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A cohesive FE model for simulating the cracking/debonding pattern of composite NSC-HPFRC/UHPFRC members

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Abstract

The aim of this work is to propose to practitioners a simple cohesive Finite-Element model able to simulate the cracking/debonding pattern of retrofitted concrete elements, in particular Normal-Strength-Concrete members (slabs, bridge decks, pavements) rehabilitated by applying a layer of High-Performance or Ultra-High-Performance Fiber-Reinforced-Concrete as overlay. The interface was modeled with a proper nonlinear cohesive law which couples mode I (tension-crack) with mode II (shear-slip) behaviors. The input parameters of the FE simulation were provided by a new bond test which reproduces a realistic condition of cracking/debonding pattern. The FE simulations were accomplished by varying the overlay materials and the moisture levels of the substrate surface prior to overlay, since findings about their influence on the bond performances are still controversial. The proposed FE model proved to effectively predict the bond failure of composite NSC-HPFRC/UHPFRC members.

Keywords: composite structures; UHPFRC layer; debonding damage; numerical modeling; bond tests; peeling stress; shear stress; contact problem

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1. Introduction

1.1. The technology of the overlay materials : HPFRC and UHPFRC

Advanced cement-based materials and emerging techniques for the design and protection of existing concrete members have been developed in the last decades. Relevant is the growing number of applications of High Performance-Fiber-Reinforced Concrete (HPFRC) on damaged concrete members [16, 32]¹. Very interesting is also the recent application of Ultra-High Performance-Fiber-Reinforced Concrete (UHPFRC ²) in pilot projects, e.g. rehabilitation of bridge deck overlays [13, 27] and reinforcement of hydraulic structures [25, 43]. The mechanical performances of UHPFRC are superior than those of ordinary and high-performance concretes. Beside its higher strength, low permeability and high energy absorption [13], UHPFRC has also shown high bond strength and good adherence to substrate made of normal-strength concrete (NSC) [1, 29, 54]. A large experimental investigation on the behavior of structures rehabilitated with UHPFRC revealed that such a material enhances the structural performances of composite members. However, the works in [1, 13, 42, 59] confirmed that the structural resistance of the composite material NSC-UHPFRC strongly depends on the bonding conditions.

1.2. The bond performances : the risk of cracking/debonding failures

A key issue of retrofitted concrete members concerns the risk of premature deterioration in the bonding region. This phenomenon is often observed in the practice after a period of service. According to the investigations above mentioned, the application of HPFRC and UHPFRC as overlay might reduce such a risk, if precautionary measures are taken into account. In the field of the retrofitted concrete structures the term *interface* relies on the penetration and hardening of the overlay inside the open cavities at the surface of the concrete substrate, resulting in a physical anchorage [8]. Two main factors can deteriorate such adhesion: the different volume changes between overlay and substrate and the effects of the external mechanical loading applied on the composite. For both cases, it is possible to distinguish different patterns of failure: i) the peeling stress perpendicular to the interface exceeds the

¹Recent studies about damage in the framework of finite elasticity can be found in [36, 37, 38, 53].

²whose mechanical performances are better than HPFRCs [15, 48, 49, 50]

33 tensile strength, which causes **crack opening** (mode I); ii) the shear stress
34 along the interface exceeds the respective strength, which causes **slip** (mode
35 II); iii) a mix of mode I and mode II [24]. The latter is usual in retrofitted
36 concrete members, such as slabs, bridge decks and pavements, see Fig. 1.



Figure 1: Switzerland 2018 [12] - Retrofitting of a bridge deck member by using a commercial UHPFRC

37 These composite structures are frequently stressed to bending loads. Near
38 to zones of maximum negative moment the bending load induces a high stress
39 at the interface of mode I which, detrimentally, adds its effects to mode II.
40 If in these zones, there exist some discontinuities of the overlay, e.g. bound-
41 ary locations, joints or cracks, the cracking/debonding failure might occur
42 [23](Fig. 2). In such conditions the bond failure is governed by a mutual
43 interaction between mode I and mode II [24]. Current bond tests can assess
44 the bond performances subjected to solely mode I (Pulloff test) or to a given
45 combination of mode I and mode II (Slant/shear test). The latter, accord-
46 ing several authors, may not be so representative since unrealistic loading
47 conditions are applied at the interface [17]. Few research have focused on

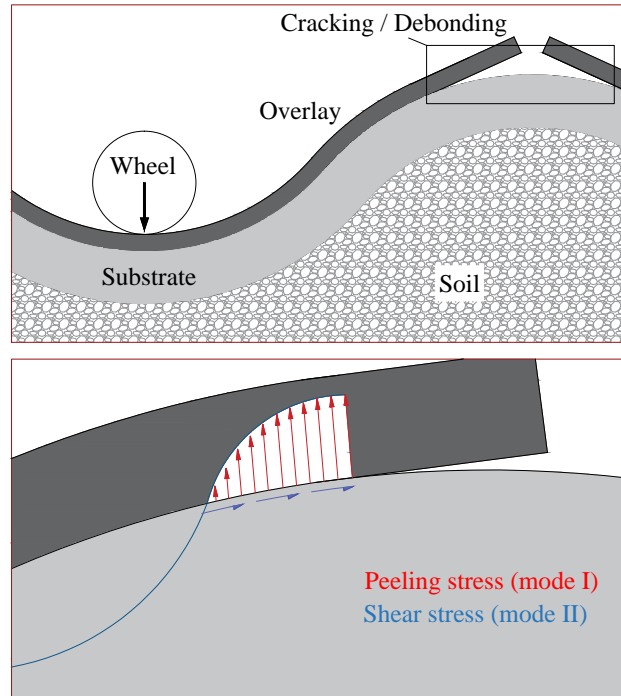


Figure 2: Illustration reported in [23] of a cracking/debonding path along the interface due to loading conditions on concrete pavements repaired by a layer of cement-based overlay

