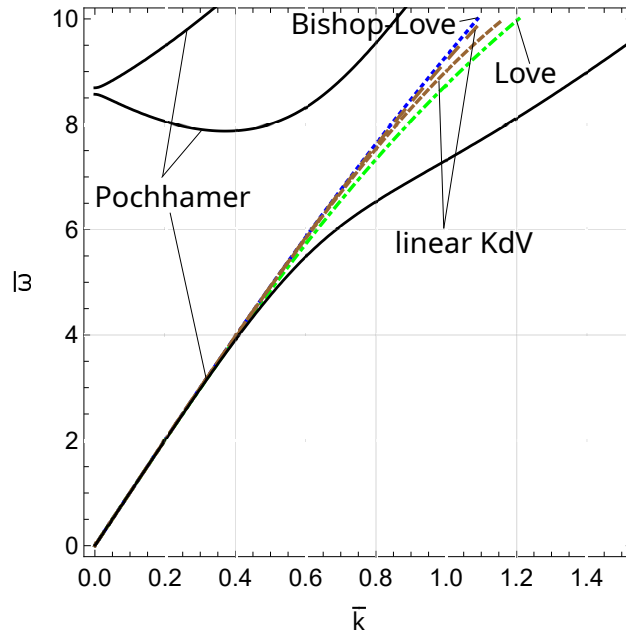
259 which no longer suffers from such drawback.

#### 260 4.1. Quality of the approximation

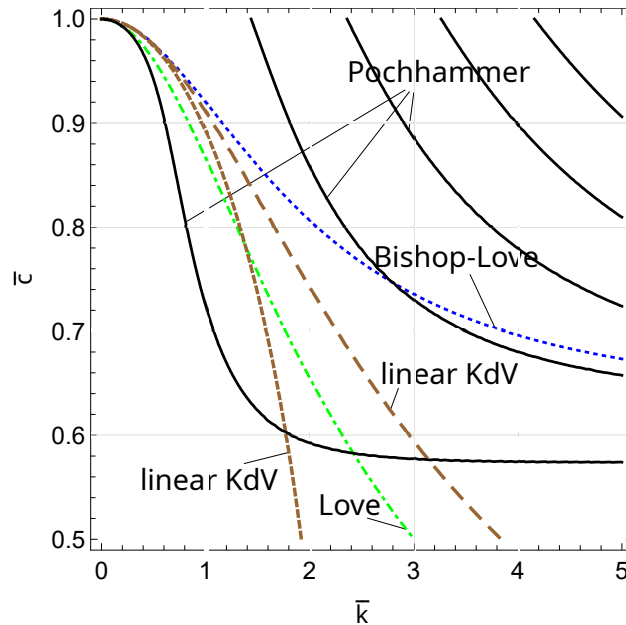
261 As we have already observed, the Love equation provides the best LWLF approximation to P-C and it cannot be  
 262 surpassed. However, it is interesting to investigate how well the linear KdV, in either of the forms (34), (35) and (36),  
 263 approximates the problem. Fig.4 shows the frequency spectrum for the P-C solution, alongside the Love, BL, and the  
 264 KdV (39,41) approximations. As already discussed, from a multiscale perspective, three models are equivalent and  
 265 correspond to the Love equation only to leading order. The frequency spectra are shown in Fig.5. All models, except  
 266 MH (not shown) and BL, fail to reproduce the flattening out of the frequency spectrum, that asymptotes to the Rayleigh  
 267 speed. The KdV (36) appears very similar to the Love model.

### 268 5. Concluding Remarks

269 A seemingly natural way to accommodate for dispersion in the equation for longitudinal waves in thin elastic  
 270 rods, originally introduced by A.H. Love, consists of accounting for the transversal motion of the cross-section. In  
 271 particular, the Love hypothesis relates the transversal to the longitudinal strain in the rod through Poisson's ratio.  
 272 Usually, this hypothesis is introduced in a two-modal kinematics connected to the Navier–Bernoulli assumption of  
 273 plane cross-sections remaining plane after deformation. The Love equation, encompassing dispersion, is finally arrived  
 274 at by Hamilton's principle. Although this derivation appears in every classical textbook, its examination reveals that  
 275 proper dealing with the elastic energy leads instead to a variant of the Love equation, sometimes named the Bishop-  
 276 Love equation. Indeed, we show that the Love equation is most simply obtained from the regular expansion of the  
 277 Pochhammer-Chree (P-C) frequency equation for longitudinal waves in cylindrical elastic rods, assuming the cylinder  
 278 radius  $A$  to be small. More specifically, the Love equation is merely a long-wave low-frequency approximation of this  
 279 solution and it matches the Bishop-Love equation only to leading order. This fact becomes important when dealing  
 280 with the nonlinear extension of this approach, which equally moves from a two-modal kinematics, in the absence of a  
 281 general solution like P-C to approximate. In the linear case, this leads to the well-known Mindlin-Herrman system of  
 282 equations. In the nonlinear case, the resulting system is often very complicated and extra assumptions are needed to  
 283 make progress. These assumptions often take the form of the Love hypothesis. One therefore wonders if this approach is  
 284 at least well founded in the linear case. Indeed, we show that the Love hypothesis may also be derived from a slow-time  
 285 perturbation of the Mindlin-Herrman system. In the process, the governing equation of the longitudinal perturbation is  
 286 arrived at, namely the linear KdV. These results suggest a rigorous method to generalize the Love hypothesis in more  
 287 general settings. Besides, it is shown that, already in the linear case, a correction to the Love hypothesis is demanded  
 288 to achieve consistency (with the accuracy of the longitudinal motion), and this correction is in fact proportional to the



**Figure 4:** Frequency spectrum for the P-C (black, solid), Love (green, dash-dotted), Bishop-Love (blue, dotted) and the linear KdV (39) (brown, short-dashed) and (41) (brown, long-dashed) for  $\nu_0 = 0.29$  and  $\delta = 0.2$



**Figure 5:** Dispersion diagram for the Pochhammer (black, solid), MH (red, dashed), Love (green, dash-dotted), Bishop-Love (blue) and for the refined model (39) (pink, solid) for  $\nu_0 = 0.29$  and  $\delta = 0.2$

289 second derivative of the rod longitudinal strain, i.e.  $W_{ZZZ}$ . This dependence of the correction on  $W_{ZZZ}$  is also met  
 290 when expanding, for  $A$  small, the P-C eigenform, although this also brings out cubic terms in the radial coordinate  
 291  $R \leq A$ , which are not accessible within our plane cross-section hypothesis. Also, the same form for the correction  
 292 term already appears in the literature, although for completely different reasons, namely in an attempt to enrich the  
 293 kinematics to tri-modal and therefore be able to meet two boundary conditions on the mantle, instead of the usual one.  
 294 Interestingly, in the linear isotropic framework (and in a two-modal kinematics), this correction term for transversal

295 strain may be taken freely, yet retaining a Lagrangian that is consistent to the first correction terms (and likewise for the  
 296 longitudinal motion). This surprising outcome results from cancellations in the Lagrangian, and in fact we may equally  
 297 define the Love hypothesis as the assumption through which first order terms in the transversal strain do not affect the  
 298 Lagrangian first correction. However, in the general case, the original Love hypothesis is not accurate enough, even  
 299 in the linear case, and should be refined. Besides, slow-time perturbation lends static boundary conditions which no  
 300 longer cause stress-type problems to be ill-posed. The application of this approach to non-linear scenarios will form  
 301 the basis for future work.

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## 309 Conflict of Interest statement

310 Authors have no conflict of interest to declare.

## 311 Data Availability

312 This paper makes use of no data.

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