48 a finely prediction of the realistic mixed mode pattern, by coupling pulloff
 49 and slant/shear tests and adopting some empirical bond failure envelopes
 50 such as the Griffith theory and the Mohr-Coulomb criterion. Despite the
 51 efforts carried out by these authors, attempts according to the Griffith the-
 52 ory have proved unsuccessful, while the Mohr-Coulomb criterion is concerned
 53 with stress states within a material rather than at the interface between two
 54 bonded together [2]. In conclusion, by adopting current bond tests the risk
 55 to overestimate the bond performances is high, since they cannot reproduce
 56 a realistic conditions of cracking/debonding failure. Experimental evidences
 57 have also confirmed that the bond performances are sensitive to the substrate
 58 preparation prior to overlay. Recent works pointed out that the type of the
 59 overlay used and the moisture condition of the concrete substrate surface at
 60 the time of application of the overlay strongly affect the development of the
 61 bond strength. Certain authors stated that a *dry* substrate condition prior
 62 to overlay leads to better performances of the bond than *saturated-surface-*
 63 *dry* (SSD) conditions; in certain cases, SSD treatment was even detrimental

64 [6, 57]. Different observations were presented in [40, 56], claiming that SSD
65 condition improved the bond strength. Other authors suggested that the op-
66 timal saturation level ranges from 55 to 90% [9]. It can therefore be concluded
67 that these findings confirm that such a phenomenon is still controversial and
68 further investigations are needed.

69 1.3. Numerical investigations (FE simulation)

70 It is well known that the interaction between the composite concrete
71 members represents a relevant challenge in a numerical modeling, due to the
72 complicated nature of their adhesion [52]. Concerning studies have been very
73 limited in the past. The investigation of [1] and [45] predicted the behavior
74 of composite NSC-UHPFRC members using a 3D FE analysis under the as-
75 sumption of a perfect bond at the NSC-UHPC interface. This assumption
76 increases the risk to overestimate the ultimate capacity of the composite
77 structure. Other authors like [33] modeled the interface of a composite NSC-
78 UHPFRC member but no experimental data were available for validate their
79 model. Even though the efforts accomplished in the above-mentioned works
80 have been shown relevant outcomes, a calibration of the FE data on the ba-
81 sis of the experimental results was missing, or experimental investigations
82 were carried out without any numerical simulations. Recently, some works
83 proposed FE models calibrated on the basis of the experimental data. It is
84 interesting to note that different approaches for modeling the interface were
85 proposed in these works. [60] proposed equivalent beam elements to repre-
86 sent the bond behavior at the interface, instead [21] proposed to construct an
87 interface material between the concrete layers used. Both models proved to
88 be efficient and were validated by comparing their results with a three-point
89 flexural test. It is important to note that these models reduce the overesti-
90 mation of the bond performances as compared to “tie” models, in particular
91 when either no surface preparation or no bonding agent are employed in cer-
92 tain cases [11, 21]. Despite their good efficiency the aforementioned models
93 are complex and risk to reduce the practical interest of the practitioner which
94 tends to simplify its numerical simulations by using “tie” interface conditions
95 [31, 47]. However, with this assumption, the behavior of the interface cannot
96 be directly observed when the cracking/debonding failure begins, so the risk
97 to overestimate the bond performances increases. **Furthermore their calibra-**
98 **tion should be done on the basis of realistic experimental tests [19, 20].**

99 2. Scope

100 This paper presents a simple cohesive FE model able to simulate the
101 cracking/debonding failure of retrofitted concrete structures, in particular
102 a NSC member (e.g. slabs, bridge decks, pavements, etc.) rehabilitated
103 by applying a layer of HPFRC or UHPFRC as overlay. The interface has
104 been modeled with a series of vertical and horizontal truss elements which
105 permits to predict the bond loading capacity and the propagation of the
106 cracking/debonding path along the interface, on the basis of the energy bal-
107 ance concept of the fracture mechanism [44]. The mechanical response of the
108 truss elements is provided by a nonlinear cohesive law which couples mode I
109 (tension-crack) with mode II (shear-slip) behaviors. The nonlinear cohesive
110 law has been defined on the basis of the experimental data provided by a
111 new bond test designed by authors. The advantage of this test, compared
112 to the current ones, is to reproduce a realistic cracking/debonding failure of
113 the composite members, preventing the risk to overestimate the bond per-
114 formances. Different overlay materials and moisture levels of the substrate
115 surface prior to overlay are also taken into account, since findings about their
116 influence on the bond performances are still controversial.

117 The present work is organized as follows: a description about the experi-
118 mental campaign carried out for calibrating the input parameters of the co-
119 hesive FE model is provided in Section 3; in Section 4 the cohesive FE model
120 is presented; in Section 5 the FE simulations are analysed and compared with
121 the experimental results; the main conclusions are drawn in Section 6.

122 3. Experimental program

123 In order to consider the effect of different environmental conditions, six
124 slabs of substrate NSC 200x820x1140 mm were cast outdoors, both in sum-
125 mer and winter. 28 days later the slabs were demolded and exposed to
126 external weather conditions ranging from 24 °C and 74% RH in summer and
127 7 °C and 87% RH in winter, for further 90 days. Then, the upper part
128 of the NSC substrate (about 50 mm) was removed by hydro-jetting. The
129 roughness profile provided by the hydro-jetting was analyzed according to
130 the photogrammetric method. In particular a commercial software Agisoft
131 PhotoScan processed digital images and generates 3D spatial data of the
132 scanned substrate surfaces. The processed data provide the roughness alti-
133 tude in 4 points per square millimeters. Since the interface area of each

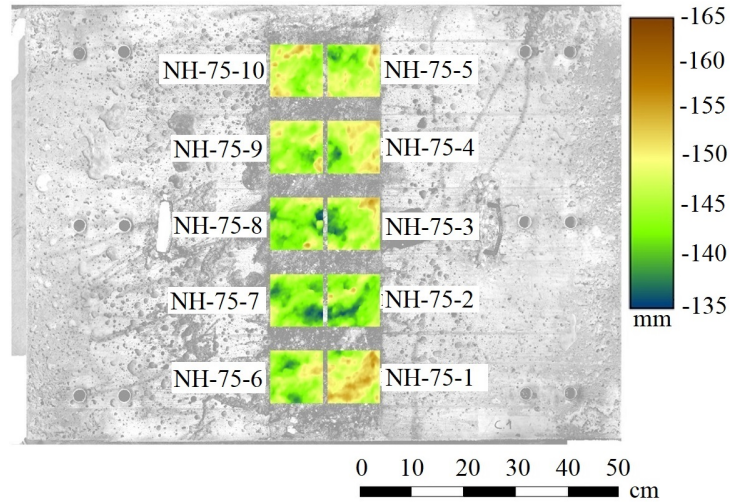


Figure 3: Roughness profile scanned for a given series (measuring in meters)

134 specimen was 100×100 mm, a population of 40000 points was used to cal-
 135 culate the average roughness and its standard deviation for each series. The
 136 analysis of the roughness magnitude was conducted for all series showing
 137 very similar values, as reported in Table 1. The colored area in Figure 3
 138 represents the roughness profile of the substrate prior to the application of
 139 the overlay. Results agreed with the investigation of [41].

Interfacial zone	Minimum (mm)	Maximum (mm)	Average (mm)	Stand. Dev. (mm)
NH-75-_1	139.1	157.1	150.2	3.13
NH-75-_2	135.7	154.0	143.6	3.16
NH-75-_3	136.3	156.5	145.9	3.82
NH-75-_4	136.4	155.0	147.2	3.90
NH-75-_5	137.3	156.5	146.8	3.22
NH-75-_6	136.9	153.6	145.7	3.19
NH-75-_7	134.5	151.9	143.1	3.05
NH-75-_8	135.2	156.0	144.3	3.17
NH-75-_9	139.2	154.0	146.3	2.81
NH-75-_10	141.2	155.6	147.4	2.89

Table 1: Logged roughness profile for a given series

140 The substrate surface provided by hydro-jetting was properly cleaned and
 141 moistened according to different moisture levels prior to the application of

Compounds	kg in 1 m ³ of composite	
	HPFRC	UHPFRC
Premix (cement, silica fume, sand)	2135	1970
Water	230	195
Superplasticizer	21.3	39
Hooked steel fibers 30/0.6 mm	25 (0.3 %)	-
Straight steel fibers 13/0.175 mm	-	296 (3.8 %)

Table 2: Material composition of the overlay

142 the overlay. Then, a commercial HPFRC was poured on three slabs, and a
 143 commercial UHPFRC³ was poured on the other ones. The material compo-
 144 sition of the overlay are reported in Table 2.

145 After 28 days of curing of the overlay the specimens were prepared for
 146 bond testing. The mechanical properties of the overlays used are reported in
 147 Table 4.

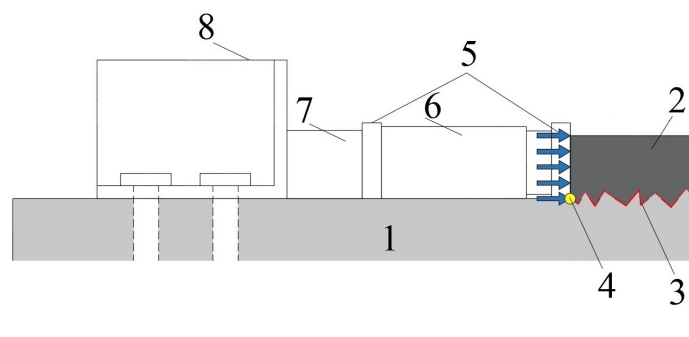


Figure 4: Bond test configuration designed by authors: (1) substrate, (2) overlay, (3) interface, (4) slip point measured by LDTV, (5) bearing plates, (6) loading device, (7) force transducer, (8) rigid support

148 The specimens were labeled according to both type of bonded materials,
 149 i.e. NH and NU stand for NSC-HPFRC and NSC-UHPFRC respectively,
 150 and the moisture levels of the substrate surface prior to overlay. The whole
 151 range of possible moisture conditions expected in the field was taken into
 152 account in series investigated, in particular dry, 75% and SSD. Dry-type sur-
 153 face was reached by curing the substrate surface for 14 days at laboratory

³previously investigated in [48]

154 conditions of $23 \pm 2^\circ\text{C}$, $55\% \pm 5\%$ RH, as also seen in [3]. During the curing,
155 surface substrate was covered with a plastic sheet, in order to slow down
156 the carbonation process. 75% and SSD conditions were achieved by keep-
157 ing wet the substrate surface for 24 hours, then surface was manually dried
158 with towels to attain the SSD conditions. Several hours later, at laboratory
159 conditions, a moisture level of 75% was reached. The surface moisture level
160 was measured by a superficially encased relative humidity probe, in particu-
161 lar a ROTRONIC type HC2-AW. The digital probe signal is processed by a
162 Hygro Palm 23 multifunction hand-held indicator. It provides temperature,
163 RH and time of measure. In order to detect the cracking/debonding failure
164 observed in field, a proper bond test, was designed by the authors. In [51],
165 Silfwerbrand J. presented various test methods used to evaluate the bond
166 strength at the interface. Among them, pull-off and slant/shear tests were
167 also adopted in standards ASTM [61] and [62], respectively. Even though in
168 [51] Silfwerbrand J. mainly presented a torsional bond test method, he also
169 provided an overview about the lateral shear bond test method. The authors
170 attempted to find regulations and other works containing further details of
171 such a test method, but with poor results. However, lateral shear test was
172 adopted in this investigation since it can reproduce the realistic condition of
173 mixed mode expected in the field [23], see Fig. 2. An external load, parallel
174 to the interface, is applied to the overlay edge. The load transmits the shear
175 stresses along the interface (mode II). A peeling stress (mode I) arises on the
176 interface as soon as the shear load is applied, due to the eccentricity of the
177 shear load from the interface. A couple of LDTVs are placed on both sides of
178 the specimen for measuring the average slip/debonding at the point of load
179 application, see Fig. 4. The loading rate is very low (0.003 ± 0.002 MPa/s)
180 in order to properly detect the interfacial bond response [10].

181 4. Modeling of composite NSC-HPFRC/UHPFRC members

182 4.1. The code *Strand7*

183 The commercial software package **Strand7** ([4, 14, 22, 26, 46]) was adopted
184 for simulating a realistic case of cracking/debonding failure (Fig. 2) between
185 a NSC substrate and a cement-based overlay. The code provides a series of
186 tools and functions for obtaining the approximate solution of the problem
187 investigated, according to the steps listed below:

- 188 1. Defining the geometric and loading characteristics of the retrofitted
189 composite member;

- 190 2. Defining the material characteristics of the bonded materials (consti-
191 tutive equations);
- 192 3. Dividing the physical system into elements and nodes (meshing of both
193 the single materials and the interface);
- 194 4. Forming the element matrices (stiffness, mass and damping elements)
195 and vectors (nodal load and restraint elements);
- 196 5. Assembling the element matrices into global matrices and the element
197 vectors into global vectors;
- 198 6. Solving the global equilibrium equations for the primary unknown vari-
199 ables and generating element results (i.e. **kinematic** and stress field at
200 the interface);
- 201 7. Generating other useful result data such as transformation and extrap-
202 olation of results;
- 203 8. Investigating and interpreting the result data.

204 Step 1 to 3 are performed with the pre-processor; step 4 to 6 are performed
205 with the solver; step 7 to 8 are performed with the post-processor. The ap-
206 proximated solution considers the three physical laws of the continuum me-
207 chanic. The equilibrium equation system, which is formulated on the basis
208 of the principle of virtual work, is a direct result of considering force equilib-
209 rium and displacement compatibility at the nodes. The global equations are
210 solved by direct or indirect methods. The direct method uses the Crour's
211 algorithm to decompose the global matrices into a triangular form. Instead,
212 the indirect method uses the Pre-conditioned Conjugate Gradient algorithm
213 [55]. The solutions yield one or more vectors of nodal displacements which
214 are used to determine element stress and strain and nodal reactions in the
215 structural solution.

216 4.2. Modeling of the interface

217 In the composite concrete members the link layer between the substrate
218 and the overlay is usually composed by a porous media thin layer of 100
219 μm consisting of weak hydrates such as calcium hydroxide [6] and plays a
220 key role in the bond strength [7, 18, 58]. In addition, the high roughness
221 profile provided by common removal methods of the deteriorated concrete,
222 like hydro-jetting, increases the bond performances thanks to the interlocking
223 mechanism provided by the hydro-jetting [5]. This aspect is considered into
224 the model presented in the following. In **Strand7**, when two surfaces are
225 bonded a fictitious layer of zero thickness exists between these. The contact

226 condition/effect to be physically modeled requires that the interface provides
227 infinite stiffness so that the two surfaces cannot go penetrate each other. The
228 deformations around the interface area occur within the material on both side
229 of the interface [55]. For this purpose, the interface is modeled by so-called
230 *master-slave* elements. This kind of link, which is a module given by the
231 code, is not a real element like *beam* or *plate*. The master-slave link provides
232 the physical condition discussed above, by defining relationships between
233 two nodes so that the displacement of the selected components will be of
234 the same magnitude. Conceptually, a master-slave link will enforce the slave
235 node to follow the master node in the selected displacement directions, ei-
236 ther in the global coordinate system or in any user coordinate system, see
237 Fig. 5. Although the link is referred to as a master-slave link, there is no
238 real distinction as to which node is the master and which node is the slave.
239 For example, a master-slave link connecting node 1 to node 40 is identical
240 to one connecting nodes 40 and 1. During a processing, the solver will en-
241 force the condition that the two nodes have same displacement values for
242 the selected components. In the model, a smooth geometrical interface is
243 assumed, since the effect of the roughness profile on the bond strength can
244 be taken into account by properly calibrating the stiffness of the master-slave
245 links. The stiffness of the the master-slave link, in regard with the relative
246 displacements of its facing nodes (opening crack v and slip u), is calibrated
247 by pin-connecting the master-slave link to *truss* elements. In the code, a truss
248 element is a straight element pin-connected at its joints, which carries only
249 tensile and compressive forces along its axial direction. In a truss element
250 all loads can be applied to its joints and not between them. The mechanical
251 behavior of the truss elements was properly calibrated on the basis of the
252 experimental data, in order to simulate the peeling mode (I) and the shear
253 mode (II) responses at the interface. For this purpose, a nonlinear cohesive
254 law was adopted. The thickness FE interface layer was assumed to be 100
255 μm length, in agreement with [6]. An illustration is reported in Fig. 5.

256 The nonlinear cohesive law above mentioned can be defined into the code
257 by selecting the function *Stress vs Strain Table*. In this table it is possi-
258 ble to calibrate the mode I and mode II relationships that will govern the
259 mechanical response of the 100 μm -vertical and 1000 μm -horizontal truss
260 elements, respectively. This technique permits to directly calibrate the non-
261 linear response of the interface face to peeling and shear stresses induced
262 by the external load, until the peak of bond strength is reached. Then, the
263 propagation of cracking/debonding begins and the frictional effect ensures a

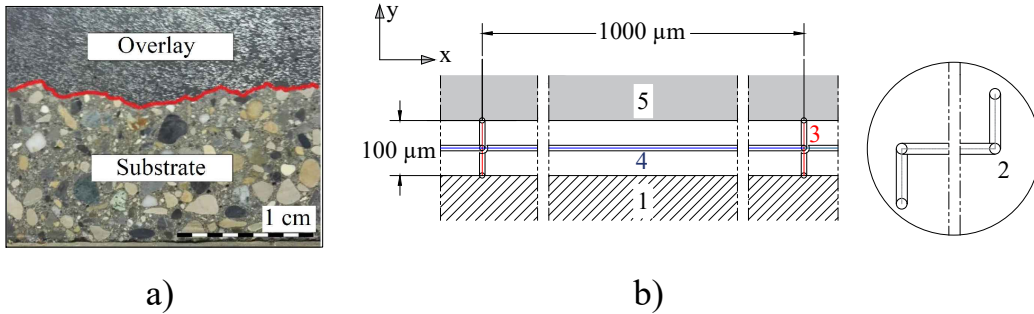


Figure 5: a) Interface profile observed by cutting the retrofitted member; b) Modeling of the interface between the substrate (MIR) (1) and the overlay (1-mm mesh) (5). The contact-condition effect between the two materials is modeled by using master-slave elements (2). The peeling-opening (mode I) and the shear-slip (mode II) relationships at the interface are modeled by using 100 μm -vertical (3) and 1000 μm -horizontal (4) truss elements, respectively

264 residual bond strength prior to reach the complete failure [24, 30, 47]. This
 265 important phenomenon cannot be directly accounted by nonlinear cohesive
 266 laws governing tied nodes. However, the residual strength provided by the
 267 frictional effect can be taken into account according to the energy balance
 268 concept of the fracture mechanism. While the cracking/debonding path in-
 269 creases, the peak of bond strength is kept constant in the truss elements,
 270 until the value of energy absorbed by the overall FE interface attains the
 271 value of the maximum energy absorbed by the real interface, prior to the
 272 complete failure. This approach requests, of course, several iterations for
 273 properly calibrating the cohesive law on the basis of the experimental test
 274 data, which are presented in Section 3. The construction of such a law into
 275 the code is illustrated in Fig. 6. The branches b-c in Fig. 6a and a-b/e-f
 276 in Fig. 6b correspond to the plateau of strength discussed above, which is
 277 reached when the propagation of cracking/debonding begins.

278 In the first iteration, the mode I and mode II relationships were calibrated
 279 on the basis of the results presented in [24]. As mentioned above, the final
 280 expressions of the cohesive law are fitted through an iterative process, until
 281 the simulated load - slip/debonding curve agrees with the experimental one
 282 presented in Section 3. The FE parameters of the nonlinear cohesive law
 283 showed in Fig. 6 are reported in Table 3, for all series investigated. In order
 284 to consider the fact that the flexural deformation of the overlay produces a
 285 compressive stress along certain regions of the interface, a compressive-strain

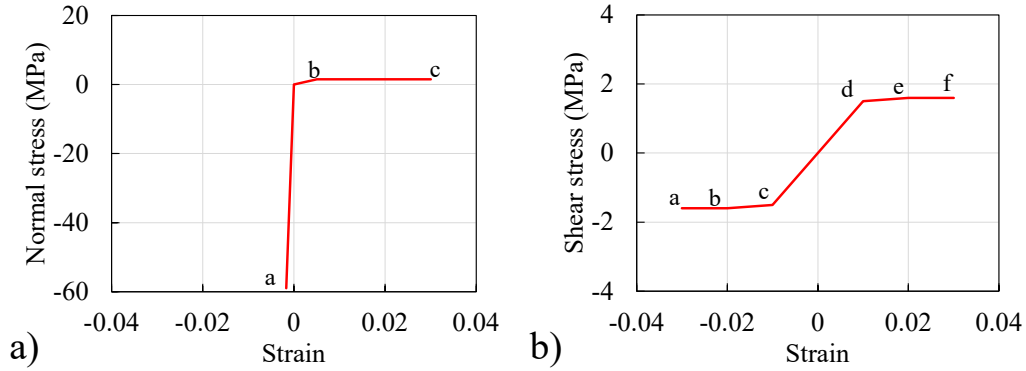


Figure 6: Strand7 environment. Series NH-dry: The function stress vs strain permits to construct the nonlinear cohesive law governing the interface response subjected to normal (a) and shear (b) stresses. In each figure, the points in which the slope of the function stress vs strain changes are labeled according to letter a, b, c, etc.

286 law was implemented (see the branch a-0 in Fig. 6a). In this law the peak
 287 point corresponds to the compressive strength of the weaker material between
 288 the substrate and overlay, i.e. the NSC substrate. The corresponding strain is
 289 derived as the ratio between the compressive strength and the elastic modulus
 290 in compression, both experimentally measured, see Table 4. For both signs
 291 of slipping (left towards or right towards) the horizontal truss response does
 292 not change in terms of absolute value, so $\tau(a) = -\tau(f)$, $\tau(b) = -\tau(e)$ and $\tau(c) = -\tau(d)$.

Series	Vertical truss						Horizontal truss					
	v(a)	v(b)	v(c)	$\sigma(a)$	$\sigma(b)$	$\sigma(c)$	u(a)	u(b)	u(c)	$\tau(a)$	$\tau(b)$	$\tau(c)$
	mm/mm			MPa			mm/mm			MPa		
NH-dry	-0.00169	0.005	0.03	-59	1.5	1.5	-0.03	-0.02	-0.01	-1.8	-1.8	-1.7
NH-75	-0.00169	0.005	0.03	-59	1.2	1.2	-0.03	-0.02	-0.01	-2	-2	-1.2
NH-SSD	-0.00169	0.005	0.03	-59	1.6	1.6	-0.03	-0.025	-0.01	-2.3	-2.3	-1.1
NU-dry	-0.00169	0.005	0.03	-59	1.7	1.7	-0.03	-0.02	-0.01	-2.8	-2.8	-1.8
NU-75	-0.00169	0.005	0.03	-59	2.1	2.1	-0.03	-0.025	-0.01	-3.1	-3.1	-1.4
NU-SSD	-0.00169	0.005	0.03	-59	3	3	-0.03	-0.02	-0.01	-4.5	-4.5	-3.4

NH: NSC bonded with HPFRC.

NU: NSC bonded with UHPFRC.

dry: dry substrate prior to be overlaid.

75: substrate moisture level of 75% prior to be overlaid.

SSD: substrate saturated-surface-dry prior to be overlaid.

Table 3: Interface: FE parameters

293 *4.3. Modeling of the single-materials (substrate and overlay)*

294 Besides the bonding properties, further properties that also affect the con-
 295 tact problems include the elastic modulus, the shear modulus, the Poisson’s
 296 ratio and the geometry of both bonded materials [35]. On the basis of the
 297 experimental data obtained from single-material tests, such properties were
 298 implemented into the FE code, see Table 4. It is worth mentioning that tests
 299 on single-materials are independent of the bonding properties of the bonded
 300 members.

Series	b	l	Overlay				h	Substrate	
			h	E	ν	f_c		Modeled	f_c
	mm	mm	mm	GPa	adim.	MPa	mm	as	MPa
NH-dry	100	100	50	38.3	0.17	78	200	MIR	59
NH-75	100	100	50	38.3	0.17	78	200	MIR	59
NH-SSD	100	100	50	38.3	0.17	78	200	MIR	59
NU-dry	100	100	50	47.1	0.2	147	200	MIR	59
NU-75	100	100	50	47.1	0.2	147	200	MIR	59
NU-SSD	100	100	50	47.1	0.2	147	200	MIR	59

b: width of the overlay.

l: length of the overlay.

h: thick of the overlay/substrate.

E: Elastic modulus measured according to the [63].

ν : Poisson’s ratio for HPFRC and UHPFRC estimated according to [39] and [28], respectively

f_c : Compressive cubic strength measured according to the [64]

MIR: Modeling of the substrate as a member infinitely rigid.

Table 4: Bonded materials: FE parameters

301 The elastic modulus E of the substrate is assumed to be 25700 MPa,
 302 according to the formulation reported in [65]. The surface area A_{sub} of the
 303 substrate and of the overlay A_{overl} along the vertical plane is 200×820 mm
 304 and 50×100 mm, respectively. Thus, the elastic and the surface ratios
 305 A_{overl}/A_{sub} between the overlay and substrate are about 1.6 and 0.03, re-
 306 spectively. The resulting stiffness ratio $EA_{overlay}/EA_{substrate}$ is about 0.045.
 307 Consequently, the substrate can be modeled as a member infinitely rigid
 308 (MIR).

309 In order to consider the non-linear response of the contact problem, a non
 310 linear static analysis was carried out. In **Strand7**, the nonlinear static solver

311 uses an algorithm based on the modified Newton-Raphson method to solve
312 the nonlinear equation system. The algorithm uses an iteration procedure
313 within each load increment to ensure that the equilibrium of forces is main-
314 tained, within a specified allowance, at the end of each load increment. An
315 incremental displacement history was assigned to the end side of the overlay
316 in order to simulate the cracking/debonding failure at the interface. Each
317 increment of displacement u , corresponding to the step 1, step 2, etc. of
318 the analysis, was small enough (0.0005 mm) to make the nonlinear analysis
319 efficient. It is worth noting that the resulting stress field was uniformly dis-
320 tributed along the width of the interface. This permitted to further simplify
321 the numerical calculations, by selecting the function of *2-D stress plane* and
322 modeling the layer of the overlay as a group of *plate*⁴ items.

323 In the field of FE models better solutions are given for meshes which have
324 both a simple geometrical shape and a sides' ratio close to 1 [55]. A 4-
325 node quadrilateral type was therefore employed for modeling the mesh of the
326 overlay. The mesh size of 1 mm was adopted, due to the fact that the inde-
327 pendence of the calculation result versus the mesh size was reached when the
328 node-to-node distance was ≤ 1 mm. The overlay size was of course defined
329 in respect to the size of the experimental specimen, see Table 4.

330 5. FE simulations and Results

331 As discussed in Section 4 a nonlinear static analysis was adopted for
332 stressing the interface to mixed mode, by increasing step by step the dis-
333 placement assigned to the end side of the overlay specimen, see Fig. 7. For
334 each increase of displacement the stress field arising on the modeled interface
335 was analyzed. In each step, the integration of the internal shear stress along
336 the modeled interface (Fig. 8b) must be equal to the experimental load F_x
337 applied to the end side of the overlay specimen (Fig. 8c). Instead the inte-
338 gration of the internal stress perpendicular to the interface must be equal to
339 zero in order to respect the vertical static equilibrium (Fig. 8a). The cohesive
340 FE model permitted to observe the propagation of the cracking/debonding
341 failure along the interface, as the external load increases. Fig. 8b denotes
342 that for small increases of displacement ($u < 0.0075$ mm, from step 0 to step
343 100) the punctual shear stress along the interface increases by moving toward

⁴The plate item is a surface element with a given thickness.

344 the edge side subjected to the external displacement u . This is due to the
 345 fact that the FE bonding response in mode II is still in elastic field : thus, the
 346 shear stress grows up as the slip magnitude increases, see Fig. 6b. For higher
 347 increases of displacement ($u > 0.0075$ mm, from step 100 to step 300) the
 348 yield strength in mode II is reached, therefore a plastic FE bonding response
 349 is achieved, see Fig. 6b. As a result, the punctual shear stress becomes al-
 350 most constant along the overall length of the interface and does not increase
 351 further, even though the slip/debonding keeps growing. The plastic behavior
 352 of the FE interface corresponds to the phenomenon of cracking/debonding
 353 which begins and quickly propagates along the real interface. This statement
 354 can be confirmed by observing the experimental curve in Fig. 8c. In par-
 355 ticular, the slip value corresponding to the drop in force just after the peak
 356 load recorded in the experimental curves almost corresponds to the total
 357 propagation of the cracking/debonding path along the modeled interface. In
 358 addition, for all series, the experimental-to-numerical peak load ratio $F_{x,exp}$
 359 / $F_{x,FEM}$ showed good accuracy. Also the initial stiffness was accurately
 360 predicted.

Step 1 (u = -0.0005 mm)

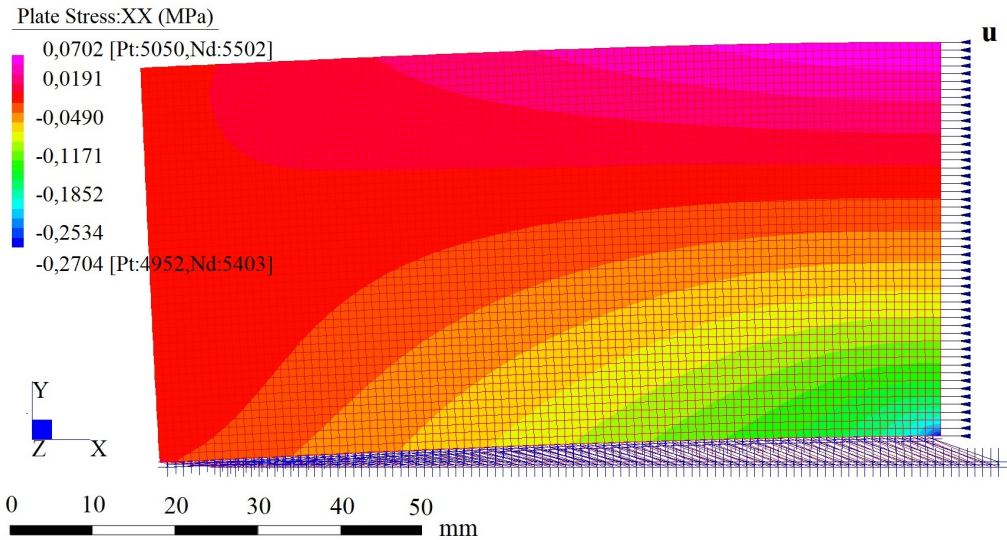


Figure 7: FE simulation of the cracking/debonding pattern of series NH-dry

361 Fig. 9 illustrates the cracking/debonding paths simulated on all series
 362 investigated, showing a good agreement with the experimental data. Each red

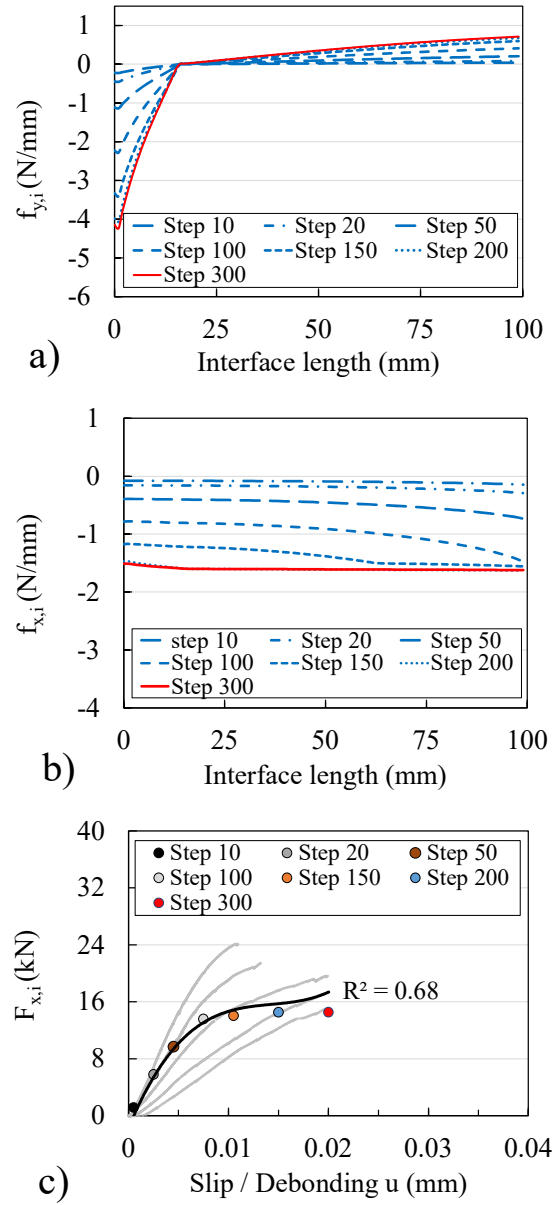


Figure 8: Analysis of the stress field on the modeled interface in series NH-dry recorded by the nonlinear static analysis: a) normal stress (mode I), b) shear stress (mode II). Load vs slip/debonding curve: c) simulation and experiment

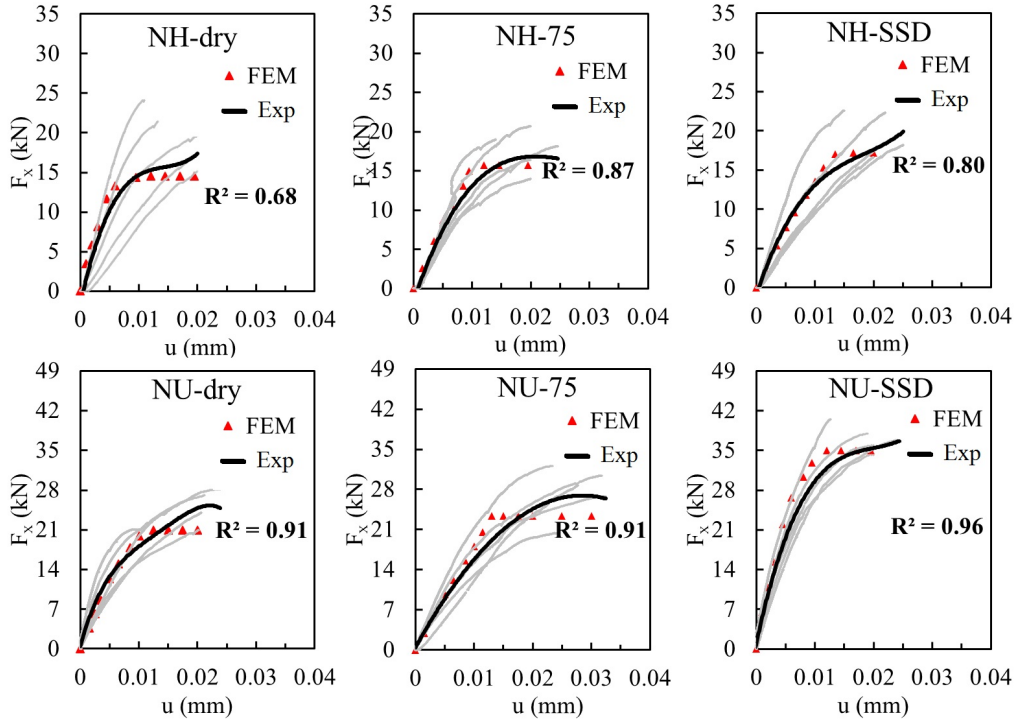


Figure 9: Numerical and experimental results of the model considering different conditions of type of overlay and moisture conditioning of the surface substrate prior to the application of the overlay

363 point in the figure represents the $F_{x,i}$ value corresponding to each increase of u
364 recorded by the experimental tests. In Figs. 8c and 9 the gray lines represent
365 the experimental curves recorded for each tested specimen. Instead, the
366 black curve represents the experimental average derived from a polynomial
367 regression analysis of the experimental data. Such a curve is considered
368 sufficiently representative because of its high R^2 value obtained. It can be
369 noted that a lower scatter of experimental data was recorded in NU series
370 (R^2 ranging from 0.91 to 0.96), especially for high moisture levels. Conversely,
371 higher scatter values were observed in NH series (R^2 ranging from 0.68 to
372 0.80), in particular for low moisture levels. This difference was likely due to
373 the fact that high moisture levels promote the hydration of the fresh overlay
374 in the interfacial zone, leading to stronger bond between substrate and
375 hardened overlay. This effect is magnified when a UHPFRC (NU series) is
376 used as overlay. The absence of aggregate within UHPFRC mixture permits

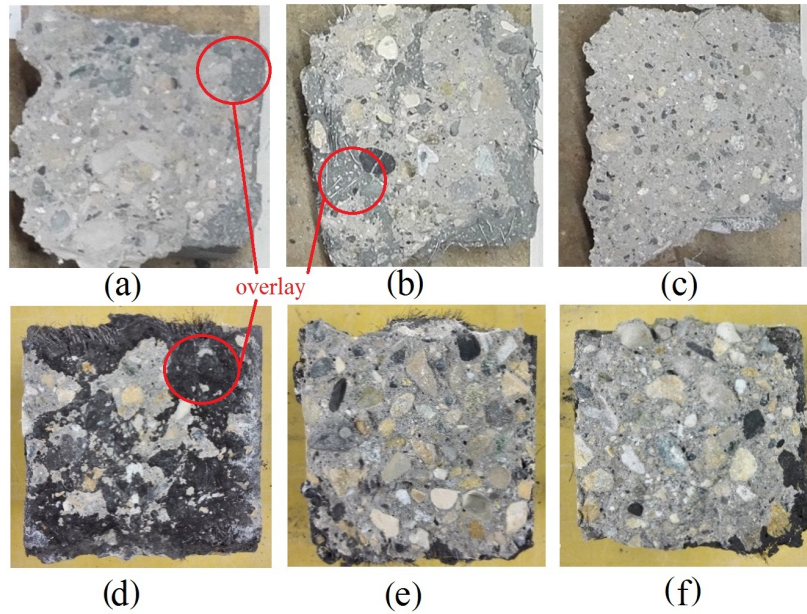


Figure 10: Surface failure observed after cracking/debonding of a) NH-dry, b) NH-75, c) NH-SSD, d) NU-dry, e) NU-75, f) NU-SSD

377 to extend the specific surface of adhesion between substrate and overlay, in-
 378 creasing the density of the interfacial zone. Both aspects reduce the defects
 379 along the interface and consequently explain the low scatter of results ob-
 380 served in NU series with high moisture levels as well, see Fig. 9.

381 The experimental results confirmed that lower moisture levels leads to lower
 382 bond strength values when UHPFRC is used as overlay. By contrast, when
 383 HPFRC is used as overlay the bond strength is almost the same under any
 384 moisture levels. Such a difference is probably due to the different w/c ratio
 385 between the two overlays investigated. The low w/c ratio of UHPFRC (< 0.2)
 386 makes this type of overlay highly sensitivity to the moisture level, especially
 387 under dry conditions. In such a condition an insufficient hydration of the
 388 fresh overlay in the interface zone occurred. This reduced the densification
 389 of the bond and its strength as well, showing a slight failure in the overlay, see
 390 Fig. 10. Instead, in the HPFRC series, the bond strength is less sensitive to
 391 the moisture level because of its higher w/c ratio (> 0.2). Series investigated
 392 confirmed that the application of UHPFRC as overlay provides higher load-
 393 ing bond capacity to the composite structure, compared to the application
 394 of HPFRC. In particular, it was observed a bond strength ratio between the

395 use of UHPFRC and HPFRC as overlay ranging from 1.13 to 2, see Table 4.

396 6. Summary and Conclusions

397 The cracking/debonding failure in composite NSC-HPFRC/UHPFRC mem-
398 bers was simulated using the developed cohesive FE model with Strand7
399 software. The interface has been modeled with a series of vertical and hori-
400 zontal truss elements which permitted to predict the bond loading capacity
401 and the propagation of the cracking/debonding path along the interface, on
402 the basis of the energy balance concept of the fracture mechanism. The me-
403 chanical response of the truss elements is provided by a nonlinear cohesive
404 law which couples mode I (peeling) with mode II (slip). The FE parameters
405 were finely calibrated on the basis of a bond test designed by the authors
406 which reproduces a realistic condition of cracking/debonding failure. The
407 main conclusions of this study can be drawn.

- 408 • The developed cohesive FE model yielded good predictions for the over-
409 all response of both the composite NSC-HPFRC and NSC -UHPFRC
410 members subjected to mixed mode. In particular, the FE model pre-
411 dicted the stress field and the propagation process of cracking/debonding
412 along the interface. These predictions are validated by the experimen-
413 tal load–slip/debonding test, in which the peak load and stiffness of
414 the numerical curves agree with the experiment;
- 415 • The technique to characterize the interface adopting truss elements gov-
416 erned by a nonlinear cohesive law proved to be effective for simulating
417 the cracking/debonding pattern of composite NSC-HPFRC/UHPFRC
418 members. This technique adequately assessed the bond loading ca-
419 pacity, whose performances exhibited a clear susceptibility to both the
420 type of the overlay used and the moisture level of the substrate prior
421 to be overlaid;
- 422 • All bond tests have showed that the cracking/debonding failure oc-
423 curred within the interface layer. For reproducing such a phenomenon
424 the technique of the nonlinear cohesive law adopted in the FEM re-
425 sulted appropriate, as confirmed by the numerical simulations;
- 426 • The presented FE model can be used for predicting the damage process
427 at the interface of retrofitted structures like bridge decks, pavements

428
429

and slabs, in which the mutual stress in **tension** and shear govern the failure pattern.

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